

LOMR

Mission Drive Conveyance
System

FEMA
LETTER OF MAP
REVISION APPLICATION

MARCH 2006



2727 S. Rainbow Boulevard, Las Vegas, Nevada 89146

Request for Letter of Map Revision
Mission Drive Conveyance System
Clark County, Nevada

Prepared for:

CITY OF HENDERSON
240 Water Street
Henderson, Nevada 89009

Prepared by:

VTN Nevada
2727 S. Rainbow Boulevard
Las Vegas, Nevada 89146
(702) 247-4020



March 2006

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1.0 INTRODUCTION

The purpose of this Letter of Map Revision (LOMR) is to analyze and address a needed revision to the C-1 Channel Watershed flood zone, in City of Henderson, Nevada, Clark County Zone A. This analysis provides documentation that demonstrates that the post-improvement conditions no longer warrants some of the flood zone delineations shown on the existing FIRM Panel 2615 dated, September 27, 2002. Due to the expanding development in this area for both residential and commercial sectors, necessary flood control facilities have been installed to accommodate the expanding growth. The flood control facility now in place is a 6'x6' RCB along Greenway Road from Paradise Hills to Mission Drive. The RCB outlets into the existing flood control channel along I-515. Flood control facilities along Greenway Road can be found in Mission Drive/Greenway Road Improvements (Paradise Hills to Greenway Road to College Drive), by VTN Nevada Final Drainage Design February 2004. With new flood control facilities in place current flood zone and floodplain areas are no longer current with today's urbanization.

Refer to Figure 1.0 Area/Vicinity Map for an overall view of the project area.

This LOMR request will analyze a portion of the Mission Drive flood zone, and will demonstrate that the future conditions no longer require certain flood zone delineations that are shown on the current effective FEMA FIRM Panel 2615 dated, September 27, 2002.

2.0 HYDROLOGY

The *HEC-1 Flood Hydrograph Computer Model* was developed by the U.S. Army Corps of Engineers Hydrologic Engineering Center in the late 1970's, and then adopted by the *CCRFGD Hydrologic Criteria and Drainage Design Manual* in 1999 for rainfall and runoff predictions. The model is used to simulate the surface runoff response of a watershed to a design rainfall event. Each subbasin in the watershed is described by a set of parameters that specify the subbasin drainage and storm characteristics. These basin parameters include precipitation, basin area, curve number, and lag time.

To use the HEC-1 computer model, the drainage system in a watershed is converted into a node-link type of system. A node is placed at the subbasin outlet or at the design point along the water course. Links between nodes represent conveyance elements in the drainage system. Hydrographs are computed for each subbasin and are placed at the subbasin outlet node. These hydrographs are then routed and/or combined according to the drainage basin network configuration through links. The DARF (Depth Area Reduction Factor) is known at each design point and is used to determine the peak flow at the design point depending on the contributing area.

Pre-Project Conditions – HEC-1

Prior to Mission Drive/Greenway Road Improvements, during a 100-yr storm runoff contributing flow from subbasins, C1G2B1, C1G2B2, & C1G2A (see Figure 1.1) would flow down the natural channel into what is now the current FEMA flood zone. Design flows for Mission Drive Pre-Project conditions (Effective/Corrective Model), was modeled after the C1 Channel FIS Hydrology Study by Carter Burgess and was used for the Pre-Project Condition HEC-RAS.

Since there are three contributing subbasins to the Pre-Project condition there are three flow design points that are used to model the Pre-Project HEC-RAS condition taken from C1 Channel FIS Hydrology Study by Carter Burgess , HEC-1 design point C1G2B1 (286 cfs) which contains the flow from its respective subbasin, design point CP7B (490 cfs) which includes subbasin C1G2B2 routed & combined with subbasin C1G2B1, and finally CP7C (799 cfs) which includes subbasins C1G2B1, C1G2B2 & C1G2A.

Post-Project Conditions – HEC-1

Design flows that was used for modeling was derived from C1 Channel FIS Hydrology Study, but was modified to meet Post-Project Conditions. Subbasins C1G2B1, & C1G2B2 were delineated to account for Mission Drive Improvements Post-Project Conditions. C1G2B1 was split up into two subbasins C1G2B0 & C1G2B1, since all of the flow from C1G2B1, is collected within the Mission Drive/Greenway Road System, the remaining area east of Greenway Road becomes subbasin C1G2B0. Subbasin C1G2B2 was delineated based on inspection of 5-foot contours which resulted in subbasins C1G2B2, C1G2B3, C1G2B4, & C1G2B5 (see Figure 1.2). New areas, CN & Lag times were calculated for all new subbasin delineations which are included in Appendix C.

There are seven contributing subbasins to the Post-Project condition, there are four HEC-1 flow design points, design point C1G2B0 (157 cfs) which contains the flow from its respective subbasin, design point CP1 (166 cfs) which includes subbasin C1G2B0 routed & combined with subbasin C1G2B4, design point CP2 (204 cfs) which includes subbasin C1G2B0, & C1G2B4 routed & combined with subbasin C1G2B3, and finally CP7C (602 cfs) which includes design point CP2 & subbasins C1G2B5, C1G2B1, C1G2B2 & C1G2A.

3.0 HYDRAULICS

Pre-Project Conditions – HEC-RAS

Pre-Project conditions analysis was modeled using HEC-RAS, which determined flood zone conditions before Mission Drive Improvements. Design flows that was used for modeling was taken from Mission Drive Pre-Development Conditions, HEC-1 run that was modeled after the C1 Channel FIS Hydrology Study. Cross sections that was used were based on 2-foot contours & grading plans, that were cut at 100-foot stations for analysis purposes. See Appendix D for Pre-Project HEC-RAS input & output conditions.

Post-Project Conditions – WSPG

Hydraulic modeling for Mission Drive was calculated using WSPG, in conformance with local standards as CCRFCD Hydrologic Criteria & Drainage Design Manual. The WSPG model input & output that was used, was taken from Mission Drive/Greenway Road Improvements; Final Drainage Report, February 2004, submitted by VTN Nevada which can be found in Appendix D, where 606 cfs was used in designing the storm drain facilities on Greenway Road. The flow cut-off in the Post-Project conditions that is used for this LOMR is only 224 cfs. Storm Drain Plan & Profiles from Mission Drive/Greenway Road Improvements can also be found in Appendix D.

Post-development Conditions – HEC-RAS

Post development conditions analysis was modeled using HEC-RAS, which determined that supercritical flow is maintained within the specified project length. Design flows that was used for modeling was derived from C1 Channel FIS Hydrology Study, but was modified to meet Post-Development Conditions. Cross sections that was used were based on 2-foot contours & grading plans, that were cut at 200-foot stations for analysis purposes. See Appendix D for Post-Development HEC-RAS input & output conditions.

4.0 RESULTS

Mission Drive LOMR HEC-RAS Results Plan: 022606

Post-Project

River Sta.	Cross Section Sta.	Q Total (cfs)	W.S. Elev (ft)	Hydr Depth (ft)
48	0+100	157	2383.5	0.91
46	0+300	157	2375.17	0.74
44	0+500	157	2363.31	0.74
42	0+700	157	2355.5	1.01*
40	0+900	157	2351.26	0.89
37	1+200	157	2344.78	1.1*
36	1+300	157	2341.02	0.95
34	1+500	157	2336.62	0.56
32	1+700	157	2330.63	0.57
30	1+900	157	2325.52	0.76
28	2+100	157	2320.99	0.76
26	2+300	166	2314.76	0.82
24	2+500	166	2308.93	0.82
22	2+700	166	2304.34	0.73
20	2+900	166	2298.67	0.54
19	3+000	204	2292.39	0.4
18	3+100	204	2287.56	1.07*
17	Culvert	Culvert		
16	3+300	204	2284.64	1.11*
15	3+400	204	2281.07	0.61
14	3+500	204	2277.39	1.03*
12	3+700	602	2267.97	1.38*
10	3+900	602	2266.85	1.03*
8	4+100	602	2263.19	1.1*
6	4+300	602	2259.8	1.03*
4	4+500	602	2256.24	1.92*
2	4+700	602	2255.94	2.18*
1	4+729	602	2255.07	1.58*

*Note: Stations with Hydraulic Depth > 1'

5.0 CONCLUSION

Based on the data and calculations shows that the existing FEMA FIRM Panel 2615 dated, September 27, 2002 needs to be revised to meet current effective flood zone delineations. See Figure 2.3, Appendix A to view the annotated FEMA flood zone map. Figure 2.5, shows the proposed revision to the existing flood zone delineations.

6.0 REFERENCES

1. Clark County Regional Flood Control District, *Hydraulic Criteria and Drainage Design manual*, August 1999.
2. Clark County Regional Flood Control District, *Flood Control Master Plan Update of the Las Vegas Valley*, 2002. – by PBS&J, G.C. Wallace, and Louis Berger Group
3. Flood Hydrograph Package (HEC-1) User Manual, Sept 1990
4. Water Surface and Pressure Gradient Hydraulic Analysis System (WSPG) User Manual, Apr 1979
5. Drainage Study of Paradise Hills Development, Pentacore, 1995 – 2000
6. Mission Drive/Greenway Road : Roadway Improvements / Final Drainage Report, VTN Nevada, Feb 2004
7. C-1 Channel System Flood Insurance Restudy, Carter & Burgess & Southwest Fluvial System, Nov 2002

APPENDIX A

FEMA FORMS

FEMA ‘OVERVIEW & CONCURRENCE FORM’
– MT-2 FORM 1

FEDERAL EMERGENCY MANAGEMENT AGENCY
OVERVIEW & CONCURRENCE FORM

O.M.B No. 3067-0148
Expires September 30, 2005

PAPERWORK BURDEN DISCLOSURE NOTICE

Public reporting burden for this form is estimated to average 1 hour per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. You are not required to respond to this collection of information unless a valid OMB control number appears in the upper right corner of this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Federal Emergency Management Agency, 500 C Street, SW, Washington DC 20472, Paperwork Reduction Project (3067-0148). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. **Please do not send your completed survey to the above address.**

A. REQUESTED RESPONSE FROM FEMA

This request is for a (check one):

- ☐ CLOMR: A letter from FEMA commenting on whether a proposed project, if built as proposed, would justify a map revision, or proposed hydrology changes (See 44 CFR Ch. 1, Parts 60, 65 & 72).
- ☒ LOMR: A letter from FEMA officially revising the current NFIP map to show the changes to floodplains, regulatory floodway or flood elevations. (See Parts 60 & 65 of the NFIP Regulations.)

B. OVERVIEW

1. The NFIP map panel(s) affected for all impacted communities is (are):

Community No.	Community Name	State	Map No.	Panel No.	Effective Date
Ex: 480301	City of Katy	TX	480301	0005D	02/08/83
480287	Harris County	TX	48201C	0220G	09/28/90
320005	CITY OF HENDERSON CLARK COUNTY, UNINCORPORATED AREAS	NV	32003C	2955E	11/06/03
320003	CITY OF HENDERSON CLARK COUNTY				

2. Flooding Source: C1 CHANNEL / C1 DETENTION BASIN

3. Project Name/Identifier: MISSION DRIVE

4. FEMA zone designations affected: A, X (choices: A, AH, AO, A1-A30, A99, AE, AR, V, V1-V30, VE, B, C, D, X)

5. Basis for Request and Type of Revision:

a. The basis for this revision request is (check all that apply)

- ☒ Physical Change ☒ Improved Methodology/Data
- ☐ Regulatory Floodway Revision ☐ Other (Attach Description)

Note: A photograph and narrative description of the area of concern is not required, but is very helpful during review.

b. The area of revision encompasses the following types of flooding and structures (check all that apply)

- Types of Flooding: ☒ Riverine ☐ Coastal ☐ Shallow Flooding (e.g., Zones AO and AH)
- ☐ Alluvial fan ☐ Lakes ☐ Other (Attach Description)
- Structures: ☒ Channelization ☐ Levee/Floodwall ☐ Bridge/Culvert
- ☐ Dam ☐ Fill ☐ Other, Attach Description

C. REVIEW FEE

Has the review fee for the appropriate request category been included?

☒ Yes

Fee amount: \$4,400

☐ No, Attach Explanation

Please see the FEMA Web site at http://www.fema.gov/fhm/frm_fees.shtml for Fee Amounts and Exemptions.

D. SIGNATURE

All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001.

Name: Jeremy Leavitt, P.E.

Company: VTN Nevada

Mailing Address:
2727 S. Rainbow Blvd.
Las Vegas, Nevada
89146

Daytime Telephone No.:
702 253-2359

Fax No.:
702 247-4262

E-Mail Address: jeremyl@vtnnv.com

Signature of Requester (required):

Date: 02/27/06

As the community official responsible for floodplain management, I hereby acknowledge that we have received and reviewed this Letter of Map Revision (LOMR) or conditional LOMR request. Based upon the community's review, we find the completed or proposed project meets or is designed to meet all of the community floodplain management requirements, including the requirement that no fill be placed in the regulatory floodway, and that all necessary Federal, State, and local permits have been, or in the case of a conditional LOMR, will be obtained. In addition, we have determined that the land and any existing or proposed structures to be removed from the SFHA are or will be reasonably safe from flooding as defined in 44CFR 65.2(c), and that we have available upon request by FEMA, all analyses and documentation used to make this determination.

Community Official's Name and Title: JOSEPH DAMIANI, P.E. PROJECT MANAGER

Telephone No.:
702 267-3050

Community Name: City of Henderson

Community Official's Signature (required):

Date:

Joseph V. Damiani

3-01-2006

CERTIFICATION BY REGISTERED PROFESSIONAL ENGINEER AND/OR LAND SURVEYOR

This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001.

Certifier's Name: Jeremy Leavitt, P.E.

License No.: NV 15536

Expiration Date:
12-31-07

Company Name: VTN Nevada

Telephone No.: 702 253-2359

Fax No.:
702 247-4262

Signature:

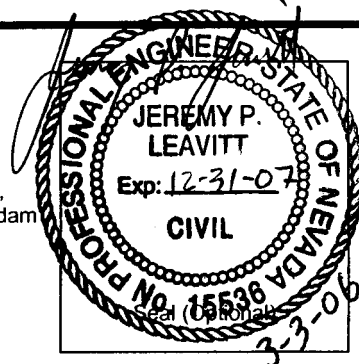
Date: 02/27/06

Ensure the forms that are appropriate to your revision request are included in your submittal.

Form Name and (Number)

Required if ...

- | | |
|---|---|
| ☒ Riverine Hydrology and Hydraulics Form (Form 2) | New or revised discharges or water-surface elevations |
| ☒ Riverine Structures Form (Form 3) | Channel is modified, addition/revision of bridge/culverts, addition/revision of levee/floodwall, addition/revision of dam |
| ☐ Coastal Analysis Form (Form 4) | New or revised coastal elevations |
| ☐ Coastal Structures Form (Form 5) | Addition/revision of coastal structure |
| ☐ Alluvial Fan Flooding Form (Form 6) | Flood control measures on alluvial fans |



FEMA ‘RIVERINE HYDROLOGY & HYDRAULICS FORM’
– MT-2 FORM 2

FEDERAL EMERGENCY MANAGEMENT AGENCY
RIVERINE HYDROLOGY & HYDRAULICS FORM

*O.M.B No. 3067-0148
Expires September 30, 2005*

PAPERWORK REDUCTION ACT

Public reporting burden for this form is estimated to average 3 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. You are not required to respond to this collection of information unless a valid OMB control number appears in the upper right corner of this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Federal Emergency Management Agency, 500 C Street, SW, Washington DC 20472, Paperwork Reduction Project (3067-0148). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. **Please do not send your completed survey to the above address.**

Flooding Source: C-1 WATERSHED
Note: Fill out one form for each flooding source studied

A. HYDROLOGY

1. Reason for New Hydrologic Analysis (check all that apply)

- | | | |
|--|--|---|
| ☐ Not revised (skip to section 2) | ☐ No existing analysis | ☒ Improved data |
| ☐ Alternative methodology | ☐ Proposed Conditions (CLOMR) | ☒ Changed physical condition of watershed |

2. Comparison of Representative 1%-Annual-Chance Discharges

Location	Drainage Area (Sq. Mi.)	FIS (cfs)	Revised (cfs)
MISSION GREENWAY	1.15	799	602
FLOOD ZONE A			

3. Methodology for New Hydrologic Analysis (check all that apply)

- | | |
|---|---|
| ☐ Statistical Analysis of Gage Records | ☒ Precipitation/Runoff Model [TR-20, HEC-1, HEC-HMS etc.] |
| ☐ Regional Regression Equations | ☐ Other (please attach description) |

Please enclose all relevant models in digital format, maps, computations (including computation of parameters) and documentation to support the new analysis. The document, "Numerical Models Accepted by FEMA for NFIP Usage" lists the models accepted by FEMA. This document can be found at: http://www.fema.gov/fhm/en_modl.shtml.

4. Review/Approval of Analysis

If your community requires a regional, state, or federal agency to review the hydrologic analysis, please attach evidence of approval/review.

5. Impacts of Sediment Transport on Hydrology

Was sediment transport considered? ☐ Yes ☒ No If yes, then fill out Section F (Sediment Transport) of Form 3. If No, then attach your explanation for why sediment transport was not considered.

B. HYDRAULICS

1. Reach to be Revised

	Description	Cross Section	Water-Surface Elevations (ft.)	
			Effective	Proposed/Revised
Downstream Limit	Existing Wash	3+900	2267.52	2266.85
Upstream Limit	Existing Channel	0+500	2363.42	2363.19

2. Hydraulic Method Used

Hydraulic Analysis HEC RAS & WSPG [HEC-2 , HEC-RAS, Other (Attach description)]

B. HYDRAULICS (CONTINUED)

3. Pre-Submittal Review of Hydraulic Models

FEMA has developed two review programs, CHECK-2 and CHECK-RAS, to aid in the review of HEC-2 and HEC-RAS hydraulic models, respectively. These review programs verify that the hydraulic estimates and assumptions in the model data are in accordance with NFIP requirements, and that the data are comparable with the assumptions and limitations of HEC-2/HEC-RAS. CHECK-2 and CHECK-RAS identify areas of potential error or concern. These tools do not replace engineering judgment. CHECK-2 and CHECK-RAS can be downloaded from http://www.fema.gov/fhm/fhm_soft.shtm. We recommend that you review your HEC-2 and HEC-RAS models with CHECK-2 and CHECK-RAS. If you disagree with a message, please attach an explanation of why the message is not valid in this case. Review of your submittal and resolution of valid modeling discrepancies will result in reduced review time.

HEC-2/HEC-RAS models reviewed with CHECK-2/CHECK-RAS? ☒ Yes ☐ No

4. Models Submitted

Duplicate Effective Model*	Natural File Name: N/A	Floodway File Name:
Corrected Effective Model*	Natural File Name: N/A	Floodway File Name:
Existing or Pre-Project Conditions Model	Natural File Name: SDN3.dat, 022206.prj	Floodway File Name:
Revised or Post-Project Conditions Model	Natural File Name: missiond.dat, 022606 .prj	Floodway File Name:
Other - (attach description)	Natural File Name: VTN3.dat	Floodway File Name:

(WSPG) Mission Drive/Greenway Rd Improvements

*Not required for revisions to approximate 1%-annual-chance floodplains (Zone A) – for details, refer to the corresponding section of the instructions.

The document "Numerical Models Accepted by FEMA for NFIP Usage" lists the models accepted by FEMA. This document can be found at: http://www.fema.gov/fhm/en_modl.shtm.

C. MAPPING REQUIREMENTS

A **certified topographic map** must be submitted showing the following information (where applicable): the boundaries of the effective, existing, and proposed conditions 1%-annual-chance floodplain (for approximate Zone A revisions) or the boundaries of the 1%- and 0.2%-annual-chance floodplains and regulatory floodway (for detailed Zone AE, AO, and AH revisions); location and alignment of all cross sections with stationing control indicated; stream, road, and other alignments (e.g., dams, levees, etc.); current community easements and boundaries; boundaries of the requester's property; certification of a registered professional engineer registered in the subject State; location and description of reference marks; and the referenced vertical datum (NGVD, NAVD, etc.).

Note that the boundaries of the existing or proposed conditions floodplains and regulatory floodway to be shown on the revised FIRM and/or FBFM must tie-in with the effective floodplain and regulatory floodway boundaries. Please attach a **copy of the effective FIRM and/or FBFM**, annotated to show the boundaries of the revised 1%- and 0.2%-annual-chance floodplains and regulatory floodway that tie-in with the boundaries of the effective 1%- and 0.2%-annual-chance floodplain and regulatory floodway at the upstream and downstream limits of the area of revision.

D. COMMON REGULATORY REQUIREMENTS

1. For CLOMR requests, do Base Flood Elevations (BFEs) increase? ☐ Yes ☒ No

For CLOMR requests, if either of the following is true, please submit evidence of compliance with Section 65.12 of the NFIP regulations:

- The proposed project encroaches upon a regulatory floodway and would result in increases above 0.00 foot.
- The proposed project encroaches upon a SFHA with BFEs established and would result in increases above 1.00 foot.

2. Does the request involve the placement or proposed placement of fill? ☐ Yes ☒ No

If Yes, the community must be able to certify that the area to be removed from the special flood hazard area, to include any structures or proposed structures, meets all of the standards of the local floodplain ordinances, and is reasonably safe from flooding in accordance with the NFIP regulations set forth at 44 CFR 60.3(a)(3), 65.5(a)(4), and 65.6(a)(14). Please see the MT-2 instructions for more information.

3. For LOMR requests, is the regulatory floodway being revised? ☐ Yes ☒ No

If Yes, attach evidence of regulatory floodway revision notification. As per Paragraph 65.7(b)(1) of the NFIP Regulations, notification is required for requests involving revisions to the regulatory floodway. (Not required for revisions to approximate 1%-annual-chance floodplains [studied Zone A designation] unless a regulatory floodway is being added. Elements and examples of regulatory floodway revision notification can be found in the MT-2 Form 2 Instructions.)

4. For LOMR requests, does this request require property owner notification and acceptance of BFE increases? ☐ Yes ☒ No

If Yes, please attach proof of property owner notification and acceptance (if available). Elements of and examples of property owner notification can be found in the MT-2 Form 2 Instructions.

FEMA 'HYDRAULIC STRUCTURES FORM'
– MT-2 FORM 3

FEDERAL EMERGENCY MANAGEMENT AGENCY
RIVERINE STRUCTURES FORM

O.M.B. No. 3067-0148
Expires September 30, 2005

PAPERWORK REDUCTION ACT

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Flooding Source: C-1 WATERSHED

Note: Fill out one form for each flooding source studied

A. GENERAL

Complete the appropriate section(s) for each Structure listed below:

Channelization.....complete Section B
Bridge/Culvert.....complete Section C
Damcomplete Section D
Levee/Floodwallcomplete Section E
Sediment Transportcomplete Section F (if required)

Description Of Structure

1. Name of Structure: Mission Drive 7'x4' RCB

Type (check one): ☐ Channelization ☒ Bridge/Culvert ☐ Levee/Floodwall ☐ Dam

Location of Structure: Crossing Mission Drive

Downstream Limit/Cross Section: 3+100

Upstream Limit/Cross Section: 3+300

2. Name of Structure: Mission Drive / Greenway Road Improvements

Type (check one): ☒ Channelization ☐ Bridge/Culvert ☐ Levee/Floodwall ☐ Dam

Location of Structure: Greenway Road

Downstream Limit/Cross Section: 10+00

Upstream Limit/Cross Section: 40+00

3. Name of Structure:

Type (check one) ☐ Channelization ☐ Bridge/Culvert ☐ Levee/Floodwall ☐ Dam

Location of Structure:

Downstream Limit/Cross Section:

Upstream Limit/Cross Section:

NOTE: For more structures, attach additional pages as needed.

B. CHANNELIZATION

Flooding Source: C-1 WATERSHED

Name of Structure: Mission Drive / Greenway Road Improvements

1. Accessory Structures

The channelization includes (check one):

- | | |
|--|--|
| ☐ Levees [Attach Section E (Levee/Floodwall)] | ☐ Drop structures |
| ☐ Superelevated sections | ☐ Transitions in cross sectional geometry |
| ☐ Debris basin/detention basin | ☐ Energy dissipator |
| ☒ Other (Describe): RCB | |

2. Drawing Checklist

Attach the plans of the channelization certified by a registered professional engineer, as described in the instructions.

3. Hydraulic Considerations

The channel was designed to carry 630 (cfs) and/or the 100-year flood.

The design elevation in the channel is based on (check one):

- ☒ Subcritical flow ☐ Critical flow ☐ Supercritical flow ☐ Energy grade line

If there is the potential for a hydraulic jump at the following locations, check all that apply and attach an explanation of how the hydraulic jump is controlled without affecting the stability of the channel.

- ☐ Inlet to channel ☐ Outlet of channel ☐ At Drop Structures ☐ At Transitions
☐ Other locations (specify):

4. Sediment Transport Considerations

Was sediment transport considered? ☐ Yes ☒ No If Yes, then fill out Section F (Sediment Transport).

If No, then attach your explanation for why sediment transport was not considered. N/A

C. BRIDGE/CULVERT

Flooding Source: C-1 WATERSHED

Name of Structure: Mission Drive 7'x4' RCB

1. This revision reflects (check one):

- ☒ New bridge/culvert not modeled in the FIS
☐ Modified bridge/culvert previously modeled in the FIS
☐ New analysis of bridge/culvert previously modeled in the FIS

2. Hydraulic model used to analyze the structure (e.g., HEC-2 with special bridge routine, WSPRO, HY8): HEC-RAS

If different than hydraulic analysis for the flooding source, justify why the hydraulic analysis used for the flooding source could not analyze the structures. Attach justification.

3. Attach plans of the structures certified by a registered professional engineer. The plan detail and information should include the following (check the information that has been provided):

- | | |
|--|---|
| ☒ Dimensions (height, width, span, radius, length) | ☐ Erosion Protection |
| ☒ Shape (culverts only) | ☐ Low Chord Elevations – Upstream and Downstream |
| ☒ Material | ☐ Top of Road Elevations – Upstream and Downstream |
| ☐ Beveling or Rounding | ☒ Structure Invert Elevations – Upstream and Downstream |
| ☒ Wing Wall Angle | ☒ Stream Invert Elevations – Upstream and Downstream |
| ☒ Skew Angle | ☐ Cross-Section Locations |
| ☒ Distances Between Cross Sections | |

4. Sediment Transport Considerations

Was sediment transport considered? ☐ Yes ☒ No If yes, then fill out Section F (Sediment Transport).

If No, then attach your explanation for why sediment transport was not considered. N/A

D. DAM

Flooding Source:

PAGES 3-10 NOT APPLICABLE

Name of Structure:

1. This request is for (check one): ☐ Existing dam ☐ New dam ☐ Modification of existing dam

2. The dam was designed by (check one): ☐ Federal agency ☐ State agency ☐ Local government agency

☐ Private organization Name of the agency or organization:

3. Does the project involve revised hydrology? ☐ Yes ☐ No

If Yes, complete the Riverine Hydrology & Hydraulics Form (Form 2).

4. Does the submittal include debris/sediment yield analysis? ☐ Yes ☐ No

If yes, then fill out Section F (Sediment Transport).

If No, then attach your explanation for why debris/sediment analysis was not considered.

5. Does the Base Flood Elevation behind the dam or downstream of the dam change?

☐ Yes ☐ No If Yes, complete the Riverine Hydrology & Hydraulics Form (Form 2) and complete the table below.

Stillwater Elevation Behind the Dam

FREQUENCY (% annual chance)

FIS

REVISED

10-year (10%)

50-year (2%)

100-year (1%)

500-year (0.2%)

Normal Pool Elevation

6. Please attach a copy of the formal Operation and Maintenance Plan

E. LEVEE/FLOODWALL

1. System Elements

a. This Levee/Floodwall analysis is based on (check one):

- ☐ upgrading of an existing levee/floodwall system
☐ a newly constructed levee/floodwall system
☐ reanalysis of an existing levee/floodwall system

b. Levee elements and locations are (check one):

- ☐ earthen embankment, dike, berm, etc. Station to
☐ structural floodwall Station to
☐ Other (describe): Station to

c. Structural Type (check one):

- ☐ monolithic cast-in place reinforced concrete
☐ reinforced concrete masonry block
☐ sheet piling
☐ Other (describe):

d. Has this levee/floodwall system been certified by a Federal agency to provide protection from the base flood?

☐ Yes ☐ No

If Yes, by which agency?

e. Attach certified drawings containing the following information (indicate drawing sheet numbers):

- | | |
|--|----------------|
| 1. Plan of the levee embankment and floodwall structures. | Sheet Numbers: |
| 2. A profile of the levee/floodwall system showing the Base Flood Elevation (BFE), levee and/or wall crest and foundation, and closure locations for the total levee system. | Sheet Numbers: |
| 3. A profile of the BFE, closure opening outlet and inlet invert elevations, type and size of opening, and kind of closure. | Sheet Numbers: |
| 4. A layout detail for the embankment protection measures. | Sheet Numbers: |
| 5. Location, layout, and size and shape of the levee embankment features, foundation treatment, floodwall structure, closure structures, and pump stations. | Sheet Numbers: |

2. Freeboard

a. The minimum freeboard provided above the BFE is:

Riverine

- 3.0 feet or more at the downstream end and throughout
3.5 feet or more at the upstream end
4.0 feet within 100 feet upstream of all structures and/or constrictions

☐ Yes ☐ No
☐ Yes ☐ No
☐ Yes ☐ No

Coastal

1.0 foot above the height of the one percent wave associated with the 1%-annual-chance stillwater surge elevation or maximum wave runup (whichever is greater).

☐ Yes ☐ No

2.0 feet above the 1%-annual-chance stillwater surge elevation

☐ Yes ☐ No

E. LEVEE/FLOODWALL (CONTINUED)

2. Freeboard (continued)

Please note, occasionally exceptions are made to the minimum freeboard requirement. If an exception is requested, attach documentation addressing Paragraph 65.10(b)(1)(ii) of the NFIP Regulations.

If No is answered to any of the above, please attach an explanation.

- b. Is there an indication from historical records that ice-jamming can affect the BFE? ☐ Yes ☐ No

If Yes, provide ice-jam analysis profile and evidence that the minimum freeboard discussed above still exists.

3. Closures

- a. Openings through the levee system (check one): ☐ exists ☐ does not exist

If opening exists, list all closures:

Channel Station	Left or Right Bank	Opening Type	Highest Elevation for Opening Invert	Type of Closure Device

(Extend table on an added sheet as needed and reference)

Note: Geotechnical and geologic data

In addition to the required detailed analysis reports, data obtained during field and laboratory investigations and used in the design analysis for the following system features should be submitted in a tabulated summary form. (Reference U.S. Army Corps of Engineers [USACE] EM-1110-2-1906 Form 2086.)

4. Embankment Protection

- a. The maximum levee slope landside is:
- b. The maximum levee slope floodside is:
- c. The range of velocities along the levee during the base flood is: (min.) to (max.)
- d. Embankment material is protected by (describe what kind):
- e. Riprap Design Parameters (check one): ☐ Velocity ☐ Tractive stress
Attach references

Reach	Sideslope	Flow Depth	Velocity	Curve or Straight	Stone Riprap			Depth of Toedown
					D ₁₀₀	D ₅₀	Thickness	
Sta to								
Sta to								
Sta to								
Sta to								
Sta to								
Sta to								

(Extend table on an added sheet as needed and reference each entry)

E. LEVEE/FLOODWALL (CONTINUED)

4. Embankment Protection (continued)

- f. Is a bedding/filter analysis and design attached? ☐ Yes ☐ No
- g. Describe the analysis used for other kinds of protection used (include copies of the design analysis):

Attach engineering analysis to support construction plans.

5. Embankment And Foundation Stability

- a. Identify locations and describe the basis for selection of critical location for analysis:

☐ Overall height: Sta. ; height ft.

☐ Limiting foundation soil strength:

Sta. , depth to

strength ϕ = degrees, c = psf

slope: SS = (h) to (v)

(Repeat as needed on an added sheet for additional locations)

- b. Specify the embankment stability analysis methodology used (e.g., circular arc, sliding block, infinite slope, etc.):

- c. Summary of stability analysis results:

Case	Loading Conditions	Critical Safety Factor	Criteria (Min.)
I	End of construction		1.3
II	Sudden drawdown		1.0
III	Critical flood stage		1.4
IV	Steady seepage at flood stage		1.4
VI	Earthquake (Case I)		1.0

(Reference: USACE EM-1110-2-1913 Table 6-1)

- d. Was a seepage analysis for the embankment performed? ☐ Yes ☐ No

If Yes, describe methodology used:

- e. Was a seepage analysis for the foundation performed? ☐ Yes ☐ No

- f. Were uplift pressures at the embankment landside toe checked? ☐ Yes ☒ No

- g. Were seepage exit gradients checked for piping potential? ☐ Yes ☐ No

- h. The duration of the base flood hydrograph against the embankment is hours.

Attach engineering analysis to support construction plans.

E. LEVEE/FLOODWALL (CONTINUED)

6. Floodwall And Foundation Stability

a. Describe analysis submittal based on Code (check one):

☐ UBC (1988) or ☐ Other (specify):

b. Stability analysis submitted provides for:

☐ Overturning ☐ Sliding If not, explain:

c. Loading included in the analyses were:

☐ Lateral earth @ $P_A =$ psf; $P_p =$ psf

☐ Surcharge-Slope @ , ☐ surface psf

☐ Wind @ $P_w =$ psf

☐ Seepage (Uplift); ☐ Earthquake @ $P_{eq} =$ %g

☐ 1%-annual-chance significant wave height: ft.

☐ 1%-annual-chance significant wave period: sec.

d. Summary of Stability Analysis Results: Factors of Safety.

Itemize for each range in site layout dimension and loading condition limitation for each respective reach.

Loading Condition	Criteria (Min)		Sta	To	Sta	To
	Overturn	Sliding	Overturn	Sliding	Overturn	Sliding
Dead & Wind	1.5	1.5				
Dead & Soil	1.5	1.5				
Dead, Soil, Flood, & Impact	1.5	1.5				
Dead, Soil, & Seismic	1.3	1.3				

(Ref: FEMA 114 Sept 1986; USACE EM 1110-2-2502)

(Note: Extend table on an added sheet as needed and reference)

e. Foundation bearing strength for each soil type:

Bearing Pressure	Sustained Load (psf)	Short Term Load (psf)
Computed design maximum		
Maximum allowable		

f. Foundation scour protection ☐ is, ☐ is not provided. If provided, attach explanation and supporting documentation:

Attach engineering analysis to support construction plans.

E. LEVEE/FLOODWALL (CONTINUED)

7. Settlement

- a. Has anticipated potential settlement been determined and incorporated into the specified construction elevations to maintain the established freeboard margin? ☐ Yes ☐ No
- b. The computed range of settlement is ft. to ft.
- c. Settlement of the levee crest is determined to be primarily from :
- ☐ Foundation consolidation
- ☐ Embankment compression
- ☐ Other (Describe):
- d. Differential settlement of floodwalls ☐ has ☐ has not been accommodated in the structural design and construction.
- Attach engineering analysis to support construction plans.

8. Interior Drainage

- a. Specify size of each interior watershed:
- Draining to pressure conduit: acres
- Draining to ponding area: acres
- b. Relationships Established
- Ponding elevation vs. storage ☐ Yes ☐ No
- Ponding elevation vs. gravity flow ☐ Yes ☐ No
- Differential head vs. gravity flow ☐ Yes ☐ No
- c. The river flow duration curve is enclosed: ☐ Yes ☐ No
- d. Specify the discharge capacity of the head pressure conduit: cfs
- e. Which flooding conditions were analyzed?
- | | | |
|-------------------------------------|------------------------------|-----------------------------|
| • Gravity flow (Interior Watershed) | ☐ Yes | ☐ No |
| • Common storm (River Watershed) | ☐ Yes | ☐ No |
| • Historical ponding probability | ☐ Yes | ☐ No |
| • Coastal wave overtopping | ☐ Yes | ☐ No |
- If No for any of the above, attach explanation.
- f. Interior drainage has been analyzed based on joint probability of interior and exterior flooding and the capacities of pumping and outlet facilities to provide the established level of flood protection. ☐ Yes ☐ No
- If No, attach explanation.
- g. The rate of seepage through the levee system for the base flood is cfs
- h. The length of levee system used to drive this seepage rate in item g: ft.

E. LEVEE/FLOODWALL (CONTINUED)

8. Interior Drainage (continued)

- i. Will pumping plants be used for interior drainage?

☐ Yes ☐ No

If Yes, include the number of pumping plants:
For each pumping plant, list:

	Plant #1	Plant #2
The number of pumps		
The ponding storage capacity		
The maximum pumping rate		
The maximum pumping head		
The pumping starting elevation		
The pumping stopping elevation		
Is the discharge facility protected?		
Is there a flood warning plan?		
How much time is available between warning and flooding?		

Will the operation be automatic?

☐ Yes ☐ No

If the pumps are electric, are there backup power sources?

☐ Yes ☐ No

(Reference: USACE EM-1110-2-3101, 3102, 3103, 3104, and 3105)

Include a copy of supporting documentation of data and analysis. Provide a map showing the flooded area and maximum ponding elevations for all interior watersheds that result in flooding.

9. Other Design Criteria

- a. The following items have been addressed as stated:

Liquefaction ☐ is ☐ is not a problem

Hydrocompaction ☐ is ☐ is not a problem

Heave differential movement due to soils of high shrink/swell ☐ is ☐ is not a problem

- b. For each of these problems, state the basic facts and corrective action taken:

Attach supporting documentation

- c. If the levee/floodwall is new or enlarged, will the structure adversely impact flood levels and/or flow velocities floodside of the structure?
☐ Yes ☐ No

Attach supporting documentation

- d. Sediment Transport Considerations:

Was sediment transport considered? ☐ Yes ☐ No If Yes, then fill out Section F (Sediment Transport).

If No, then attach your explanation for why sediment transport was not considered.

E. LEVEE/FLOODWALL (CONTINUED)

10. Operational Plan And Criteria

- a. Are the planned/installed works in full compliance with Part 65.10 of the NFIP Regulations? ☐ Yes ☐ No
- b. Does the operation plan incorporate all the provisions for closure devices as required in Paragraph 65.10(c)(1) of the NFIP regulations?
☐ Yes ☐ No
- c. Does the operation plan incorporate all the provisions for interior drainage as required in Paragraph 65.10(c)(2) of the NFIP regulations?
☐ Yes ☐ No

If the answer is No to any of the above, please attach supporting documentation.

11. Maintenance Plan

- a. Are the planned/installed works in full compliance with Part 65.10 of the NFIP Regulations? ☐ Yes ☐ No
If No, please attach supporting documentation.

12. Operations and Maintenance Plan

Please attach a copy of the formal Operations and Maintenance Plan for the levee/floodwall.

F. SEDIMENT TRANSPORT

Flooding Source:

Name of Structure:

If there is any indication from historical records that sediment transport (including scour and deposition) can affect the Base Flood Elevation (BFE); and/or based on the stream morphology, vegetative cover, development of the watershed and bank conditions, there is a potential for debris and sediment transport (including scour and deposition) to affect the BFEs, then provide the following information along with the supporting documentation:

Sediment load associated with the base flood discharge: Volume acre-feet

Debris load associated with the base flood discharge: Volume acre-feet

Sediment transport rate (percent concentration by volume)

Method used to estimate sediment transport:

Most sediment transport formulas are intended for a range of hydraulic conditions and sediment sizes; attach a detailed explanation for using the selected method.

Method used to estimate scour and/or deposition:

Method used to revise hydraulic or hydrologic analysis (model) to account for sediment transport:

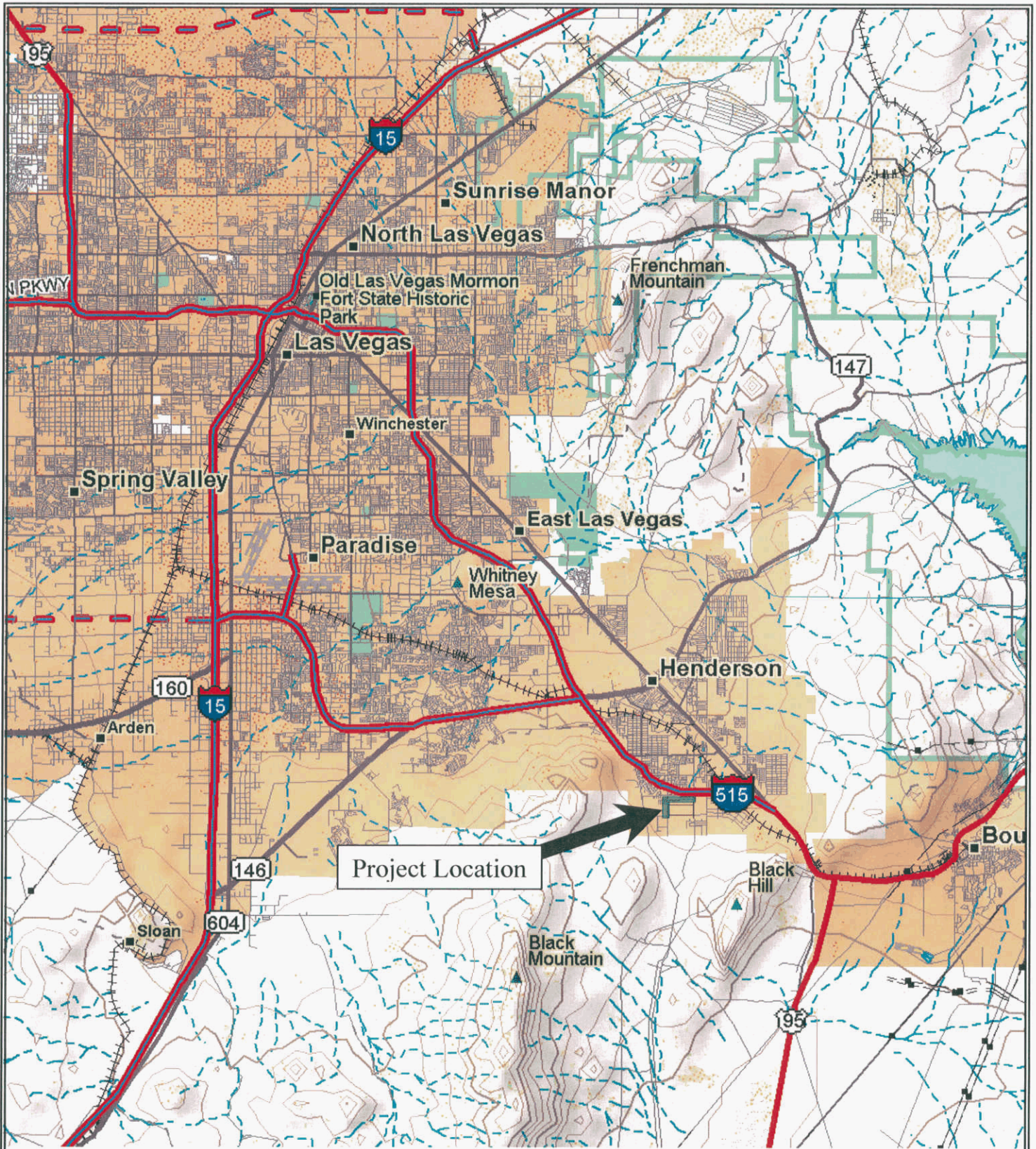
Please note that bulked flows are used to evaluate the performance of a structure during the base flood; however, FEMA does not map BFEs based on bulked flows.

If a sediment analysis has not been performed, an explanation as to why sediment transport (including scour and deposition) will not affect the BFEs or structures must be provided.

APPENDIX B

FIGURES

**MISSION DRIVE
AREA / VICINITY MAP**
-FIGURE 1.0



Vicinity Map
Mission Drive/Greenway Road –
Roadway Improvements

Figure 1

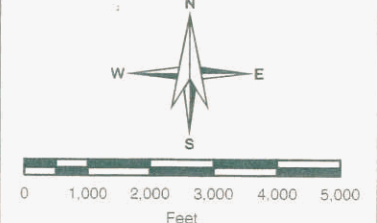
CCRFCD FLOOD CONTROL FACILITIES MAP
- FIGURE F-26



2002 LAS VEGAS VALLEY FLOOD CONTROL MASTER PLAN UPDATE

LEGEND

- Ultimate Development Boundary
- Existing Facilities
- Category A Proposed Facilities
- Category B Proposed Facilities
- Local Existing Facilities
- Local Proposed Facilities
- Detention Basin
- Culvert
- Bridge
- Pipeline
- Lined Channel
- Unlined Channel
- Dike
- Natural Wash
- ID-Mile Separator



SCALE: 1 inch = 3000 feet

1	2	3	4	5	6
7	8	9	10	11	12
13	14	15	16	17	18
19	20	21	22	23	24
25	26	27	28	29	30

FLOOD CONTROL FACILITIES
FIGURE F-26

ID / River Mile	Status	Facility Description	Length (ft.)	Flow (cfs)	HEC-1 Node	HEC-1 Model	Tributary Area (sq.mi.)	Channel Slope (%) **
C1BH		C-1 CHANNEL - BOULDER HWY						
0000	P1	Conc Chnl 30"W 6"D 2:1 SS	2140	3224	CP22	C1SDN3	3.19	1.00
0040	P1	3: 15' X 6' RCBC @ Horizon Dr	100	3194	CP21	C1SDN3	3.11	1.00
0042	P1	Conc Chnl 30"W 6"D 2:1 SS	1525	3194	CP21	C1SDN3	3.11	1.00
0071	E	10' X 4' RCBC @ Equestrian Dr	100	2842	CP20	C1SDN3	2.77	1.00
0071	P1	3: 14' X 6' RCBC @ Equestrian Dr	100	2842	CP20	C1SDN3	2.77	1.00
0073	P1	Conc Chnl 30"W 6"D 2:1 SS	2000	2842	CP20	C1SDN3	2.77	0.80
0111	P1	Conc Chnl 20"W 6"D 2:1 SS	1960	1937	CP17	C1SDN3	1.53	0.80
0148	E	5: 8' X 4' RCBC @ Robert Way	120	1832	CP16	C1SDN3	1.42	1.00
0150	E	Earth Chnl 80'-90"W 5"D 2:1 SS with Drop Structures	1745	1832	CP16	C1SDN3	1.42	1.30
0150	P0	Conc Chnl 40"W 4"D 2:1 SS	1745	1832	CP16	C1SDN3	1.42	1.30
0184	E	Rip Rap Chnl 30"W 4"D 2:1 SS	545	1368	CP15	C1SDN3	1.09	1.30
0184	P0	Conc Chnl 30"W 4"D 2:1 SS	545	1368	CP15	C1SDN3	1.09	1.30
0194	E	3: 8' X 4' RCBC	125	1368	CP15	C1SDN3	1.09	1.00
0196	E	Rip Rap Chnl 30"W 4"D 2:1 SS	250	1368	CP15	C1SDN3	1.09	1.00
0196	P0	Conc Chnl 30"W 4"D 2:1 SS	250	1368	CP15	C1SDN3	1.09	1.00
0201	E	3: 8' X 4' RCBC	265	1368	CP15	C1SDN3	1.09	1.00
0206	E	Rip Rap Chnl 30"W 4"D 2:1 SS	425	1368	CP15	C1SDN3	1.09	1.00
0206	P0	Conc Chnl 30"W 4"D 2:1 SS	425	1368	CP15	C1SDN3	1.09	1.00
0214	E	3: 8' X 4' RCBC @ Conestoga Way	100	1368	CP15	C1SDN3	1.09	1.00
0216	P0	Conc Chnl 25"W 4"D 2:1 SS	1800	1368	CP15	C1SDN3	1.09	1.80
0250	P0	16' X 6' RCBC @ UPRR	50	803	C1-16	C1SDN3	0.52	0.50
0251	P0	Conc Chnl 10"W 5"D 2:1 SS	100	803	C1-16	C1SDN3	0.52	1.00
0253	P0	16' X 6' RCBC @ Dawson Ave	100	803	C1-16	C1SDN3	0.52	0.50
0255	P0	Conc Chnl 10"W 5"D 2:1 SS	2380	803	C1-16	C1SDN3	0.52	1.00
0300	P0	16' X 6' RCBC @ Foothills Dr	110	803	C1-16	C1SDN3	0.52	0.50
0302	P0	Conc Chnl 10"W 5"D 2:1 SS	1090	803	C1-16	C1SDN3	0.52	1.00
C1CH		C-1 CHANNEL						
0561	P3	Conc Chnl 20"W 6"D 0:1 SS	1801	1765	CP14	C1SDN3	2.08	2.00
0600	E	3: 10' X 7' RCBC @ Horizon Dr	436	1765	CP14	C1SDN3	2.08	1.20
0603	P3	Conc Chnl 30"W 6"D 0:1 SS	520	1765	CP14	C1SDN3	2.08	5.34
0604	E	Bridge 36"W 8.5"D @ UPRR	50	1765	CP14	C1SDN3	2.08	1.00
0613	P3	Conc Chnl 12.5"W 6"D 2:1 SS	1470	1765	CP14	C1SDN3	2.08	2.40
0641	P3	Conc Chnl 12.5"W 5"D 2:1 SS	1645	1641	CP13	C1SDN3	1.84	2.70
0672	E	4: 10' X 5' RCBC @ Vermillion Dr	115	1641	CP13	C1SDN3	1.84	0.50
0674	E	Conc Chnl 25"W 6"D 2:1 SS	630	1641	CP13	C1SDN3	1.84	0.70
0686	E	NDOT Sediment Basin		1239	CP12	C1SDN3	1.43	
0711	E	2: 10' X 10' RCBC @ US95	378	1239	CP12	C1SDN3	1.43	0.50
0718	E	NDOT Sediment Basin		1239	CP12	C1SDN3	1.43	
0742	E	10' X 8' RCBC @ Mission Dr	125	425	CP9	C1SDN4B	9.75	1.80
0744	E	Conc Chnl 14"W 8"D 0:1 SS	295	300	DB2	C1SDN4B	9.33	1.80
0750	E	Conc Chnl 14"W 4.5"D 0:1 SS	360	300	DB2	C1SDN4B	9.33	5.90
0757	E	84" RCP Outlet	5070	300	DB2	C1SDN4B	9.33	0.90
0853	E	20,000 cfs PMF Spillway		20000	CP8	C1SDN4B	9.33	
0854	E	402 ac-ft Mission Hills Detention Basin		3467	CP8	C1SDN4B	9.33	
0871	E	12' X 12' RCB	1830	2140	CP5	C1SDN3B	2.22	1.30
0882	E	Rip Rap Levee 10'	7000	1425	CP7	C1SDN3B	6.27	2.40
0905	E	12' X 10' RCB	1312	1779	CP4	C1SDN3B	5.22	1.10
0930	E	12' X 8' RCB	2207	1621	CP3	C1SDN3B	5.09	1.00
0972	E	8' X 8' RCB	2122	943	CP2	C1SDN3B	4.50	1.50
1012	E	54" RCP Outlet	4300	199	DB1	C1SDN3B	3.77	1.50
1094	E	21,600 cfs PMF Spillway		21600	C1-1	C1SDN3B	3.77	
1095	E	366 ac-ft Black Mountain Detention Basin		2709	C1-1	C1SDN3B	3.77	
1110	E	Soil Cement Levee 4'	1100	2709	C1-1	C1SDN3B	3.77	3.00
1138	E	Soil Cement Levee 4'	700	2709	C1-1	C1SDN3B	3.77	3.00

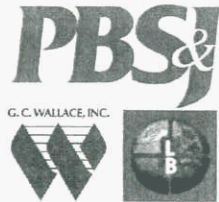
ID / River Mile	Status	Facility Description	Length (ft.)	Flow (cfs)	HEC-1 Node	HEC-1 Model	Tributary Area (sq.mi.)	Channel Slope (%) **
C1E1		C-1 CHANNEL - EQUESTRIAN TRIBUTARY						
0000	P1	Energy Dissipator	50	688	CP30	C1SDN3B	1.21	
0002	P1	Conc Chnl 10"W 4.5"D 2:1 SS	2200	688	CP30	C1SDN3B	1.21	1.40
C1EQ		C-1 CHANNEL - EQUESTRIAN D.B. OUTFALL						
0158	E	39,100 cfs PMF Spillway		39100	CP44	C1SDN3B	7.06	
0159	E	409 ac-ft Equestrian Detention Basin		5196	CP44	C1SDN3B	7.06	
0202	E	Conc Chnl 20"W 8.0"D 2:1 SS	5000	3115	CP38	C1SDN3B	4.35	2.40
0297	E	Rip Rap Levee 10'	9000	3115	CP38	C1SDN3B	3.49	2.00
C1U1		C-1 CHANNEL - US 95 TRIBUTARY 1						
0000	P1	72" RCP	2950	404	C1-10	C1SDN3	0.41	2.00
0056	E	66" RCP	318	404	C1-10	C1SDN3	0.41	0.90
0062	E	60" RCP	742	404	C1-10	C1SDN3	0.41	2.10
C1US		C-1 CHANNEL - US95						
0000	E	4: 10' X 6' RCBC @ College Dr	171	900	CP11	C1SDN3	1.01	0.50
0003	E	Earth Chnl 30'-100"W 5"D 2:1 SS	3225	900	CP11	C1SDN3	1.01	2.10
0003	P1	Conc Chnl 20"W 4"D 2:1 SS	3225	900	CP11	C1SDN3	1.01	2.10
0064	E	Conc Chnl 18"W 6"D 2:1 SS	590	189	C1-11	C1SDN3	0.23	0.70
0075	E	4: 8' X 5' RCBC @ Greenway Road	140	189	C1-11	C1SDN3	0.23	0.40
0078	E	Conc Chnl 11.5"W 6"D 2:1 SS	1900	189	C1-11	C1SDN3	0.23	2.70
PTGL		PITTMAN GAS LINE						
0000	E	72" RCP	1675	678	CPPD030	PIT3SC	0.69	3.40
PTHR		PITTMAN HORIZON RIDGE						
0140	P1	Conc Chnl 15"W 4"D 2:1 SS	3425	1065	CPPD135	PIT3SC	0.89	4.00
0203	P1	84" RCP Outlet	200	882	CPPD125	PIT3SC	0.72	4.00
0204	P1	882 cfs Spillway		882	CPPD125	PIT3SC	0.72	
0205	P1	2.5 ac-ft Pittman Horizon Ridge Debris Basin		882	CPPD125	PIT3SC	0.72	
0210	E	Natural Wash	2950	882	CPPD125	PIT3SC	0.72	7.00
PTIS		PITTMAN WASH - INTERSTATE						
0102	E	Rip Rap Chnl 35"W 6"D 2:1 SS	3390	2380	CPPD060	PIT3SC	2.36	1.10
0166	E	2: 6' X 6' RCB	950	1365	CPPD045	PIT3SC	1.17	3.50
0184	E	Conc Chnl 9"W 4"D 3:1 SS	750	1962	CPPD050	PIT3SC	1.86	5.00
0197	E	3: 60" RCP @ Horizon Ridge Pkwy	150	681	CPPD030	PIT3SC	0.69	3.00
0198	E	Conc Chnl 10"W 4"D 2:1 SS	3150	681	CPPD030	PIT3SC	0.69	1.30
PTWH		PITTMAN WEST HORIZON						
0000	P1	Conc Chnl 12"W 5"D 2:1 SS	500	1365	CPPD045	PIT3	1.17	4.00
0010	P1	12' X 6' RCBC @ Horizon Dr	50	1365	CPPD045	PIT3	1.17	4.00
0011	P1	Conc Chnl 12"W 5"D 2:1 SS	6300	1365	CPPD045	PIT3	1.17	4.10

*The HEC-1 node shown identifies the controlling concentration point for the associated facility and is located upstream of this facility due to decreasing peak flow with increasing tributary area caused by storm distribution transitions, depth area reduction factors, or attenuation of flow from routing.
**As-built or design slopes were used when available. All other slopes are based on existing topography. The user should verify the facility slope listed prior to performing any facility specific analysis.

REGIONAL FLOOD CONTROL DISTRICT

2002 LAS VEGAS VALLEY
FLOOD CONTROL MASTER PLAN UPDATE
FACILITY INVENTORY
FIGURE F-26

LEGEND	Street Name Designator	AA BB	Existing Facility	E	Bottom Width	W	Construction Features	
	Parent Stream Name		Proposed or Modified Facility	P			Cast in Place Concrete Pipe	CIPCP
	Stream Name		Contingency Level				Corrugated Metal Arch Pipe Culvert	CMAF
	ID / River Mile	00 00	Category B	P0	Depth	D	Corrugated Metal Pipe Culvert	CMP
	Distance above confluence		Master Plan	P1			High Density Polyethylene	HDPE
	With parent stream		Preliminary Design	P2	Side Slope, H:V	SS	Helical Elliptical Reinforced Concrete Pipe	HERCP
	Miles in tenths		Design	P3			Reinforced Concrete Arch Pipe	RCAC
							Reinforced Concrete Box	RCB
							Reinforced Concrete Box Culvert	RCBC
							Reinforced Concrete Pipe	RCP
							Reinforced Concrete Pipe Culvert	RCPC
							Storm Sewer Pipe	SSP



The map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding. Participants from local communities are responsible for determining if additional flood hazard information is available.

To obtain more detailed information in areas where Flood Elevation Data is shown, users are encouraged to consult the Flood Profiles and Floodway Data tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that the FIS contains the final elevation rounded whole-foot elevations. These EFIs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Area Flood Elevation (CAFE) shown on this map may apply only to areas with CLE North American Vertical Datum (NAVD83). Users of this FIRM Summary of Significant Elevations Table may also be provided in the study community. Elevations shown in the Summary of Significant Elevations Table will be referenced in measurements taken at the time of future flood damage assessments if they are higher than the elevations shown on this FIRM.

Boundaries of the Floodways were computed at cross sections and interpolated between cross sections. The Floodways were based on hydraulic considerations and hydrologic data from the National Flood Insurance Program. Floodway widths and other pertinent floodway data are presented in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by levees or dikes. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures in this jurisdiction.

The projection used in the preparation of this map is Universal Transverse Mercator (UTM) zone 11. The horizontal datum is NAD83. GRS1980 ellipsoid was used. All coastal flood profiles are referenced to the mean low water of the production of the FIRM for adjacent Federal District. The information was converted using Datumsurveying software dated 1989 or newer, and GRS1980 datum. Segments were adjusted so of the orthorectification based on corner of pavement.

Composite tables shown on this map are based on the best data available at the time of publication. However, changes in inundation or delineations may have occurred after the map was published, and GIS users should contact appropriate community officials to verify current coastal limit locations.

Potential error to the separately printed Map Index for an overview map of the county showing the location of maps in this series, and digital versions, and a Listing of Communities List concerning National Flood Insurance Program data for each community as well as a listing of the panels on which each community is located.

An accompanying Flood Insurance Study report, Letters of Map Revision or Letters of Map Amendment revising portions of this panel, and digital versions of the PANEL may be available. Contact the FEMA Map Service Center at the following phone numbers and internet address for information on all related products available from FEMA:

Phone: 800-354-3615
FAX: 800-258-9610
www.fema.gov

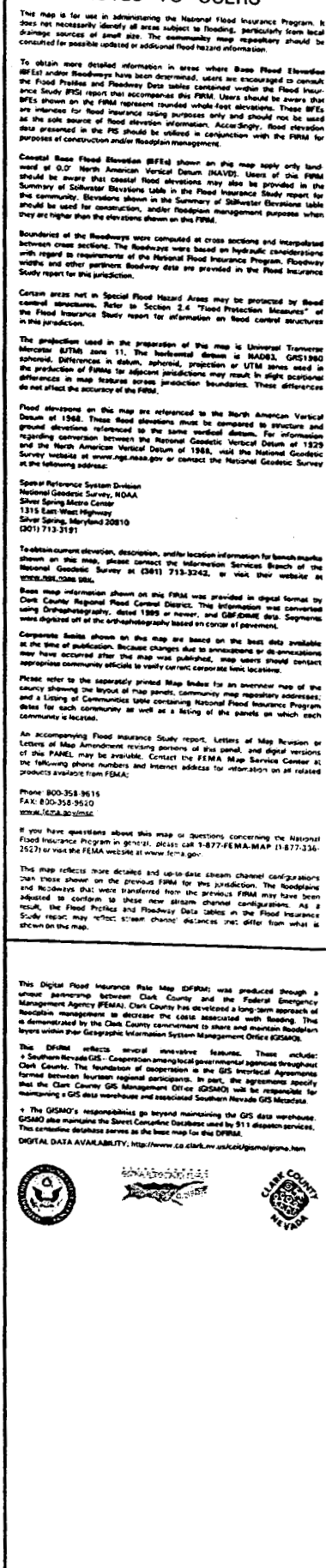
If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA-MAP (1-877-334-2571) visit the FEMA website at www.fema.gov.

This map reflects those decisions and up-to-date stream channel configurations that show shown on the previous FIRM for this jurisdiction. The boundaries and hydrology that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report may reflect stream channel distances that differ from what is indicated on this panel.

This Digital Flood Insurance Data Map (DFIRM) was produced through a Management Agency (FEMA), Clark County and the Federal Emergency response planning team. Clark County has developed a long-term approach of floodplain management to decrease the costs associated with flooding. The DFIRM is demonstrated by the County government to issue and maintain flood reports by their Geographic Information System Management Office (GISMO).

This DFIRM includes several innovative features. Those include:
• A Southern Nevada GIS Consortium among local governmental agencies throughout Clark County. The foundation of cooperation is the GIS Technical Agreement formed between fourteen participating partners. In part, the agreement specifies that the Clark County GIS Management Office (GISMO) will be responsible for maintaining a GIS data warehouse and associated Southern Nevada GIS Metadata.
• The GISMO's responsibility go beyond maintaining the GIS data warehouse. GISMO also maintains the Street/Coverage Database used by 911 dispatch services. This database is the base map for this DFIRM.

DIGITAL DATA AVAILABILITY: <http://www.ccgis.com/clark/gisinfo/gisinfo.htm>

[illegible]

FIRM
FLOOD INSURANCE RATE MAP
CLARK COUNTY,
NEVADA
AND INCORPORATED AREAS

PANEL 2955 OF 4090

USE MAP INDEX FOR FIRM PANEL LAYOUT.

COVERAGE

EXCLUSIONS

SEWER WATER WINDSTORM

CLARK COUNTY
UNINCORPORATED AREAS
UNINCORPORATED AREAS
SCHOOL CITY, CITY OF

SEWER 000 000 000
WATER 000 000 000
WINDSTORM 000 000 000

**REVISED TO
REFLECT LOSS
DATED NOV 06 2003**

Revised to reflect the following: Additional details for areas
under existing map 2955 of the Flood Insurance Rate Map
for Clark County, Nevada. The following information is for
information only and is not intended to be used as a basis for
underwriting.

MAP NUMBER
32003C2955E

MAP REVISED:
SEPTEMBER 27, 2002



Federal Emergency Management Agency

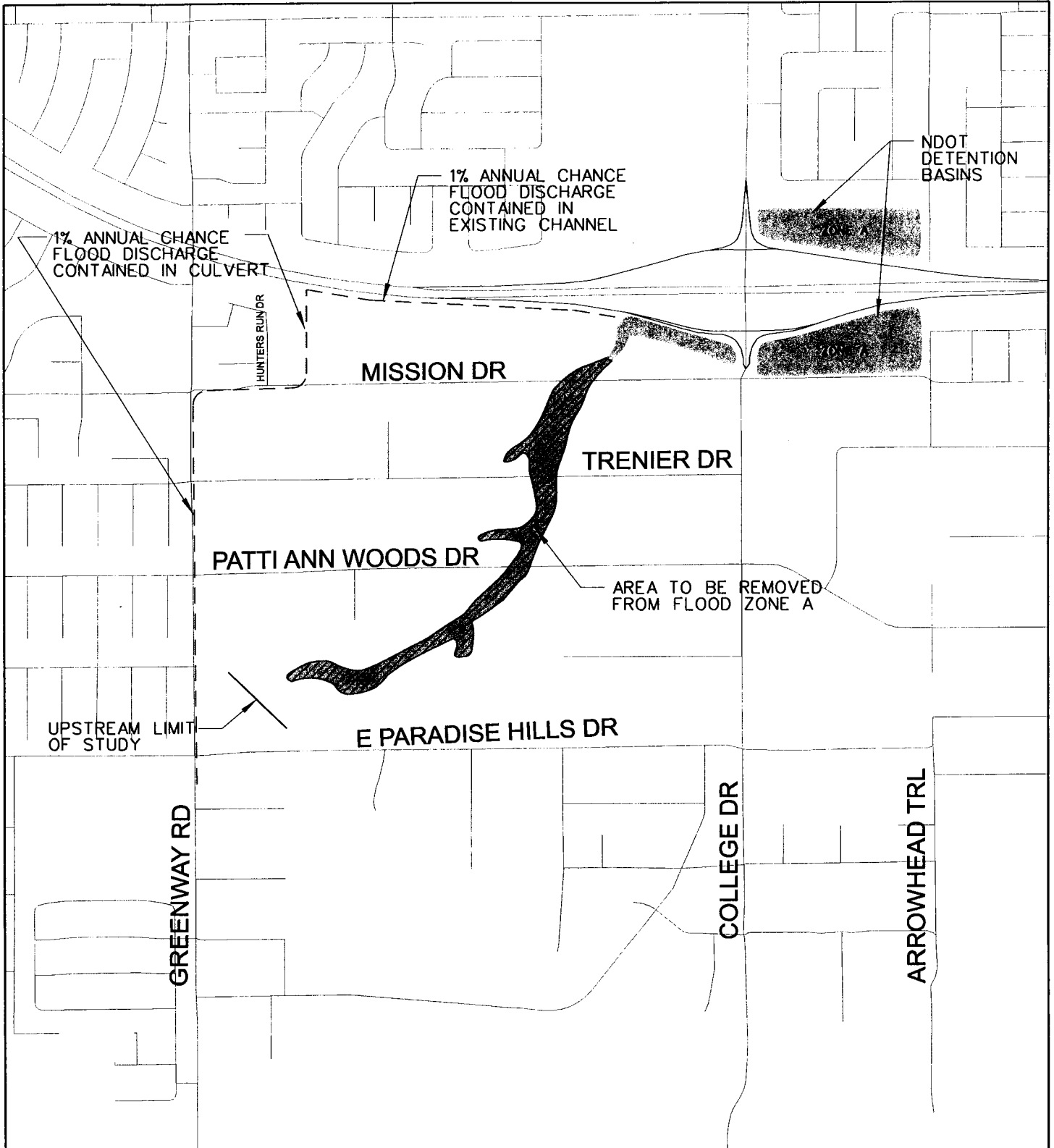
FLOOD ZONE (A) MAP
w/ 5-foot contours
- FIGURE 2.1



NOTE:
THIS MAP IS FOR PLANNING PURPOSES
ONLY. NO REPRESENTATION IS MADE
CONCERNING THE ACCURACY OF THE DATA
DELINEATED HEREIN.

 VTM nevada 2727 S. RAINBOW BOULEVARD LAS VEGAS, NEVADA 89146-5148	MISSION DRIVE FLOOD ZONE EXHIBIT with 5-foot contours (1996)			W.O.#: 6139
				DATE: 03-11-05
				BY:
				SCALE: 1"=500'
			SHEET 1 OF 1	

**VTN POST-PROJECT
ANNOTATED FLOOD ZONE MAP
- FIGURE 2.3**



PANEL 2955 OF 4090

CITY OF HENDERSON

MAP NUMBER: 32003C2955E

NUMBER	PANEL	SUFFIX
320005	2955	E

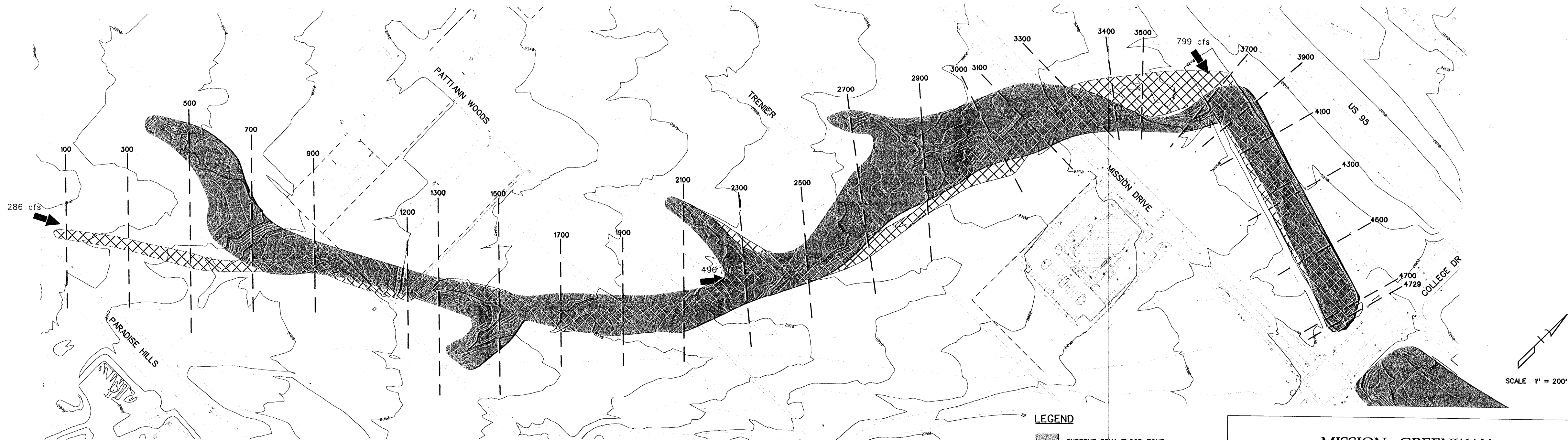
SCALE 1" = 1000'

ANNOTATED FLOOD ZONE MAP

FIGURE X

vtm CONSULTING ENGINEERS
 PLANNERS
 LAND SURVEYORS 3227 S. RAINBOW BLVD
 LAS VEGAS, NV 89146
 PHONE (702) 547-1000
 FAX (702) 547-2822
 nevada

MISSION-GREENWAY: PRE-PROJECT CONDITIONS
(EFFECTIVE WORK MAP)
FIGURE 2.4



LEGEND

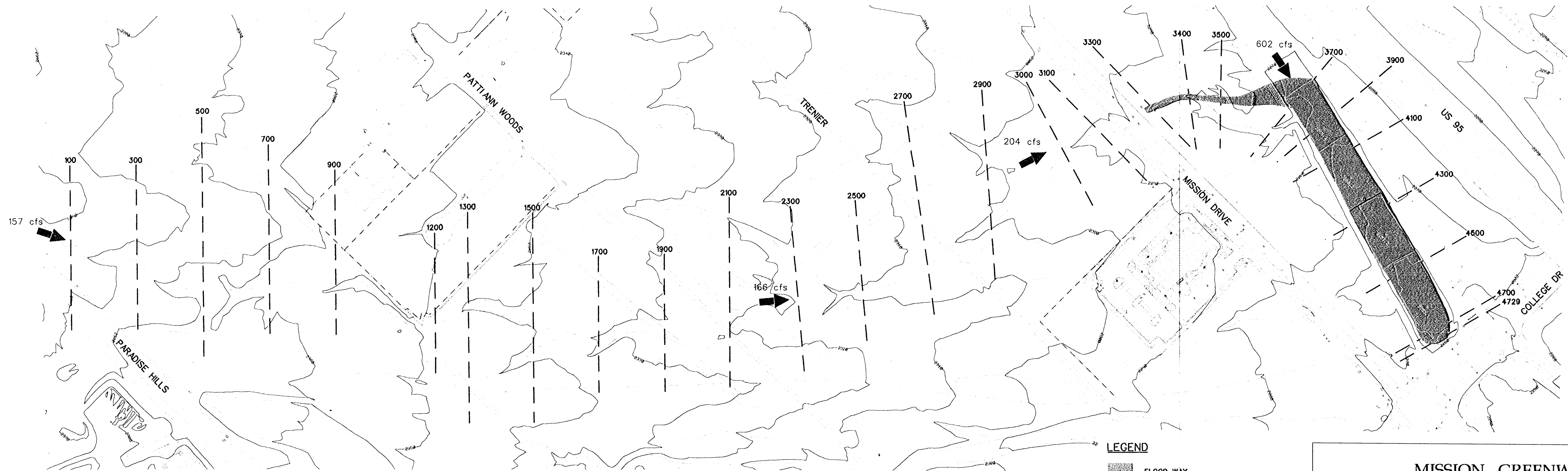
-  CURRENT FEMA FLOOD ZONE
-  EFFECTIVE 100-YEAR FLOOD PLAIN
-  100 YEAR FLOW

MISSION - GREENWAY PRE-PROJECT CONDITIONS (EFFECTIVE WORK MAP)

vtm CONSULTING ENGINEERS
PLANNERS
LAND SURVEYORS
NEVADA

SCALE 1" = 200'

MISSION-GREENWAY: POST-PROJECT CONDITIONS
(POST-PROJECT WORK MAP)
FIGURE 2.5



LEGEND

-  FLOOD WAY
-  100 YEAR FLOW

SCALE 1" = 200'

**MISSION - GREENWAY
POST-PROJECT CONDITIONS
(POST PROJECT WORK MAP)**

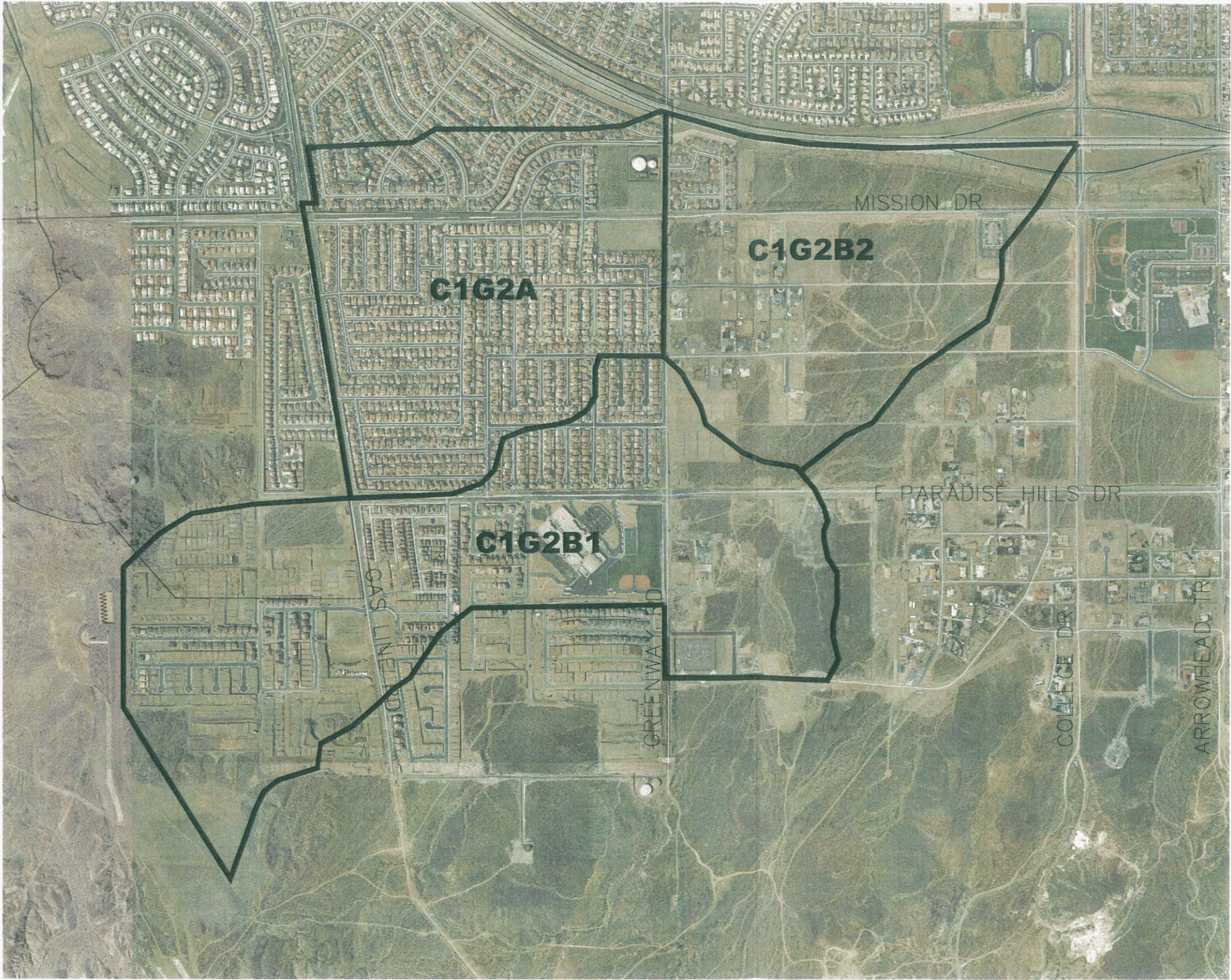
vtn nevada
CONSULTING ENGINEERS
 PLANNERS
 LAND SURVEYORS
 2727 S. RANNEY BLVD.
 LAS VEGAS, NV 89146
 PHONE: 702.734.4222 FAX: 702.734.4222

APPENDIX C

HYDROLOGY

**MISSION DRIVE LOMR
PRE-PROJECT: SUBBASIN MAP**

PLT (95)
E:\6139-CLOMR\DWG\6139-CLOMR-SUB-BASIN-MAP



TITLE
SUBBASIN MAP

FIGURE 1.1

PROJECT
MISSION DRIVE CLOMR
PRE-IMPROVEMENT

SEAL

WD. NO. 6139-CLOMR

BY DRF
DATE 01/03/06

SCALE HORIZ.
VERT.

DRAWING 1
SHEET 1 OF 1
SHEETS



CONSULTING ENGINEERS • PLANNERS • LAND SURVEYORS
2727 SOUTH RAINBOW BOULEVARD
LAS VEGAS, NEVADA 89102-5148 PHONE (702) 873-7550 FAX (702) 362-2597

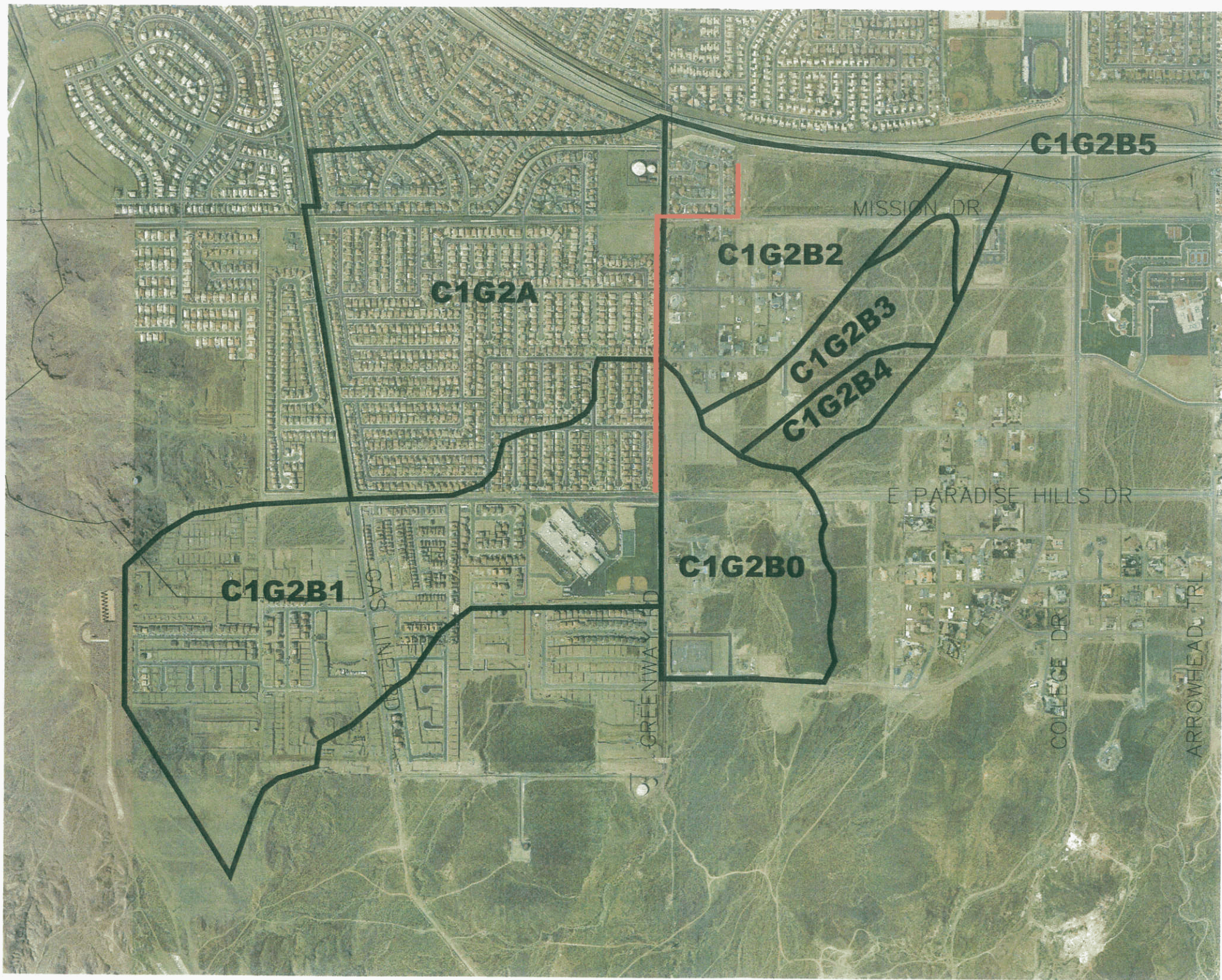
REVISION

BY

DATE

REV

**MISSION DRIVE LOMR
POST-PROJECT: SUBBASIN MAP**

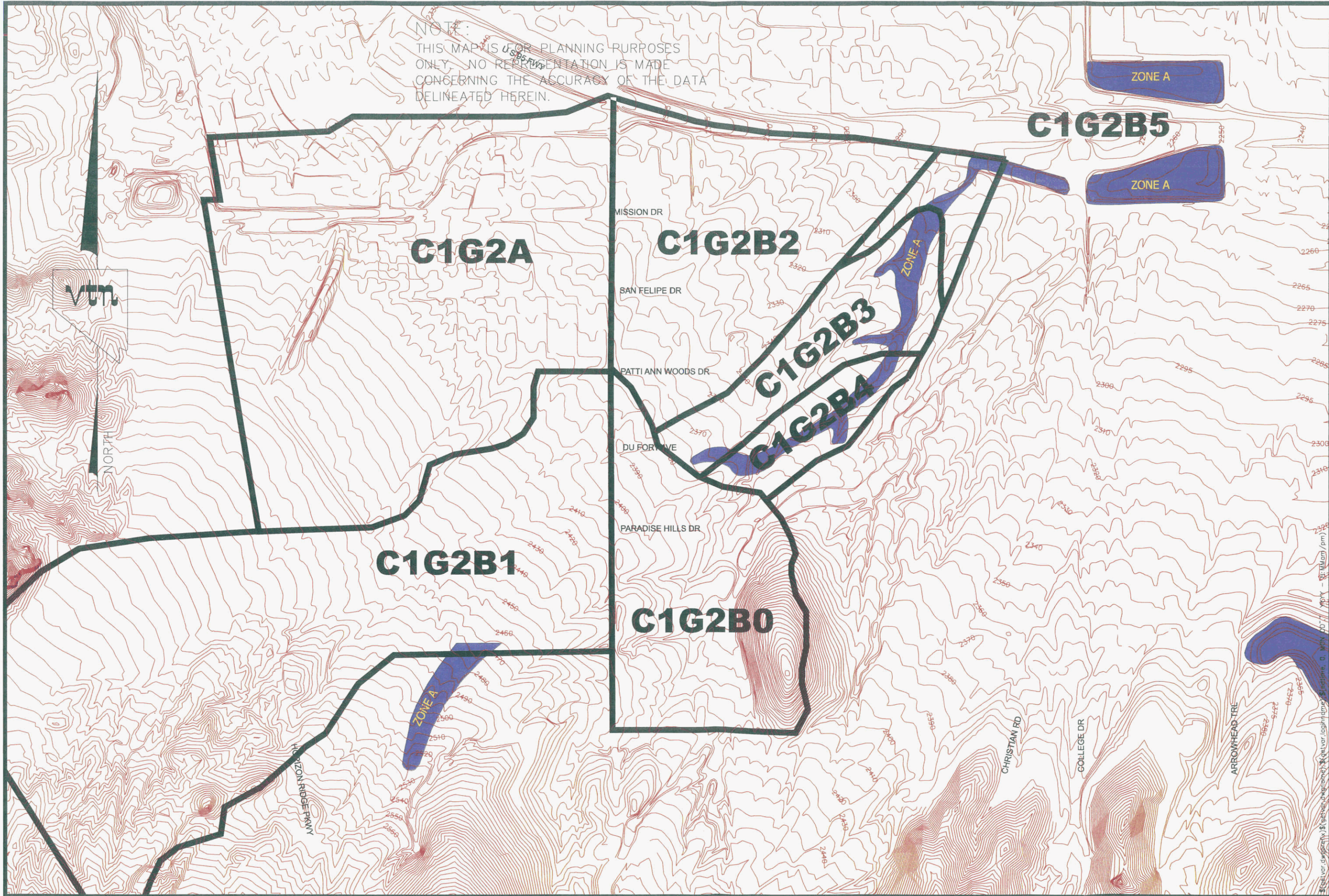


EXISTING CHANNEL
(MISSION DRIVE/GREENWAY
IMPROVEMENTS)



TITLE		SUBBASIN MAP FIGURE 1.2	
PROJECT		MISSION DRIVE CLOMR POST IMPROVEMENT	
SEAL			
WO. NO.		6139-CLOMR	
BY		DRF	
DATE		01/03/06	
SCALE		HORIZ. VERT.	
DRAWING		SHEET 1 OF 1 SHEETS	

CONSULTING ENGINEERS		PLANNERS • LAND SURVEYORS	
LAS VEGAS, NEVADA 89102-5148		2727 SOUTH RAINBOW BOULEVARD	
PHONE (702) 873-7550		FAX (702) 362-2597	
vtm nevada			
REVISION			
REV	DATE	BY	
1			
2			
3			



MISSION DRIVE
POST PROJECT
SUBBASIN MAP

**HYDROLOGIC PARAMETERS: PRE-PROJECT
CN, AREAS, LAGTIME**

CURVE NUMBER DETERMINATION
MISSION DRIVE IMPROVEMENTS : PRE-PROJECT LOMR
(MPU 2002 CONDITIONS)

* See end of table for abbreviated landuse descriptions.

Hydrologic Soil Group (Soil Survey Reference #'s)			Hydrologic Soil Group A (107 & 262)										Hydrologic Soil Group B										Hydrologic Soil Group D (150, 152, 240, 360)									
Subbasin		* Existing Landuse	LDR %			HFR %				UNF %	UNP %	LDR %			HFR %				UNF %	UNP %	LDR %			HFR %				UNF %	UNP %			
	CHECK	CN #	51.0	61.0	76.0	81.0	89.0	39.0	81.0	55.0	63.0	68.0	75.0	84.0	88.0	92.0	61.0	88.0	72.0	77.0	84.0	87.0	91.0	93.0	95.0	80.0	93.0	86.0	88.0			
Subbasins Contributing Directly to Debris Basin Below																																
C1G2B1	0	74.0	CN, Area & Lag Time Value C-1 WATERSHED FIS RESTUDY - SDN3 (NOV 2002)																													
C1G2B2	0	77.0	CN, Area & Lag Time Value C-1 WATERSHED FIS RESTUDY - SDN3 (NOV 2002)																													
C1G2A	0	79.0	CN, Area & Lag Time Value C-1 WATERSHED FIS RESTUDY - SDN3 (NOV 2002)																													

Abbreviated Landuse Description:

LDR = Low Density Residential (40,000 sq-ft lots)
MDR = Medium Density Residential (10,000 sq-ft lots)
HDR = High Density Residential (7,000 sp-ft lots)
HFR = Multi Family Residential (Apartments/Condos)
COM = Commercial And Business
PRK = Parks, Golf Courses (Open Space - Good Condition, Grass Cover > 75%)
IND = Industrial
UNF = Undeveloped Semiarid Rangeland (Desert Shrub - Fair, 30 to 70% Ground Cover)
UNP = Undeveloped Semiarid Rangeland (Desert Shrub - Poor, Ground Cover < 30%)

**HYDROLOGIC PARAMETERS: POST-PROJECT
CN, AREAS, LAGTIME**

CURVE NUMBER DETERMINATION
MISSION DRIVE IMPROVEMENTS: POST-PROJECT LOMR
(MPU 2002 CONDITIONS)

* See end of table for abbreviated landuse descriptions.

Hydrologic Soil Group (Soil Survey Reference #'s)			Hydrologic Soil Group A (107 & 262)										Hydrologic Soil Group B								Hydrologic Soil Group D (150, 152, 240, 360)									
Subbasin		* Existing Landuse	LDR %		HFR %		UNF %		UNP %		LDR %		HFR %		UNF %		UNP %		LDR %		HFR %		UNF %		UNP %					
	CHECK	CN #	51.0	61.0	76.0	81.0	89.0	39.0	81.0	55.0	63.0	68.0	75.0	84.0	88.0	92.0	61.0	88.0	72.0	77.0	84.0	87.0	91.0	93.0	95.0	80.0	93.0	86.0	88.0	
Subbasins Contributing Directly to Debris Basin Below																														
C1G2A	-	79.0	CN, Area & Lag Time Value C-1 WATERSHED FIS RESTUDY - SDN3 (NOV 2002)																											
C1G2B1	-	74.0	CN, Area & Lag Time Value C-1 WATERSHED FIS RESTUDY - SDN3 (NOV 2002)																											
C1G2B0	100	80.0															7			73									20	
C1G2B2	100	71.6										60							40											
C1G2B3	100	75.2										20							80											
C1G2B4	100	77.0																	100											
C1G2B5	100	77.0																	100											

Abbreviated Landuse Description:

LDR = Low Density Residential (40,000 sq-ft lots)
MDR = Medium Density Residential (10,000 sq-ft lots)
HDR = High Density Residential (7,000 sp-ft lots)
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PRK = Parks, Golf Courses (Open Space - Good Condition, Grass Cover > 75%)
IND = Industrial
UNF = Undeveloped Semiarid Rangeland (Desert Shrub - Fair, 30 to 70% Ground Cover)
UNP = Undeveloped Semiarid Rangeland (Desert Shrub - Poor, Ground Cover < 30%)

**CARTER BURGESS POST DEVELOPMENT
HEC-1 MODEL
(REFERENCE FOR VTN NEVADA
PRE-PROJECT CONDITIONS HEC-1)**

*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

1 HEC-1 INPUT PAGE 1

1 HEC-1 INPUT PAGE 2

Page 1

SDN3.OUT

1

HEC-1 INPUT

PAGE 3

1

HEC-1 INPUT

PAGE 4

1

HEC-1 INPUT

PAGE 9

Page 2

```

161 KK C5ICB
162 KM ROUTE C5ICB TO MISSION HILLS DETENTION BASIN
163 KM FACILITY # = C1CH 0882
164 KM TYPE OF FACILITY = ROCK LEVEE
165 RD 2350 0.024 0.040 0 TRAP 50 2
*

166 KK C5I2A
167 KM PART OF 2001 MPU C1-9
168 BA 1.400
169 PB 3.33
170 LS 0 80
171 UD 0.14
*

172 KK CP6B
173 KM COMBINE RC5ICB AND C5I2A
174 HC 2
*

175 KK CP6
176 KM COMBINE CP6A AND CP6B
177 KM @ MISSION HILLS DETENTION BASIN
178 HC 2
*
* THE MISSION HILLS DETENTION BASIN STAGE/DISCHARGE AND STAGE/VOLUME RELATIONS
* WERE CHECKED AGAINST THE LATEST RECORD DRAWINGS AND PREDESIGN REPORTS.
* THE FOLLOWING INPUT REFLECTS RECORD DRAWING INFORMATION
*

179 KK DB2
180 KM FACILITY = MISSION HILLS DETENTION BASIN
181 KM FACILITY # C1CH 0854
182 KM STORAGE VOLUME = 402 ACRE-FEET (100-YR WSE)
183 KM OUTLET = 84" RCP
184 KO 3
185 RS 1 STOR -1
186 SV 0 2.55 15.85 40.23 72.34 107.2 185.2 273.0 371.6 480.1
187 SV 598.5 630.2
188 SE 2323 2326 2328 2330 2332 2334 2338 2342 2346 2350
189 SE 2354 2355
190 SQ 0 56.78 108.7 142.9 170.4 193.9 234.1 268.4 298.7 326.1
191 SQ 351.6 357.6
192 SE 2323 2326 2328 2330 2332 2334 2338 2342 2346 2350
193 SE 2354 2355
*

194 KK RDB2
195 KM ROUTE DB2 TO C1G2D
196 KM FACILITY = MISSION HILLS DETENTION BASIN
197 KM FACILITY # = 0757
198 KM TYPE OF FACILITY = RCP
199 RD 6100 0.025 0.013 0 CIRC 7.0
*

```

1

HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

200 KK C1G2C
201 KM PART OF 2001 MPU C1-13
202 BA .2925
203 PB 3.23
204 LS 0 76
205 UD 0.27
*

206 KK C1G2D
207 KM PART OF 2001 MPU C1-21
208 BA .2244
209 PB 3.27
210 LS 0 73
211 UD .22
*

212 KK CP7A
213 KM COMBINE RDB2, C1G2C, AND C1G2D
214 KM NDOT DETENTION BASIN @ US95
215 HC 3
*

216 KK C1G2B1
217 KM PART OF 2001 MPU C1-10
218 BA .5231
219 PB 3.17
220 LS 0 74
221 UD .42
*

222 KK RG2B1
223 KM ROUTE C1G2B1 TO C1G2B2
224 KM NO FACILITY - OVERLAND FLOW
225 RD 4400 .028 .030 0 TRAP 200
*

226 KK C1G2B2
227 KM PART OF 2001 MPU C1-12
228 BA .3097
229 PB 3.20
230 LS 0 77
231 UD .27
*

232 KK CP7B
233 KM COMBINE C1G2B1, C1G2B2
234 KM COLLEGE AT US95
235 HC 2
*

236 KK C1G2A
237 KM PART OF 2001 MPU C1-11
238 BA .3468
239 PB 3.17
240 LS 0 79
241 UD 0.22
*

242 KK RC1G2A
243 KM ROUTE C1G2A TO CP7C
244 KM NDOT FACILITY @US95
245 RD 3800 .018 .030 0 TRAP 100
*

```

1

HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

246 KK CP7C
247 KM COMBINE CP7B AND C1G2A
248 KM COLLEGE AT US95
249 HC 2
*

250 KK CP7
251 KM COMBINE CP7B AND CP7C
252 KM NDOT FACILITY AT US95
253 HC 2
*

* NDOT DETENTION BASIN INPUT IS TAKEN FROM PREDESIGN REPORT AND DRAWINGS
* THIS DETENTION BASIN IS BROKEN INTO TWO DETENTION PONDS, NAMELY POND A AND
* POND B, ON THE UPPER AND LOWER SIDE OF THE INTERCHANGE, RESPECTIVELY. THE
* 100-YR PEAK IS ATTENUATED THROUGH THE BASIN BY ROUTING OF THE HYDROGRAPH,
* FIRST THROUGH POND A AND SECOND THROUGH POND B. A DOUBLE 10X10 RCB CONNECTS
* THE TWO PONDS UNDER I-515, INV EL = 2230 (INLET) AND 2221 (OUTLET) WHEREAS
* A TRIPPLE RCB WAS DESIGNED AT THE OUTLET WITH INVERT EL = 2219.68, BUT IS NOT
* CONSTRUCTED TO DATE. THE FOLLOWING STAGE/STORAGE AND STAGE/DISCHARGE RELATION
* WERE TAKEN FROM THE NDOT PREDESIGN REPORT.
*

254 KK CP7DB
255 KM FACILITY = NDOT DETENTION BASIN
256 KM FACILITY # C1CH 0658
257 KM POND A
258 KM STORAGE VOLUME = 94 AC-FT AT WSE= 2248
259 KM OUTLET = DOUBLE 10 X 10 RCB
260 KO 3
261 RS 1 STOR -1
262 SV 0 .125 .660 1.852 3.904 6.967 11.156 16.146 21.506 27.208
263 SV 33.219 39.589 46.369 53.528 61.032 68.877 77.056 85.507 94.163 102.957
264 SE 2230 2231 2232 2233 2234 2235 2236 2237 2238 2239
265 SE 2240 2241 2242 2243 2244 2245 2246 2247 2248 2249
266 SQ 0 70.2 180.1 317.4 479.1 659.2 854.5 1068.1 1290.9 1525.9
267 SQ 1776.1 2038.6 2256.8 2384.2 2511.7 2700 2887.0 3060.9 3225.7 3515.4
268 SE 2230 2231 2232 2233 2234 2235 2236 2237 2238 2239
269 SE 2240 2241 2242 2243 2244 2245 2246 2247 2248 2249
*

SDN3.OUT

1

HEC-1 INPUT

PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

270 KK CP7DB
271 KM FACILITY = NDOT DETENTION BASIN
272 KM FACILITY # C1CH 0658
273 KM POND B
274 KM STORAGE VOLUME = 94 AC-FT AT WSE= 2232
275 KO 3
276 RS 1 STOR -1
277 SV 0 .677 5.419 13.616 21.947 30.416 39.025 47.764 56.622 65.611
278 SV 74.74 84.018 93.457 103.051 112.794 2225 2226 2227 2228 2229
279 SE 2220 2221 2222 2223 2224 2225 2226 2227 2228 2229
280 SE 2230 2231 2232 2233 2234 2235 2236 2237 2238 2239
281 SQ 0 13.2 37.2 152.0 340.3 578.1 849.7 1155.1 1488.1 1845.5
282 SQ 2224.9 2481.1 2700.8 3035.5 3461.4 2225 2226 2227 2228 2229
283 SE 2220 2221 2222 2223 2224 2225 2226 2227 2228 2229
284 SE 2230 2231 2232 2233 2234
*

285 KK RCP7
286 KM ROUTE CP7 TO CP8A
287 KM PARTIALLY IMPROVED CHANNEL
288 KM FACILITY # C1CH 0613, 0641, AND 0674
289 RD 3960 .025 .030 0 TRAP 20
*

290 KK C1NA
291 KM 2001 MPU C1-14
292 BA .4139
293 PB 3.18
294 LS 0 84
295 UD 0.03
*

296 KK RC1NA
297 KM ROUTE C1NA TO CP8A
298 KM FACILITY = PARTIALLY IMPROVED CHANNEL
299 KM FACILITY # C1CH 0613, 0641, AND 0674
300 RD 1980 .025 .030 0 TRAP 20
*

301 KK CP8
302 KM COMBINE C1NA AND CP8A
303 HC 2
*

304 KK RCP8
305 KM ROUTE CP8 TO C1HA
306 KM C1 AND PUEBLO
307 RD 2500 .025 .030 0 TRAP 20
*

* BEGIN POGGEMEYER DESIGN GROUP INPUT FROM 1998 LETTER OF MAP REVISION
* FOR THE EQUESTRIAN DETENTION BASIN, CASE NO 99-09-623P. SOME SUBBASINS
* IN THIS MODEL HAVE BEEN MODIFIED TO REFLECT POST 1998 DEVELOPMENT.
* THE FOLLOWING TABLE CORRELATES 1998 LOMR SUBBASIN LABELS WITH LABELS IN
* THIS MODEL.

* *
* * EQUIVALENT 1998 LOMR SUBBASIN LABELS *
* *
* *
* * 1998 LOMR THIS MODEL *
* *
* * C5FD C5FD *
* * C5FA C5FA *
* * C5FB C5FB *
* * C5FC C5FC *
* * C5EA C5EA *
* * C5EC C5EC *
* * C5EB C5EB *
* * C5ED C5ED *
* * C5DA C5DA *
* * C5DB C5DB *
* * C5CAa N/A *
* * C5CAb N/A *
* * C5CB C5CB *
* * C5DC N/A *
* * OFF-2A N/A *
* * OFF-2B N/A *
* * OFF-2C C1HD *
* * OFF-3 C1HE *
* * OFF-4 C1HF *
* * OFF-6 N/A *
* * OFF-8 C5IID *
* * OFF-9 C5IIE *
* * OFF-10 C5GD *
* * OFF-11 N/A *

```

* *                OFF-12                C5I1C                *
* *                OFF-13                N/A                    *
* *                OFF-14                C5GA                    *
* *                OFF-15                C5GB                    *
* *                OFF-16                C5GC                    *
* *                OFF-21                N/A                    *
* *                OFF-23                N/A                    *
* *                OFF-24                N/A                    *
* *****

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HEC-1 INPUT

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

308      KK      C5GC
309      KM      1998 LOMR OFF-16
310      BA      .1107
311      PB      3.43
312      LS      0      84
313      UD      0.04
*

314      KK      RC5GC
315      KM      ROUTE C5GC TO C5GB
316      RD      1000 .020 .030      TRAP      100
*

317      KK      C5GB
318      KM      1998 LOMR OFF-15
319      BA      .3249
320      PB      3.43
321      LS      0      83
322      UD      .16
*

323      KK      CP9
324      KM      COMBINE C5GB AND C5GC
325      HC      2
*

326      KK      RCP9
327      KM      ROUTE CP9 TO C5GA
328      RD      2640 .035 .030      TRAP      40
*

329      KK      C5GA
330      KM      1998 LOMR OFF-14
331      BA      .2723
332      PB      3.39
333      LS      0      66
334      UD      .30
*

335      KK      CP10
336      KM      COMBINE RCP9 AND C5GA
337      HC      2
*

338      KK      RCP10
339      KM      ROUTE CP10 TO C5I1E
340      RD      2200 .033 .030      TRAP      100
341      *

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HEC-1 INPUT

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

342      KK      RCP10
343      KM      ROUTE CP10 TO C5I1E
344      RD      2200 .030 .030      TRAP      100
*

345      KK      C5GD
346      KM      1998 LOMR OFF-10
347      BA      .4447
348      PB      3.46
349      LS      0      67
350      UD      0.46
*

351      KK      DIVER1
352      KM      DIVERT FLOWS CONVEYED INTO CULVERT "A" STA 296+24, ACROSS BOULDER HIGHWAY
353      DT      DIVER1
354      DI      0      37      126      260      502
355      DQ      0      10      20      30      40
*

356      KK      RC5GD
357      KM      ROUTE C5GD TO C5I1E
358      RD      2200 .030 .030      TRAP      100
*

359      KK      C5I1E
360      KM      1998 LOMR OFF-9
361      BA      .1634
362      PB      3.45
363      LS      0      79
364      UD      .05
*

365      KK      CP11
366      KM      COMBINE RCP10, C5I1E, AND RC5GD
367      HC      3
*

368      KK      RCP11
369      KM      ROUTE CP11 TO C1HF
370      RD      1600 .04 .030      TRAP      100
*

371      KK      C1HF
372      KM      1998 LOMR OFF-4
373      BA      .1008
374      PB      3.45
375      LS      0      78
376      UD      0.27
*

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HEC-1 INPUT

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

377      KK      CP12
378      KM      COMBINE RCP11 AND C1HF
379      HC      2
*

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380 KK RCP12
381 KM ROUTE CP12 TO C1HE
382 RD 1800 .013 .030 TRAP 200
  *

383 KK C5I1B
384 KM MODIFIED 1998 LOMR SUBBASIN OFF-13
385 BA .5185
386 PB 3.43
387 LS 0 71
388 UD 0.08
  *

389 KK RC5I1B
390 KM ROUTE C5I1B TO C5I1D
391 RD 1100 .018 .030 TRAP 100
  *

392 KK C5I1D
393 KM 1998 LOMR OFF-8
394 BA .1158
395 PB 3.43
396 LS 0 77
397 UD .15
  *

398 KK CP13
399 KM COMBINE RC5I1B TO C5I1D
400 HC 2
  *

401 KK RCP13
402 KM ROUTE CP13 TO C1HE
403 RD 2100 .021 .030 TRAP 100
  *

404 KK C1HE
405 KM 1998 LOMR OFF-3
406 BA .1467
407 PB 3.29
408 LS 0 72
409 UD .14
  *

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HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

410 KK CP14
411 KM COMBINE RCP12, RCP13, AND C1HE
412 HC 3
  *

413 KK DIVER2
414 KM DIVERT CULVERT AND BOULDER HIGHWAY OVERFLOWS INTO MAGIC WAY 844+00, 843+52,
415 AND 840+46, TO SUBBASIN C5CC
416 DT DIVER2
417 DI 0 1255 2000
418 DQ 0 116 900
  *

419 KK RCP14
420 KM ROUTE CP14 TO C1HD
421 RD 800 .010 .030 TRAP 100
  *

422 KK C1HD
423 KM 1998 LOMR OFF-2C
424 BA .0716
425 PB 3.29
426 LS 0 77
427 UD 0.15
  *

428 KK CP15
429 KM COMBINE RCP14 AND C1HD
430 HC 2
  *

431 KK RCP15
432 KM ROUTE CP15 TO C1HCB
433 RD 1700 .010 .030 TRAP 100
  *

434 KK DIVER3
435 KM DIVERT CULVERT FLOWS INTO SUBBASIN C5CC, STA 832+02, 825+52, AND 834+82
436 DT DIVER3
437 DI 0 1171 2000
438 DQ 0 217 900
  *

439 KK C5I1
440 KM 1998 LOMR OFF-11
441 BA .2432
442 PB 3.43
443 LS 0 76
444 UD .17
  *

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HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

445 KK C5I1C
446 KM 1998 LOMR OFF-12
447 BA 0.0643
448 PB 3.43
449 LS 0 80
450 UD .23
  *

451 KK RC5I1C
452 KM ROUTE C5I1C TO C5I1
453 RD 700 .014 .030 TRAP 100
  *

454 KK CP16
455 KM COMBINE RC5I1C AND C5I1
456 HC 2
  *

457 KK RCP16
458 KM ROUTE CP16 TO C1G1B
459 RD 1200 .018 .030 TRAP 50
  *

460 KK C1G1B
461 KM 1998 LOMR OFF-6 IS PART OF THIS SUBBASIN
462 PB 3.21

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463 BA .1428
 464 LS 0 87
 465 UD .18
 *
 466 KK CP17
 467 KM COMBINE RCP16 AND C1G1B
 468 HC 2
 *
 469 KK RCP17
 470 KM ROUTE CP17 TO C1HCB
 471 RD 1700 .010 .030 TRAP 100
 *
 472 KK C1HCB
 473 KM MODIFIED 1998 LOMR OFF-2B
 474 BA .1818
 475 PB 3.29
 476 LS 0 78
 477 UD 0.06
 *

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HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

478 KK CP18A
 479 KM COMBINE RCP17, AND C1HCB
 480 HC 2
 *
 481 KK CP18
 482 KM COMBINE RCP15 AND CP18A
 483 HC 2
 *
 484 KK DIVER4
 485 KM DIVERT CULVERT FLOWS AND BOULDER OVERFLOWS INTO SUBBASIN C5CC
 486 KM STA 816+22 AND 819+84, BOULDER HIGHWAY
 487 DT DIVER4
 488 DI 0 1234 2000
 489 DQ 0 111 1000
 *
 490 KK RCP18
 491 KM ROUTE CP18 TO C1HB
 492 RD 1100 .007 .030 TRAP 100
 *
 493 KK C1G1A
 494 KM 2001 MPU C1-15
 495 BA .2243
 496 PB 3.20
 497 LS 0 84
 498 UD 0.22
 *
 499 KK RC1G1A
 500 KM ROUTE TO C1HB
 501 KM OVERLAND FLOW
 502 RD 2600 .025 .030 TRAP 200
 *
 503 KK C1HB
 504 KM MODIFIED 1998 LOMR OFF-2A
 505 BA .1472
 506 PB 3.21
 507 LS 0 85
 508 UD 0.03
 *
 509 KK CP19A
 510 KM COMBINE C1HB, RC1G1A
 511 HC 2
 *

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HEC-1 INPUT

PAGE 15

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

512 KK CP19
 513 KM COMBINE CP19A AND RCP18
 514 HC 2
 *
 515 KK DIVER5
 516 KM DIVERT CULVERT FLOWS INTO SUBBASIN C4A1C, STA 807+37
 517 DT DIVER5
 518 DI 0 798 2000
 519 DQ 0 70 970
 *
 520 KK RCP19
 521 KM ROUTE CP19 TO BOULDER HIGHWAY AND PUEBLO
 522 RD 2300 .013 .030 TRAP 100
 *
 523 KK C1HA
 524 KM SUBBASIN C1HA
 525 KM 2001 MPU C1-24
 526 BA .0735
 527 PB 3.13
 528 LS 0 66
 529 UD .21
 *
 530 KK CP20A
 531 KM COMBINE C1HA AND RCP19
 532 HC 2
 *
 533 KK CP20
 534 KM COMBINE CP20A AND RCP8
 535 HC 2
 *
 536 KK RCP20
 537 KM ROUTE CP20 TO C1B
 538 KM FACILITY = C-1 CHANNEL
 539 KM FACILITY # C1CH 0528
 540 KM TYPE OF FACILITY = CONCRETE CHANNEL
 541 RD 1700 .027 .015 TRAP 25 1
 *
 542 KK C1D
 543 KM 2001 MPU C1-26
 544 BA .4005
 545 PB 3.14

546 LS 0 78
 547 UD .21
 *

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HEC-1 INPUT

PAGE 16

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

548 KK RC1D
 549 KM ROUTE C1D TO C1C
 550 KM UNION PACIFIC RAILROAD
 551 RD 1600 .014 .030 0 TRAP 0 50
 *

552 KK C1C
 553 KM 2001 MPU C1-27
 554 BA .2307
 555 PB 3.08
 556 LS 0 80
 557 UD .19
 *

558 KK CP21
 559 KM COMBINE RC1D AND C1C
 560 HC 2
 *

561 KK RCP21
 562 KM ROUTE CP21 TO C1B
 563 RD 4600 .010 .015 0 TRAP 0 30
 *

564 KK C1B
 565 KM 2001 MPU C1-28
 566 BA .3773
 567 PB 3.11
 568 LS 0 86
 569 UD .21
 *

570 KK C4A1D
 571 KM 2001 MPU C1-25
 572 BA 0.062
 573 PB 3.11
 574 LS 0 78
 575 UD .19
 *

576 KK RC4A1D
 577 KM ROUTE C4A1D TO C1B
 578 RD 700 .020 .015 TRAP 25 1
 *

579 KK CP22
 580 KM COMBINE RCP19, RCP20, C1B, AND RC4A1D
 581 HC 4
 *

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HEC-1 INPUT

PAGE 17

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

582 KK RCP22
 583 KM ROUTE CP21 TO C1A
 584 KM FACILITY = C-1 CHANNEL
 585 KM FACILITY # = C1CH 0455, 0502
 586 KM TYPE OF FACILITY = CONCRETE CHANNEL
 587 RD 3200 .021 .015 TRAP 25 1
 *

588 KK C1A
 589 KM 2001 MPU C1-29
 590 BA .1456
 591 PB 2.99
 592 LS 0 84
 593 UD .22
 *

594 KK CP23
 595 KM COMBINE CP22 AND C1A
 596 HC 2
 *

597 KK RCP23
 598 KM ROUTE CP23 TO C4A1B
 599 KM FACILITY = C-1 CHANNEL
 600 KM FACILITY # = C1CH 0455
 601 KM TYPE OF FACILITY = CONCRETE CHANNEL
 602 RD 1250 .025 .025 TRAP 25 1
 *

603 KK C5CC
 604 KM 1998 LOMR OFF-21
 605 PB 3.29
 606 BA .3346
 607 LS 0 79
 608 UD 0.28
 *

609 KK RET4
 610 KM RETRIEVE FLOWS FROM C1HCB
 611 DR DIVER4
 *

612 KK RDIV4
 613 KM ROUTE DIVERSION 4 TO CP24A
 614 KM TYPE OF FACILITY = OVERLAND FLOW TO EQUESTRIAN
 615 RD 1100 .027 .030 TRAP 100 1
 *

616 KK RDIV4
 617 KM ROUTE DIVERSION 4 TO CP24A
 618 KM TYPE OF FACILITY = STREET FLOW IN EQUESTRIAN
 619 RD 1700 .009 .016 TRAP 80 1
 *

1

HEC-1 INPUT

PAGE 18

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

620 KK CP24A
 621 KM COMBINE C5CC AND RDIV4
 622 HC 2
 *

623 KK RET3
 624 KM RETRIEVE DIVERSION 3 FROM C1HD
 625 DR DIVER3
 *

```

626 KK RDIV3
627 KM ROUTE DIVERSION 3 TO CP24A
628 KM TYPE OF FACILITY = OVERLAND FLOW TO EQUESTRIAN
629 RD 2000 .023 .030 TRAP 100 1
*

630 KK RDIV3
631 KM ROUTE DIVERSION 3 TO CP24A
632 KM TYPE OF FACILITY = STREET FLOW IN EQUESTRIAN
633 RD 1100 .009 .016 TRAP 80 1
*

634 KK CP24B
635 KM COMBINE CP24A AND RDIV4
636 HC 2
*

637 KK RET2
638 KM RETRIEVE DIVERSION 2 FROM C1HE
639 DR DIVER2
*

640 KK RDIV2
641 KM ROUTE DIVERSION 2 TO CP24A
642 KM TYPE OF FACILITY = OVERLAND FLOW TO EQUESTRIAN
643 RD 2500 .024 .030 TRAP 100 1
*

644 KK RDIV2
645 KM ROUTE DIVERSION 2 TO CP24A
646 KM TYPE OF FACILITY = STREET FLOW IN EQUESTRIAN
647 RD 600 .009 .016 TRAP 80 1
*

648 KK CP24C
649 KM COMBINE CP24B AND RDIV2
650 HC 2
*

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HEC-1 INPUT

PAGE 19

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

651 KK C5CA
652 KM PART OF 1998 LOMR C5Cab
653 KM 2001 MPU C1-30
654 BA .2974
655 PB 3.41
656 LS 0 70
657 UD 0.22
*

658 KK RC5CA
659 KM ROUTE C5CA TO C5CF
660 KM APPALOOSA RD
661 RD 2000 .019 .016 0 TRAP 0 50
*

662 KK C5CF
663 KM PART OF 1998 LOMR C5CA6
664 KM 2001 MPU C1-31
665 BA .3233
666 PB 3.25
667 LS 0 68
668 UD 0.07
*

669 KK CP25
670 KM COMBINE RC5CA AND C5CF
671 KM APPALOOSA ROAD AND PALOMINO DRIVE
672 HC 2
*

673 KK RCP25
674 KM ROUTE CP25 TO C5CE
675 KM APPALOOSA ROAD
676 RD 2640 .020 .016 TRAP 50 0
*

677 KK C5CE
678 KM PART OF 1998 LOMR C5Cab
679 BA .3244
680 PB 3.29
681 LS 0 68
682 UD .08
*

683 KK CP26
684 KM COMBINE RCP25 AND C5CE
685 KM APPALOOSA ROAD AND EQUESTRIAN
686 HC 2
*

```

1

HEC-1 INPUT

PAGE 20

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

687 KK RCP26
688 KM ROUTE CP26 TO C5CD
689 KM EQUESTRIAN DRIVE
690 RD 1200 .016 .016 TRAP 50 0
*

691 KK C5CD
692 KM PART OF 1998 LOMR C5CAa AND C5Cab
693 BA .2668
694 PB 3.31
695 LS 0 73
696 UD .34
*

697 KK RET1
698 KM RETRIEVE DIVERSION 1 FROM C5GD
699 DR DIVER1
*

700 KK RDIV1
701 KM ROUTE DIVERSION 1 TO CP27
702 KM TYPE OF FACILITY = OVERLAND FLOW TO EX CONC CHANNEL
703 RD 2600 .019 .030 TRAP 100 1
*

704 KK RDIV1
705 KM ROUTE DIVERSION 1 TO CP27
706 KM TYPE OF FACILITY = CONCRETE CHANNEL
707 RD 1300 .014 .015 TRAP 20 1
*

```


SDN3.OUT

708 KK RDIV1
 709 KM ROUTE DIVERSION 1 TO CP27
 710 KM TYPE OF FACILITY = STREET TO EQUESTRIAN
 711 RD 2000 .014 .016 TRAP 60 1
 *
 712 KK CP27
 713 KM COMBINE RCP26, C5CD, AND RDIV1
 714 HC 3
 *
 715 KK RCP27
 716 KM ROUTE CP27 TO CP24C
 717 RD 1450 .017 .017 TRAP 100
 *
 718 KK CP24D
 719 KM COMBINE CP24C AND RCP27
 720 HC 2
 *

1

HEC-1 INPUT

PAGE 21

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

721 KK C5CB
 722 KM MODIFIED 1998 LOMR C5CB
 723 KM 2001 MPU C1-47A
 724 BA .1409
 725 PB 3.26
 726 LS 0 81
 727 UD .30
 *
 728 KK CP24E
 729 KM COMBINE CP24D AND C5CB
 730 HC 2
 *
 731 KK C5FD
 732 KM 1998 LOMR C5FD
 733 BA .1706
 734 PB 3.43
 735 LS 0 83
 736 UD .07
 *
 737 KK RC5FD
 738 KM ROUTE C5FD TO C5FB
 739 RD 2500 .02 .040 0 TRAP 50 2
 *
 740 KK C5FA
 741 KM 1998 LOMR C5FA
 742 BA .5071
 743 PB 3.43
 744 LS 0 87
 745 UD .02
 *
 746 KK RC5FA
 747 KM ROUTE C5FA TO C5FB
 748 RD 4600 .065 .040 0 TRAP 100 1
 *
 749 KK C5FB
 750 KM 1998 LOMR C5FB
 751 BA .2592
 752 PB 3.43
 753 LS 0 69
 754 UD .17
 *
 755 KK CP28
 756 KM COMBINE RC5FD, RC5FA, AND C5FB
 757 HC 3
 *

1

HEC-1 INPUT

PAGE 22

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

758 KK RCP28
 759 KM ROUTE CP28 TO C5FC
 760 KM FACILITY = C-1 CHANNEL - EQUESTRIAN LEVEE
 761 KM FACILITY # = C1EQ 0297
 762 KM TYPE OF FACILITY = ROCK LEVEE
 763 RD 2000 0.019 .040 0 TRAP 50 3
 *
 764 KK C5FC
 765 KM 1998 LOMR C5FC
 766 KM 2001 MPU C1-37
 767 BA .2222
 768 PB 3.43
 769 LS 0 73
 770 UD 0.16
 *
 771 KK CP29
 772 KM COMBINE RCP28 AND C5FC
 773 HC 2
 *
 774 KK RCP29
 775 KM ROUTE CP29 TO C5EA
 776 KM FACILITY = C-1 CHANNEL - EQUESTRIAN LEVEE
 777 KM FACILITY # = C1EQ 0297
 778 KM TYPE OF FACILITY = ROCK LEVEE
 779 RD 1900 0.018 .040 0 TRAP 100 3
 *
 780 KK C5EA
 781 KM 1998 LOMR C5EA
 782 KM 2001 MPU C1-38
 783 BA .4873
 784 PB 3.43
 785 LS 0 82
 786 UD 0.12
 *
 787 KK CP30
 788 KM COMBINE RCP29 AND C5EA
 789 HC 2
 *
 790 KK RCP30
 791 KM ROUTE CP30 TO C5EC
 792 KM FACILITY = C-1 CHANNEL - EQUESTRIAN LEVEE

SDN3.OUT

793 KM FACILITY # = C1EQ 0297

794 KM TYPE OF FACILITY = ROCK LEVEE

795 RD 1600 0.017 .040 0 TRAP 100 3

1 HEC-1 INPUT PAGE 23

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

796 KK C5EB

797 KM 1998 LOMR C5EB

798 BA .5469

799 PB 3.43

800 LS 0 88

801 UD .21

802 KK RC5EB

803 KM ROUTE C5EB TO C5EC

804 RD 3500 0.040 .040 0 TRAP 50 3

805 KK C5EC

806 KM 1998 LOMR C5EC

807 BA .2214

808 PB 3.43

809 LS 0 71

810 UD .14

811 KK CP31

812 KM COMBINE RC5EB, C5EC, AND RCP30

813 HC 3

814 KK RCP31

815 KM ROUTE CP31 TO C5ED

816 KM FACILITY = C-1 CHANNEL - EQUESTRIAN LEVEE

817 KM FACILITY # = C1EQ 0297

818 KM TYPE OF FACILITY = ROCK LEVEE

819 RD 2500 0.020 .040 0 TRAP 35 3

820 KK C5ED

821 KM 1998 LOMR C5ED

822 KM 2001 MPU C1-41

823 BA .1578

824 PB 3.41

825 LS 0 79

826 UD 0.17

827 KK CP32

828 KM COMBINE RCP31 AND C5ED

829 HC 2

830 KK RCP32

831 KM ROUTE CP32 TO C5DA

832 KM FACILITY = C-1 CHANNEL - EQUESTRIAN LEVEE

833 KM FACILITY # = C1EQ 0349

834 KM TYPE OF FACILITY = ROCK LEVEE

835 RD 1000 0.020 .040 0 TRAP 35 3

1 HEC-1 INPUT PAGE 24

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

836 KK C5DA

837 KM 1998 LOMR C5DA

838 KM 2001 MPU C1-42

839 BA 1.063

840 PB 3.42

841 LS 0 86

842 UD 0.05

843 KK C5DB

844 KM 1998 LOMR C5DB

845 KM 2001 MPU C1-43

846 BA .5321

847 PB 3.40

848 LS 0 88

849 UD 0.07

850 KK CP33

851 KM COMBINE RCP32, C5DA, C5DB

852 HC 3

853 KK RCP33

854 KM ROUTE CP33 TO C5CB

855 KM FACILITY = C-1 CHANNEL - EQUESTRIAN CHANNEL

856 KM FACILITY # = C1EQ 0297

857 KM TYPE OF FACILITY = CONCRETE TRAP CHANNEL

858 RD 5000 0.027 .013 0 TRAP 20 1

859 KK CP24

860 KM COMBINE RCP33 AND CP24E

861 HC 2

862 KK RCP24

863 KM ROUTE CP24 TO CP34

864 KM FACILITY = MAGIC WAY

865 KM TYPE OF FACILITY = STEET

866 RD 3000 0.010 .016 0 TRAP 20 1

867 KK C5DC

868 KM MODIFIED 1998 LOMR SUBBASIN C5DC

869 PB 3.31

870 BA .3264

871 LS 0 83

872 UD .02

1 HEC-1 INPUT PAGE 25

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

873 KK RC5DC

874 KM ROUTE C5DC TO C4BD

875 RD 6600 .024 .040 0 TRAP 100

```

876 KK C4BD
877 KM MODIFIED 1998 LOMR SUBBASIN C5DC
878 KM 2001 MPU C1-47
879 BA .5243
880 PB 3.23
881 LS 0 82
882 UD 0.42
*
883 KK CP34A
884 KM COMBINE RC4BF, C4BD, AND C5DC
885 HC 2
*
886 KK CP34B
887 KM COMBINE RCP24 AND CP34A
888 KM EQUESTRIAN DETENTION BASIN
889 HC 2
*
* THE EQUESTRIAN DETENTION BASIN STAGE/DISCHARGE AND STAGE/VOLUME RELATIONSHIPS
* WERE CHECKED AGAINST THE LATEST RECORD DRAWINGS AND PREDESIGN REPORTS.
* THE FOLLOWING INPUT REFLECTS RECORD DRAWING INFORMATION
*
890 KK DB4
891 KM FACILITY = EQUESTRIAN DETENTION BASIN
892 KM FACILITY # = C1EQ 0159
893 KM STORAGE VOLUME = 409 AC-FT, (100-YR PEAK STAGE AT EL = 2069, W/O FREEBOARD)
894 KM OUTLET = 48" RCP
895 KO 3
896 RS 1 STOR 0
897 SV 0 2 13 31 61 97 118 140 171 200
898 SV 229 261 290 315 344 379 409 437 470 504
899 SE 2048 2050 2052 2054 2056 2058 2059 2060 2061 2062
900 SE 2063 2064 2065 2066 2067 2068 2069 2070 2071 2072
901 SQ 0 37 80 117 142 163 173 182 191 198
902 SQ 206 213 221 228 235 248 2755 7761 14467
903 SS 2069 900 3.0 1.5
*
* *****END OF 1998 LOMR INPUT*****
*
*
*

```

1

HEC-1 INPUT

PAGE 26

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

904 KK C4BF
905 KM PART OF 1998 LOMR SUBBASIN C5DC
906 PB 3.21
907 BA .2776
908 LS 0 81
909 UD .06
*
910 KK RC4BF
911 KM ROUTE C4BF TO C4BC
912 RD 3100 .020 .033 0 TRAP 100.0
*
913 KK C4BC
914 KM SUBBASIN C4BC
915 PB 3.15
916 BA .2402
917 LS 0 82
918 UD .19
*
919 KK CP34
920 KM COMBINE CP34B, C4BC, AND RC4BF
921 HC 3
*
922 KK RCP34
923 KM ROUTE CP34 TO C4A1C ALONG EQUESTRIAN OUTFALL
924 KM FACILITY = C-1 CHANNEL - EQUESTRIAN DETENTION BASIN OUTFALL
925 KM FACILITY # C1EQ 0078, 0112, 0139
926 RD 3600 .018 .030 0 TRAP 100
*
927 KK C4A1C
928 KM 2001 MPU C1-49
929 BA .5200
930 PB 3.07
931 LS 0 82
932 UD .25
*
933 KK RET5
934 KM RETRIEVE DIVERSION 5
935 DR DIVER5
*
936 KK RDIV5
937 KM ROUTE DIV5 ALONG RACE TRACK ROAD TO NEWPORT
938 KM FACILITY = STREET
939 RD 5000 .024 .016 0 TRAP 100
*

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HEC-1 INPUT

PAGE 27

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

940 KK CP35A
941 KM COMBINE RDIV5, RCP34, AND C4A1C
942 KM RACETRACK AND NEWPORT
943 HC 3
*
944 KK C4A1
945 KM 2001 MPU C1-50
946 BA .3493
947 PB 3.07
948 LS 0 79
949 UD .32
*
950 KK CP35
951 KM COMBINE CP35A AND C4A1
952 HC 2
*
953 KK RCP35
954 KM ROUTE TO C4A1B
955 KM OVERLAND FLOW
956 KM C-1 CHANNEL AT BURKHOLDER

```

957 RD 3500 .02 .030 TRAP 100 SDN3.OUT
*

958 KK C4BE
959 KM NOT A PART OF THE 1998 LOMR
960 PB 3.17
961 BA .2206
962 LS 0 85
963 UD 0.26
*

964 KK RC4BE
965 KM ROUTE C4BE TO C4BB
966 RD 3400 .036 .030 TRAP 100
*

967 KK C4BB
968 BA .3477
969 PB 3.09
970 LS 0 87
971 UD 0.29
*

972 KK CP36
973 KM COMBINE RC4BE AND C4BB
974 HC 2
*

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HEC-1 INPUT

PAGE 28

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

975 KK RCP36
976 KM ROUTE CP36 TO C4A2B
977 KM ROUTE TO BURKHOLDER AND RACETRACK
978 RD 2640 0.033 0.016 0 TRAP 0 50
*

979 KK C4A2B
980 KM 2001 MPU C1-52
981 BA .2491
982 PB 3.03
983 LS 0 75
984 UD 0.10
*

985 KK CP37
986 KM COMBINE RC4BB AND C4A2B
987 KM RACETRACK ROAD @ BURKHOLDER BOULEVARD
988 HC 2
*

989 KK RCP37
990 KM ROUTE CP37 TO C4A1B ALONG BURKHOLDER
991 RD 2700 0.033 0.016 0 TRAP 0 50
*

992 KK CP38A
993 KM COMBINE CP35 AND RCP37 AT BURKHOLDER AND PUEBLO
994 HC 2
*

995 KK C4A1B
996 KM 2001 MPU C1-53
997 BA .2492
998 PB 2.98
999 LS 0 72
1000 UD .20
*

1001 KK CP38
1002 KM COMBINE RCP22, CP38A, AND C4A1B @ BURKHOLDER AND PUEBLO
1003 HC 3
*

1004 KK RCP38
1005 KM ROUTE CP38 TO CP45
1006 RD 2200 0.021 0.015 0 TRAP 10 02
*

1007 KK C4CB
1008 KM 2001 MPU C1-54
1009 BA 5.408
1010 PB 3.43
1011 LS 0 85
1012 UD 0.06
*

*
*
* THE EAST C-1 DETENTION BASIN STAGE/STORAGE AND STAGE/DISCHARGE RELATIONSHIPS
* WERE CHECKED AGAINST THE LATEST RECORD DRAWINGS AND PREDESIGN REPORTS.
* THE FOLLOWING INPUT WAS DIGITIZED FROM RECORD DRAWINGS AS THE HEC-1 INPUT
* WAS NOT AVAILABLE. THE RECORD DRAWINGS DIFFERED SLIGHTLY FROM THE
* PREDESIGN INPUT.
*
*
*

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HEC-1 INPUT

PAGE 29

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1013 KK DB5
1014 KM FACILITY = EAST C-1 DETENTION BASIN
1015 KM FACILITY # = CLIT 0492
1016 KM STORAGE VOLUME = 400 AC-FY (100-YR PK STAGE WSE = 2485.3)
1017 KM OUTLET = 48" RCP
1018 KO 3
1019 RS 1 STOR -1
1020 SV 1.2 3.3 12.1 28.0 49.0 79.8 115.0 166.1 232.2 320.1
1021 SV 418.8 534.5 605.5 681.1 765.1 846.8 943.4 1044.8 1261.8 1426.1
1022 SE 2446.0 2450.0 2454.0 2458.0 2462.0 2466.0 2470.0 2474.0 2478.0 2482.0
1023 SE 2486.0 2490.0 2492.0 2494.0 2496.0 2498.0 2500.0 2502 2506.0 2510.0
1024 SQ 0.5 22.9 36.1 45.7 53.6 60.4 66.5 72.3 77.5 82.4
1025 SQ 87.0 91.2 93.5 95.6 97.6 99.5 101.4 103.4 107.2 110.7
1026 SE 2446.0 2450.0 2454.0 2458.0 2462.0 2466.0 2470.0 2474.0 2478.0 2482.0
1027 SE 2486.0 2490.0 2492.0 2494.0 2496.0 2498.0 2500.0 2502 2506.0 2510.0
*

1028 KK RDB5
1029 KM ROUTE DB5 TO C4CA
1030 KM FACILITY = EAST C-1 DETENTION BASIN LEVEE
1031 KM FACILITY # = CIDK 0226
1032 KM TYPE OF FACILITY = SOIL CEMENT LEVEE
1033 RD 5300 .034 .025 0 TRAP 50 2
*

1034 KK C4CA
1035 KM PART OF 2001 MPU C1-55

1036 BA .1964
 1037 PB 3.43
 1038 LS 0 85
 1039 UD 0.27
 *

1040 KK C3B3E
 1041 KM PART OF 2001 MPU C1-55
 1042 BA .2225
 1043 PB 3.43
 1044 LS 0 90
 1045 UD .16
 *

1046 KK CP39
 1047 KM COMBINE C4CA, C3B3E, AND RDB5
 1048 HC 3
 *

1049 KK RCP39
 1050 KM ROUTE CP39 TO C3B3D 0 TRAP 50 2
 1051 RD 2650 .023 .025
 *

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HEC-1 INPUT

PAGE 30

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1052 KK C3B3D
 1053 KM PART OF 2001 MPU C1-55
 1054 PB 3.43
 1055 BA .2554
 1056 LS 0 89
 1057 UD .14
 *

1058 KK CP40
 1059 KM COMBINE RCP39 AND C3B3D
 1060 HC 2
 *

1061 KK RCP40
 1062 KM ROUTE TO CP42
 1063 RD 1400 .05 .025 TRAP 50 3
 *

1064 KK C3B3C
 1065 KM PART OF 2001 MPU C1-65
 1066 BA 1.238
 1067 PB 3.50
 1068 LS 0 88
 1069 UD 0.07
 *

1070 KK RC3B3C
 1071 KM ROUTE C3B3C TO C3B3B
 1072 RD 2300 .024 .030 TRAP 100 3
 *

1073 KK C3B3B
 1074 KM PART OF 2001 MPU C1-65
 1075 BA .3220
 1076 PB 3.43
 1077 LS 0 87
 1078 UD 0.17
 *

1079 KK CP41
 1080 KM COMBINE C3B3C AND C3B3B
 1081 HC 2
 *

1082 KK RCP41
 1083 KM ROUTE TO C3B3A
 1084 RD 6300 .05 .030 TRAP 100 3
 *

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HEC-1 INPUT

PAGE 31

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1085 KK C3B3A
 1086 BA .5107
 1087 PB 3.43
 1088 LS 0 85
 1089 UD 0.10
 *

1090 KK CP42
 1091 KM COMBINE RCP41, RCP40, AND C3B3A
 1092 HC 3
 *

1093 KK RCP42
 1094 KM ROUTE CP42 TO CP43 @ MAGIC WAY AND DRAKE CHANNEL
 1095 KM OVERLAND FLOW THROUGH C4BA2
 1096 RD 5300 .015 .030 TRAP 100 3
 *

1097 KK C4BA2
 1098 KM PART OF 2001 MPU C1-46
 1099 BA .1351
 1100 PB 3.43
 1101 LS 0 74
 1102 UD .16
 *

1103 KK CP43A
 1104 KM COMBINE C4BA2 AND RCP42
 1105 HC 2
 *

1106 KK RCP43
 1107 KM ROUTE CP43 TO C4A2A ALONG DRAKE CHANNEL
 1108 KM FACILITY = C-1 CHANNEL - DRAKE CHANNEL
 1109 KM FACILITY # - C1DC 0051
 1110 KM TYPE OF FACILITY = EARTHEN W\ GABION DROPS
 1111 RD 2640 .029 .030 TRAP 20 2
 *

1112 KK C4BA3
 1113 KM PART OF 2001 MPU C1-46
 1114 BA .4069
 1115 PB 3.43
 1116 LS 0 78
 1117 UD .41
 *

1118 KK RC4BA3

1119 KM ROUTE C4BA3 TO C4A2A SDN3.OUT
 1120 RD 2900 .031 .030 TRAP 200
 1121 *
 1 HEC-1 INPUT PAGE 32

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1122 KK C4A2A
 1123 KM 2001 MPU C1-57
 1124 BA .2607
 1125 PB 3.05
 1126 LS 0 77
 1127 UD .04
 *
 1128 KK CP44
 1129 KM COMBINE C4A2A, RCP43, AND RC4BA3
 1130 KM DRAKE AND RACETRACK
 1131 HC 3
 *
 1132 KK RCP44
 1133 KM ROUTE CP44 TO C4A1A
 1134 KM FACILITY = C-1 CHANNEL -DRAKE CHANNEL
 1135 KM TYPE OF FACILITY = CONCRETE CHANNEL
 1136 RD 2640 .021 .015 TRAP 10 2
 *
 1137 KK C4A1A
 1138 KM 2001 MPU C1-58
 1139 BA .2544
 1140 PB 2.92
 1141 LS 0 79
 1142 UD .66
 *
 1143 KK CP45
 1144 KM COMBINE RCP44, RCP38, AND C4A1A
 1145 KM CONFLUENCE OF C1 CHANNEL AND DRAKE CHANNEL
 1146 HC 3
 *
 1147 KK RCP45
 1148 KM ROUTE CP45 TO C3B1C
 1149 KM FACILITY = C-1 CHANNEL
 1150 KM FACILITY # = C1CH 0321
 1151 KM TYPE OF FACILITY = CONCRETE CHANNEL
 1152 RD 2640 .025 .015 TRAP 15 1
 *
 1153 KK C3A2B
 1154 KM PART OF 2001 MPU C1-65
 1155 BA .5139
 1156 PB 3.23
 1157 LS 0 86
 1158 UD .13
 *

1 HEC-1 INPUT PAGE 33

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1159 KK RC3A2B
 1160 KM ROUTE C3A2B TO CP46
 1161 KM FACILITY = OVERLAND FLOW
 1162 RD 4100 .030 .030 TRAP 100 1
 *
 1163 KK C4BA1
 1164 KM PART OF 2001 MPU C1-62
 1165 BA .4758
 1166 PB 2.99
 1167 LS 0 74
 1168 UD .21
 *
 1169 KK CP46
 1170 KM COMBINE RC3A2B AND C4BA1
 1171 HC 2
 *
 1172 KK RCP46
 1173 KM ROUTE CP46 TO C3B1D
 1174 KM OVERLAND FLOW TO RACETRACK
 1175 RD 2640 .03 .03 TRAP 100 3
 *
 1176 KK C3B1D
 1177 KM 2001 MPU C1-60
 1178 BA .2455
 1179 PB 2.93
 1180 LS 0 73
 1181 UD .05
 *
 1182 KK CP47
 1183 KM COMBINE RC4BA1 AND C3B1D
 1184 KM RACETRACK AND WARM SPRINGS
 1185 HC 2
 *
 1186 KK RCP47
 1187 KM ROUTE CP47 TO C3B1C
 1188 KM WARM SPRINGS ROAD AND PUEBLO
 1189 RD 2640 .025 .016 TRAP 0 50
 *
 1190 KK C3B1C
 1191 KM 2001 MPU C1-61
 1192 BA .2434
 1193 PB 2.87
 1194 LS 0 84
 1195 UD .04
 *

1 HEC-1 INPUT PAGE 34

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1196 KK CP48
 1197 KM COMBINE RCP45, C3B1C, AND RCP46
 1198 HC 3
 *
 1199 KK RCP48
 1200 KM ROUTE CP47 TO C3B1A
 1201 KM FACILITY = C-1 CHANNEL
 1202 KM FACILITY # C1CH 0284, 0340

SDN3.OUT

1203	KM	TYPE OF FACILITY = CONCRETE CHANNEL			
1204	RD	2640 .025 .015 TRAP	15	1	
1205	KK	C3B1B			
1206	KM	PART OF 2001 MPU C1-67			
1207	BA	.2094			
1208	PB	2.92			
1209	LS	0 76			
1210	UD	.20			
1211	KK	RC3B1B			
1212	KM	ROUTE C3B1B TO C3B1A			
1213	KM	ITHACA AVENUE AND PUEBLO			
1214	RD	2640 .025 .016 TRAP	0	50	
1215	KK	C3B1A			
1216	KM	2001 MPU C1-63			
1217	PB	2.85			
1218	BA	.2435			
1219	LS	0 78			
1220	UD	.21			
1221	KK	CP49			
1222	KM	COMBINE C3B1A, RC3B1B, AND RCP48			
1223	HC	3			
1224	KK	RCP49			
1225	KM	ROUTE CP49 TO C3A1A			
1226	KM	FACILITY = C-1 CHANNEL			
1227	KM	FACILITY # C1CH 0220, 0269			
1228	KM	TYPE OF FACILITY = CONCRETE CHANNEL			
1229	RD	3960 .025 .015 TRAP	15	1	
1230	KK	C3A2A			
1231	KM	PART OF 2001 MPU C1-66			
1232	BA	.4708			
1233	PB	3.23			
1234	LS	0 88			
1235	UD	.09			

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HEC-1 INPUT

PAGE 35

LINE	ID	1	2	3	4	5	6	7	8	9	10
1236	KK	RC3A2A									
1237	KM	ROUTE C3A2A TO C3A1B									
1238	KM	OVERLAND FLOW									
1239	RD	7900 .03 .030 TRAP	0	100	3						
1240	KK	C3A1B									
1241	KM	PART OF 2001 MPU C1-66									
1242	BA	1.018									
1243	PB	3.23									
1244	LS	0 81									
1245	UD	.08									
1246	KK	CP50									
1247	KM	COMBINE C3A1B, RC3A2A, AND CP49									
1248	HC	2									
1249	KK	RCP50									
1250	KM	ROUTE CP50 TO C3A1A									
1251	KM	ITHACA									
1252	RD	2600 .019 .016 TRAP	50								
1253	KK	C3A1A									
1254	KM	PART OF 2001 MPU C1-64									
1255	BA	.3744									
1256	PB	2.84									
1257	LS	0 81									
1258	UD	.07									
1259	KK	CP51									
1260	KM	COMBINE C3A1A, RCP50, AND RCP49 - C-1 CHANNEL AND LAKE MEAD DRIVE									
1261	HC	3									
1262	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

56      C1H
      V
      V
69      DB1
      V
84      RDB1
      .
      .
90      C1HB1
      .
      .
96      CP2.....
      V
      V
99      RCP2
      .
      .
105     C1G3A
      .
      .
111     CP3.....
      V
      V
114     RCP3
      .
      .
120     C1G3B
      .
      .
126     CP4.....
      V
      V

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129      RCP4
135      .      C1G3C
141      CP5.....
145      .      C1G3D
151      CP6A.....
155      .      C5ICB
161      .      C5ICB
166      .      C5I2A
172      .      CP6B.....
175      CP6.....
179      DB2
194      RDB2
200      .      C1G2C
206      .      C1G2D
212      CP7A.....
216      .      C1G2B1
222      .      RG2B1
226      .      C1G2B2
232      .      CP7B.....
236      .      C1G2A
242      .      RC1G2A
246      .      CP7C.....
250      CP7.....
254      CP7DB
270      CP7DB
285      RCP7
290      .      C1NA
296      .      RC1NA
301      CP8.....
304      RCP8
308      .      C5GC
314      .      RC5GC
317      .      C5GB
323      .      CP9.....
326      .      RCP9
329      .      C5GA
335      .      CP10.....
338      .      RCP10
342      .      RCP10
345      .      C5GD
353      .      DIVER1-----> DIVER1
356      .      R5GD
359      .      C5I1E

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365      CP11 .....
366      V
368      RCP11 .....
371      C1HF .....
372      V
377      CP12 .....
378      V
380      RCP12 .....
383      C5I1B .....
384      V
389      RC5I1B .....
392      C5I1D .....
393      V
398      CP13 .....
399      V
401      RCP13 .....
404      C1HE .....
410      CP14 .....
416      DIVER2 -----> DIVER2
417      V
419      RCP14 .....
422      C1HD .....
423      V
428      CP15 .....
429      V
431      RCP15 .....
436      DIVER3 -----> DIVER3
437      V
439      C5I1 .....
440      V
445      C5I1C .....
446      V
451      RC5I1C .....
452      V
454      CP16 .....
455      V
457      RCP16 .....
460      C1G1B .....
461      V
466      CP17 .....
467      V
469      RCP17 .....
472      C1HCB .....
473      V
478      CP18A .....
481      CP18 .....
482      V
487      DIVER4 -----> DIVER4
488      V
490      RCP18 .....
493      C1G1A .....
494      V
499      RC1G1A .....
503      C1HB .....
504      V
509      CP19A .....
512      CP19 .....
513      V
517      DIVER5 -----> DIVER5
518      V
520      RCP19 .....
523      C1HA .....
524      V
530      CP20A .....
533      CP20 .....
534      V
536      RCP20 .....

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542      .      .      C1D
548      .      .      V
548      .      .      RC1D
552      .      .      .      C1C
558      .      .      CP21
561      .      .      V
561      .      .      RCP21
564      .      .      .      C1B
570      .      .      .      .      C4A1D
576      .      .      .      .      V
576      .      .      .      .      RC4A1D
579      .      .      .      .      .
582      .      .      .      .      .
588      .      .      .      .      .
594      .      .      .      .      .
597      .      .      .      .      .
603      .      .      .      C5CC
611      .      .      .      .      .
609      .      .      .      .      .
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687      .      .      .      .      .
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697      .      .      .      .      .
700      .      .      .      .      .
704      .      .      .      .      .
708      .      .      .      .      .
712      .      .      .      .      .
715      .      .      .      .      .

```

RET4 ←----- DIVER4
 RDIV4
 RDIV4
 CP24A
 RET3 ←----- DIVER3
 RDIV3
 RDIV3
 CP24B
 RET2 ←----- DIVER2
 RDIV2
 RDIV2
 CP24C
 C5CA
 RC5CA
 C5CF
 CP25
 RCP25
 C5CE
 CP26
 RCP26
 C5CD
 RET1 ←----- DIVER1
 RDIV1
 RDIV1
 RDIV1
 RDIV1
 CP27
 RCP27


```

718      . CP24D.....
721      .         C5CB
728      . CP24E.....
731      .         C5FD
737      .         V
740      .         RCP28
746      .         C5FA
749      .         V
755      .         RCP28
764      .         C5FC
771      .         CP29.....
774      .         V
780      .         RCP29
787      .         C5EA
790      .         CP30.....
796      .         V
802      .         RCP30
805      .         C5EB
811      .         V
814      .         RCP31
820      .         C5ED
827      .         CP32.....
830      .         V
836      .         RCP32
843      .         C5DA
850      .         C5DB
853      .         CP33.....
859      .         V
862      .         RCP33
867      .         CP24.....
873      .         V
876      .         RCP24
883      .         C5DC
886      .         V
890      .         RCP24
904      .         C5DB
910      .         V
913      .         RCP24
919      .         C4BD
922      .         CP34A.....
927      .         CP34B.....
933      .         V
935      .         DB4
938      .         C4BF
941      .         V
944      .         RCP34
947      .         C4BC
950      .         CP34.....
953      .         V
956      .         RCP34
959      .         C4A1C
962      .         RET5
965      .         V
968      .         <----- DIVERS
971      .
974      .
977      .
980      .
983      .
986      .
989      .
992      .
995      .
998      .

```

SDN3.OUT

936	.	.	.	V
	.	.	.	RDIV5
940	.	CP35A	.	.
944	.	.	C4A1	.
950	.	CP35	.	.
	.	V	.	.
953	.	RCP35	.	.
958	.	.	C4BE	.
	.	.	V	.
964	.	.	RC4BE	.
967	.	.	.	C4BB
	.	.	.	.
972	.	.	CP36	.
	.	.	V	.
975	.	.	RCP36	.
	.	.	.	.
979	.	.	.	C4A2B
985	.	.	CP37	.
	.	.	V	.
989	.	.	RCP37	.
992	.	CP38A	.	.
995	.	.	C4A1B	.
1001	.	CP38	.	.
	.	V	.	.
1004	.	RCP38	.	.
1007	.	C4CB	.	.
	.	V	.	.
1013	.	DB5	.	.
	.	V	.	.
1028	.	RDB5	.	.
1034	.	.	C4CA	.
	.	.	.	.
1040	.	.	.	C3B3E
1046	.	CP39	.	.
	.	V	.	.
1049	.	RCP39	.	.
1052	.	.	C3B3D	.
	.	.	.	.
1058	.	CP40	.	.
	.	V	.	.
1061	.	RCP40	.	.
1064	.	.	C3B3C	.
	.	.	V	.
1070	.	.	RC3B3C	.
	.	.	.	.
1073	.	.	.	C3B3B
	.	.	.	.
1079	.	.	CP41	.
	.	.	V	.
1082	.	.	RCP41	.
	.	.	.	.
1085	.	.	.	C3B3A
1090	.	CP42	.	.
	.	V	.	.
1093	.	RCP42	.	.
1097	.	.	C4BA2	.
1103	.	CP43A	.	.
	.	V	.	.
1106	.	RCP43	.	.
1112	.	.	C4BA3	.
	.	.	V	.
1118	.	.	RC4BA3	.
	.	.	.	.
1122	.	.	.	C4A2A
1128	.	CP44	.	.
	.	V	.	.
1132	.	RCP44	.	.

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1137      .      .      C4A1A
1143      CP45 .....
1147      RCP45
1153      .      C3A2B
1159      .      RC3A2B
1163      .      .      C48A1
1169      .      CP46 .....
1172      .      RCP46
1176      .      .      C3B1D
1182      .      CP47 .....
1186      .      RCP47
1190      .      .      C3B1C
1196      .      CP48 .....
1199      .      RCP48
1205      .      C3B1B
1211      .      RC3B1B
1215      .      .      C3B1A
1221      .      CP49 .....
1224      .      RCP49
1230      .      C3A2A
1236      .      RC3A2A
1240      .      .      C3A1B
1246      .      CP50 .....
1249      .      RCP50
1253      .      .      C3A1A
1259      .      CP51 .....

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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1 *****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 12NOV02 TIME 17:28:02 *
* *****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
* *****

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***** C-1 WATERSHED FIS RESTUDY *****

***** PREPARED FOR: CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT *****
 ** CLARK COUNTY, NEVADA **

***** PREPARED BY: CARTER BURGESS AND SOUTHWEST FLUVIAL SYSTEMS *****

EXISTING CONDITIONS DRAINAGE SYSTEM
 INPUT FILE = SDN3.DAT
 INPUT FILE DATE = NOV 2002
 DESIGN STORM = 100-YEAR 6-HR STORM
 STORM DISTRIBUTION = SDN #3

REFERENCED HYDROLOGIC MODELS:
 PREDESIGN REPORT FOR THE BLACK MOUNTAIN AND MISSION HILLS DETENTION BASINS
 AND OUTFALL STRUCTURES (VTN 1992)
 SNWA RIVER MOUNTAINS WATER TREATMENT FACILITY DRAFT TECHNICAL DRAINAGE STUDY
 (MONTGOMERY WATSON/CH2MHILL 1997)
 EAST C-1 DETENTION BASIN FINAL DESIGN (VTN 1998)
 DESIGN MEMORANDUM FOR THE EQUESTRIAN DETENTION BASIN (POGGEMEYER 1994)
 DESIGN CALCULATION NOTEBOOK FOR THE BLACK MOUNTAIN DETENTION BASIN
 (VTN 1998)
 CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2002 MASTER PLAN UPDATE (LBA)
 1-515 BOULDER HIGHWAY TO LAKE MEAD DRIVE DRAINAGE STUDY (SVERDRUP, 1991)

3R CARDS CONTAINED DARFS BASED ON THE FOLLOWING VALUES:

AREA SQ.MI.	DARF
0 - 5	0.950
5 - 12	0.880
12 - 16	0.832
16 - 20	0.804
20 - 30	0.765
30 - 40	0.725

THE FOLLOWING REDUCTION FACTORS ARE USED FOR MODIFIED USLE COMPUTATIONS

2-YR	0.260
5-YR	0.440
10-YR	0.570
25-YR	0.765
50-YR	0.880

54 IO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN	5	MINUTES IN COMPUTATION INTERVAL
IDATE	1	STARTING DATE
ITIME	0000	STARTING TIME
NQ	300	NUMBER OF HYDROGRAPH ORDINATES
NDDATE	2	ENDING DATE
NDTIME	0055	ENDING TIME
ICENT	19	CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA	SQUARE MILES
PRECIPITATION DEPTH	INCHES
LENGTH, ELEVATION	FEET
FLOW	CUBIC FEET PER SECOND
STORAGE VOLUME	ACRE-Feet
SURFACE AREA	ACRES
TEMPERATURE	DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.95 .88 .83 .80 .76 .73 .57 .44 .26

*** **

69 KK *****
* DB1 *
* *

74 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

75 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	STOR	TYPE OF INITIAL CONDITION
RSVRIC	-1.00	INITIAL CONDITION
X	.00	WORKING R AND D COEFFICIENT

76 SV	STORAGE	.0	1.2	4.6	10.3	22.6	38.7	54.9	73.4	92.6	113.5
		135.2	158.2	183.2	208.1	234.7	262.5	292.0	325.3		
78 SE	ELEVATION	2556.00	2558.00	2560.00	2562.00	2564.00	2566.00	2568.00	2570.00	2572.00	2574.00
		2576.00	2578.00	2580.00	2582.00	2584.00	2586.00	2588.00	2590.00		
80 SQ	DISCHARGE	0.	1.	27.	58.	78.	95.	109.	121.	132.	142.
		151.	160.	169.	177.	184.	191.	198.	205.		
82 SE	ELEVATION	2556.00	2558.00	2560.00	2562.00	2564.00	2566.00	2568.00	2570.00	2572.00	2574.00
		2576.00	2578.00	2580.00	2582.00	2584.00	2586.00	2588.00	2590.00		

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	1.19	4.55	10.32	22.58	38.69	54.90	73.42	92.55	113.51
OUTFLOW	.00	1.28	27.31	57.88	77.52	95.42	108.73	120.50	131.87	141.78
ELEVATION	2556.00	2558.00	2560.00	2562.00	2564.00	2566.00	2568.00	2570.00	2572.00	2574.00
STORAGE	135.16	158.22	183.23	208.10	234.67	262.55	292.02	325.32		
OUTFLOW	150.74	159.67	168.97	176.60	183.71	190.74	197.77	204.93		
ELEVATION	2576.00	2578.00	2580.00	2582.00	2584.00	2586.00	2588.00	2590.00		

*** **

HYDROGRAPH AT STATION DB1
FOR PLAN 1, RATIO = .95

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)				
+	198.	5.33			
	(CFS)	191.	146.	141.	141.
	(INCHES)	.443	1.356	1.356	1.356
	(AC-FT)	95.	290.	290.	290.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)				
+	294.	5.33			
		264.	152.	146.	146.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)				
+	2588.10	5.33			
		2586.03	2576.45	2575.70	2575.70
	CUMULATIVE AREA =		4.01 SQ MI		

*** **

HYDROGRAPH AT STATION DB1
FOR PLAN 1, RATIO = .88

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW
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								SDN3.OUT
+	(CFS)	(HR)		6-HR	24-HR	72-HR	24.92-HR	
+	190.	5.33	(CFS)	182.	135.	130.	130.	
			(INCHES)	.423	1.256	1.256	1.256	
			(AC-FT)	90.	268.	268.	268.	
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR		
+	258.	5.33		229.	126.	121.	121.	
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE		
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR		
+	2585.67	5.33		2583.56	2574.20	2573.53	2573.53	
CUMULATIVE AREA =				4.01 SQ MI				
***	***	***	***	***	***	***	***	
HYDROGRAPH AT STATION DB1								
FOR PLAN 1, RATIO = .83								
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW		
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR		
+	184.	5.33	(CFS)	176.	127.	123.	123.	
			(INCHES)	.408	1.181	1.181	1.181	
			(AC-FT)	87.	252.	252.	252.	
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR		
+	234.	5.33		206.	109.	105.	105.	
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE		
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR		
+	2583.94	5.33		2581.82	2572.66	2572.05	2572.05	
CUMULATIVE AREA =				4.01 SQ MI				
***	***	***	***	***	***	***	***	
HYDROGRAPH AT STATION DB1								
FOR PLAN 1, RATIO = .80								
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW		
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR		
+	180.	5.33	(CFS)	172.	122.	118.	118.	
			(INCHES)	.399	1.135	1.135	1.135	
			(AC-FT)	85.	243.	243.	243.	
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR		
+	220.	5.33		193.	100.	96.	96.	
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE		
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR		
+	2582.91	5.33		2580.80	2571.76	2571.18	2571.18	
CUMULATIVE AREA =				4.01 SQ MI				
***	***	***	***	***	***	***	***	
HYDROGRAPH AT STATION DB1								
FOR PLAN 1, RATIO = .76								
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW		
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR		
+	175.	5.33	(CFS)	166.	115.	111.	111.	
			(INCHES)	.385	1.067	1.067	1.067	
			(AC-FT)	82.	228.	228.	228.	
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR		
+	201.	5.33		176.	88.	85.	85.	
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE		
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR		
+	2581.46	5.33		2579.38	2570.52	2569.98	2569.98	
CUMULATIVE AREA =				4.01 SQ MI				
***	***	***	***	***	***	***	***	
HYDROGRAPH AT STATION DB1								
FOR PLAN 1, RATIO = .73								
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW		
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR		
+	169.	5.33	(CFS)	159.	106.	103.	103.	
			(INCHES)	.370	.988	.988	.988	
			(AC-FT)	79.	211.	211.	211.	
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR		
+	182.	5.33		158.	76.	73.	73.	
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE		
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR		
+	2579.94	5.33		2577.91	2569.22	2568.74	2568.74	
CUMULATIVE AREA =				4.01 SQ MI				
***	***	***	***	***	***	***	***	
HYDROGRAPH AT STATION DB1								
FOR PLAN 1, RATIO = .57								

SDN3.OUT

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)					
+ 142.	5.25	(CFS)	132.	69.	67.	67.
		(INCHES)	.306	.644	.644	.644
		(AC-FT)	65.	138.	138.	138.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	24.92-HR
+ (AC-FT)	(HR)					
+ 114.	5.25		94.	37.	36.	36.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	24.92-HR
+ (FEET)	(HR)					
+ 2574.00	5.25		2572.05	2564.39	2564.08	2564.08
CUMULATIVE AREA =			4.01 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION DB1
FOR PLAN 1, RATIO = .44

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)					
+ 114.	5.25	(CFS)	102.	41.	39.	39.
		(INCHES)	.237	.378	.378	.378
		(AC-FT)	51.	81.	81.	81.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	24.92-HR
+ (AC-FT)	(HR)					
+ 63.	5.25		48.	16.	15.	15.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	24.92-HR
+ (FEET)	(HR)					
+ 2568.87	5.25		2567.11	2561.09	2560.90	2560.90
CUMULATIVE AREA =			4.01 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION DB1
FOR PLAN 1, RATIO = .26

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)					
+ 61.	5.17	(CFS)	38.	10.	10.	10.
		(INCHES)	.088	.096	.096	.096
		(AC-FT)	19.	20.	20.	20.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	24.92-HR
+ (AC-FT)	(HR)					
+ 13.	5.17		7.	2.	2.	2.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	24.92-HR
+ (FEET)	(HR)					
+ 2562.37	5.17		2560.66	2558.06	2557.99	2557.99
CUMULATIVE AREA =			4.01 SQ MI			

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179 KK * DB2 *
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184 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

185 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP STOR TYPE OF INITIAL CONDITION
RSVRIC -1.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

186 SV	STORAGE	.0	2.5	15.9	40.2	72.3	107.2	185.2	273.0	371.6	480.1
		598.5	630.2								
188 SE	ELEVATION	2323.00	2326.00	2328.00	2330.00	2332.00	2334.00	2338.00	2342.00	2346.00	2350.00
		2354.00	2355.00								
190 SQ	DISCHARGE	0.	57.	109.	143.	170.	194.	234.	268.	299.	326.
		352.	358.								
192 SE	ELEVATION	2323.00	2326.00	2328.00	2330.00	2332.00	2334.00	2338.00	2342.00	2346.00	2350.00
		2354.00	2355.00								

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	2.55	15.85	40.23	72.34	107.20	185.20	273.00	371.60	480.10
OUTFLOW	.00	56.78	108.70	142.90	170.40	193.90	234.10	268.40	298.70	326.10
ELEVATION	2323.00	2326.00	2328.00	2330.00	2332.00	2334.00	2338.00	2342.00	2346.00	2350.00
STORAGE	598.50	630.20								
OUTFLOW	351.60	357.60								
ELEVATION	2354.00	2355.00								

*** *** *** *** ***

HYDROGRAPH AT STATION DB2
FOR PLAN 1, RATIO = .95

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)					

+	308.	6.08	(CFS)	304.	258.	249.	249.
			(INCHES)	.298	1.013	1.013	1.013
			(AC-FT)	150.	512.	512.	512.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR		24.92-HR
	408.	6.17		391.	286.	276.	276.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)		24-HR	72-HR		24.92-HR
	2347.36	6.08		2346.70	2341.93	2341.23	2341.23

CUMULATIVE AREA =

9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .88

DB2

PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)		24-HR	72-HR		24.92-HR
+	294.	6.08	(CFS)	289.	243.	234.	234.
			(INCHES)	.283	.954	.954	.954
			(AC-FT)	143.	482.	482.	482.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR		24.92-HR
	357.	6.08		340.	244.	235.	235.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)		24-HR	72-HR		24.92-HR
	2345.41	6.08		2344.73	2340.11	2339.48	2339.48

CUMULATIVE AREA =

9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .83

DB2

PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)		24-HR	72-HR		24.92-HR
+	284.	6.08	(CFS)	279.	232.	224.	224.
			(INCHES)	.273	.911	.911	.911
			(AC-FT)	138.	461.	461.	461.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR		24.92-HR
	323.	6.08		307.	216.	208.	208.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)		24-HR	72-HR		24.92-HR
	2344.03	6.08		2343.38	2338.85	2338.27	2338.27

CUMULATIVE AREA =

9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .80

DB2

PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)		24-HR	72-HR		24.92-HR
+	278.	6.08	(CFS)	273.	225.	217.	217.
			(INCHES)	.268	.884	.884	.884
			(AC-FT)	135.	447.	447.	447.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR		24.92-HR
	303.	6.08		287.	200.	192.	192.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)		24-HR	72-HR		24.92-HR
	2343.23	6.08		2342.58	2338.10	2337.54	2337.54

CUMULATIVE AREA =

9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .76

DB2

PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)		24-HR	72-HR		24.92-HR
+	269.	6.08	(CFS)	264.	216.	208.	208.
			(INCHES)	.259	.847	.847	.847
			(AC-FT)	131.	428.	428.	428.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)		24-HR	72-HR		24.92-HR
	276.	6.08		261.	178.	171.	171.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)		24-HR	72-HR		24.92-HR
	2342.13	6.08		2341.45	2337.05	2336.54	2336.54

CUMULATIVE AREA =

9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .73

DB2

PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE FLOW		
				24-HR	72-HR		24.92-HR

+	(CFS)	(HR)				
+	259.	6.08	(CFS)	253.	205.	198.
			(INCHES)	.249	.805	.805
			(AC-FT)	126.	407.	407.
PEAK STORAGE	TIME			6-HR	24-HR	72-HR
+	(AC-FT)	(HR)				
+	249.	6.08		235.	156.	150.
PEAK STAGE	TIME			6-HR	24-HR	72-HR
+	(FEET)	(HR)				
+	2340.92	6.08		2340.26	2335.97	2335.49
						2335.49

CUMULATIVE AREA = 9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .57

DB2

PEAK FLOW	TIME			6-HR	24-HR	72-HR
+	(CFS)	(HR)				
+	217.	6.00	(CFS)	211.	156.	150.
			(INCHES)	.207	.610	.610
			(AC-FT)	105.	308.	308.
PEAK STORAGE	TIME			6-HR	24-HR	72-HR
+	(AC-FT)	(HR)				
+	152.	6.00		140.	78.	75.
PEAK STAGE	TIME			6-HR	24-HR	72-HR
+	(FEET)	(HR)				
+	2336.32	6.00		2335.69	2331.64	2331.32
						2331.32

CUMULATIVE AREA = 9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .44

DB2

PEAK FLOW	TIME			6-HR	24-HR	72-HR
+	(CFS)	(HR)				
+	177.	5.75	(CFS)	170.	91.	88.
			(INCHES)	.166	.357	.357
			(AC-FT)	84.	180.	180.
PEAK STORAGE	TIME			6-HR	24-HR	72-HR
+	(AC-FT)	(HR)				
+	82.	5.75		72.	30.	29.
PEAK STAGE	TIME			6-HR	24-HR	72-HR
+	(FEET)	(HR)				
+	2332.56	5.75		2331.96	2327.63	2327.46
						2327.46

CUMULATIVE AREA = 9.48 SQ MI

HYDROGRAPH AT STATION
FOR PLAN 1, RATIO = .26

DB2

PEAK FLOW	TIME			6-HR	24-HR	72-HR
+	(CFS)	(HR)				
+	101.	5.42	(CFS)	79.	22.	21.
			(INCHES)	.078	.086	.086
			(AC-FT)	39.	43.	43.
PEAK STORAGE	TIME			6-HR	24-HR	72-HR
+	(AC-FT)	(HR)				
+	14.	5.42		9.	2.	2.
PEAK STAGE	TIME			6-HR	24-HR	72-HR
+	(FEET)	(HR)				
+	2327.71	5.42		2326.85	2324.07	2324.04
						2324.04

CUMULATIVE AREA = 9.48 SQ MI

*
254 KK * CP7DB *

260 KO OUTPUT CONTROL VARIABLES
IPRINT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA
261 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
STOR TYPE OF INITIAL CONDITION
RSVRIC -1.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

262 SV	STORAGE	0	.1	.7	1.9	3.9	7.0	11.2	16.1	21.5	27.2
		33.2	39.6	46.4	53.5	61.0	68.9	77.1	85.5	94.2	103.0
264 SE	ELEVATION	2230.00	2231.00	2232.00	2233.00	2234.00	2235.00	2236.00	2237.00	2238.00	2239.00
		2240.00	2241.00	2242.00	2243.00	2244.00	2245.00	2246.00	2247.00	2248.00	2249.00
266 SQ	DISCHARGE	0.	70.	180.	317.	479.	659.	855.	1068.	1291.	1526.
		1776.	2039.	2257.	2384.	2512.	2700.	2887.	3061.	3226.	3515.

SDN3.OUT

268 SE	ELEVATION	2230.00	2231.00	2232.00	2233.00	2234.00	2235.00	2236.00	2237.00	2238.00	2239.00
		2240.00	2241.00	2242.00	2243.00	2244.00	2245.00	2246.00	2247.00	2248.00	2249.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.13	.66	1.85	3.90	6.97	11.16	16.15	21.51	27.21
OUTFLOW	.00	70.20	180.10	317.40	479.10	659.20	854.50	1068.10	1290.90	1525.90
ELEVATION	2230.00	2231.00	2232.00	2233.00	2234.00	2235.00	2236.00	2237.00	2238.00	2239.00
STORAGE	33.22	39.59	46.37	53.53	61.03	68.88	77.06	85.51	94.16	102.96
OUTFLOW	1776.10	2038.60	2256.80	2384.20	2511.70	2700.00	2887.00	3060.90	3225.70	3515.40
ELEVATION	2240.00	2241.00	2242.00	2243.00	2244.00	2245.00	2246.00	2247.00	2248.00	2249.00

*** WARNING *** MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 0. TO 70.
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .95

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)	(CFS)			
+	1009.	4.08	474.	304.	293.
	(INCHES)		.394	1.012	1.012
	(AC-FT)		235.	603.	603.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)	(HR)			
	15.	4.08	4.	2.	2.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)	(HR)			
	2236.72	4.08	2233.88	2232.80	2232.70

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .88

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)	(CFS)			
+	886.	4.08	435.	282.	272.
	(INCHES)		.362	.940	.940
	(AC-FT)		216.	560.	560.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)	(HR)			
	12.	4.08	4.	2.	2.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)	(HR)			
	2236.15	4.08	2233.67	2232.66	2232.56

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .83

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)	(CFS)			
+	803.	4.08	408.	267.	257.
	(INCHES)		.340	.889	.889
	(AC-FT)		202.	530.	530.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)	(HR)			
	10.	4.08	3.	2.	2.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)	(HR)			
	2235.73	4.08	2233.51	2232.55	2232.46

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .80

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)	(CFS)			
+	757.	4.08	393.	258.	248.
	(INCHES)		.327	.858	.858
	(AC-FT)		195.	512.	512.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)	(HR)			
	9.	4.08	3.	2.	1.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)	(HR)			
	2235.50	4.08	2233.42	2232.49	2232.40

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .76

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)						
+ 695.	4.08	(CFS)	371.	245.	236.	236.	
		(INCHES)	.309	.815	.815	.815	
		(AC-FT)	184.	486.	486.	486.	
PEAK STORAGE	TIME						
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 8.	4.08		3.	1.	1.		1.
PEAK STAGE	TIME						
+ (FEET)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 2235.18	4.08		2233.29	2232.40	2232.31		2232.31

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
FOR PLAN 1, RATIO = .73

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)						
+ 629.	4.08	(CFS)	348.	231.	223.	223.	
		(INCHES)	.290	.769	.769	.769	
		(AC-FT)	173.	458.	458.	458.	
PEAK STORAGE	TIME						
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 6.	4.08		2.	1.	1.		1.
PEAK STAGE	TIME						
+ (FEET)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 2234.83	4.08		2233.15	2232.30	2232.21		2232.21

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
FOR PLAN 1, RATIO = .57

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)						
+ 393.	4.25	(CFS)	263.	170.	164.	164.	
		(INCHES)	.219	.566	.566	.566	
		(AC-FT)	130.	337.	337.	337.	
PEAK STORAGE	TIME						
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 3.	4.25		1.	1.	1.		1.
PEAK STAGE	TIME						
+ (FEET)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 2233.47	4.25		2232.59	2231.83	2231.76		2231.76

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
FOR PLAN 1, RATIO = .44

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)						
+ 243.	5.08	(CFS)	193.	98.	94.	94.	
		(INCHES)	.161	.326	.326	.326	
		(AC-FT)	96.	194.	194.	194.	
PEAK STORAGE	TIME						
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 1.	5.08		1.	0.	0.		0.
PEAK STAGE	TIME						
+ (FEET)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 2232.46	5.08		2232.09	2231.12	2231.08		2231.08

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
FOR PLAN 1, RATIO = .26

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)						
+ 108.	5.58	(CFS)	82.	23.	22.	22.	
		(INCHES)	.068	.075	.075	.075	
		(AC-FT)	40.	45.	45.	45.	
PEAK STORAGE	TIME						
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 0.	5.58		0.	0.	0.		0.
PEAK STAGE	TIME						
+ (FEET)	(HR)		6-HR	24-HR	72-HR		24.92-HR
+ 2231.34	5.58		2231.09	2230.30	2230.29		2230.29

CUMULATIVE AREA = 11.18 SQ MI

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 * CP7DB *

275 KO OUTPUT CONTROL VARIABLES
 IPRINT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

276 RS	STORAGE ROUTING	1	NUMBER OF SUBREACHES	TYPE OF INITIAL CONDITION	INITIAL CONDITION	WORKING R AND D COEFFICIENT
	NSTPS	STOR				
	ITYP	-1.00				
	RSVRIC	.00				
	X					
277 SV	STORAGE	.0	.7	5.4	13.6	21.9
		74.7	84.0	93.5	103.1	112.8
279 SE	ELEVATION	2220.00	2221.00	2222.00	2223.00	2224.00
		2230.00	2231.00	2232.00	2233.00	2234.00
281 SQ	DISCHARGE	0.	13.	37.	152.	340.
		2225.	2481.	2701.	3036.	3463.
283 SE	ELEVATION	2220.00	2221.00	2222.00	2223.00	2224.00
		2230.00	2231.00	2232.00	2233.00	2234.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.68	5.42	13.62	21.95	30.42	39.03	47.76	56.62	65.61
OUTFLOW	.00	13.20	37.20	152.00	340.30	578.10	849.70	1155.10	1488.10	1845.50
ELEVATION	2220.00	2221.00	2222.00	2223.00	2224.00	2225.00	2226.00	2227.00	2228.00	2229.00
STORAGE	74.74	84.02	93.46	103.05	112.79					
OUTFLOW	2224.90	2481.10	2700.80	3035.50	3463.40					
ELEVATION	2230.00	2231.00	2232.00	2233.00	2234.00					

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .95

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)				
+	811.	4.50			
	(CFS)	460.	295.	284.	284.
	(INCHES)	382.	982.	982.	982.
	(AC-FT)	228.	585.	585.	585.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)				
+	38.	4.50			
	(AC-FT)	26.	19.	18.	18.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)				
+	2225.86	4.50			
	(FEET)	2224.47	2223.59	2223.46	2223.46

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .88

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)				
+	706.	4.50			
	(CFS)	420.	274.	264.	264.
	(INCHES)	349.	911.	911.	911.
	(AC-FT)	208.	543.	543.	543.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)				
+	34.	4.50			
	(AC-FT)	25.	18.	17.	17.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)				
+	2225.47	4.50			
	(FEET)	2224.30	2223.47	2223.35	2223.35

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .83

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(CFS)				
+	635.	4.58			
	(CFS)	393.	259.	249.	249.
	(INCHES)	327.	861.	861.	861.
	(AC-FT)	195.	513.	513.	513.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(AC-FT)				
+	32.	4.58			
	(AC-FT)	24.	18.	17.	17.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
+	(FEET)				
+	2225.21	4.58			
	(FEET)	2224.19	2223.39	2223.27	2223.27

CUMULATIVE AREA = 11.18 SQ MI

HYDROGRAPH AT STATION CP7DB
 FOR PLAN 1, RATIO = .80

PEAK FLOW TIME MAXIMUM AVERAGE FLOW

							SDN3.OUT
+	(CFS)	(HR)		6-HR	24-HR	72-HR	24.92-HR
+	595.	4.58	(CFS)	378.	250.	241.	241.
			(INCHES)	.314	.831	.831	.831
			(AC-FT)	187.	496.	496.	496.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE	
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR	
+	31.	4.58		23.	17.	17.	17.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE	
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR	
+	2225.06	4.58		2224.12	2223.34	2223.22	2223.22
CUMULATIVE AREA =				11.18	SQ MI		
***	***	***	***	***	***	***	***
HYDROGRAPH AT STATION CP7DB FOR PLAN 1, RATIO = .76							
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW	
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR	
+	538.	4.58	(CFS)	356.	237.	228.	228.
			(INCHES)	.296	.789	.789	.789
			(AC-FT)	176.	470.	470.	470.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE	
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR	
+	29.	4.58		22.	17.	16.	16.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE	
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR	
+	2224.83	4.58		2224.03	2223.27	2223.15	2223.15
CUMULATIVE AREA =				11.18	SQ MI		
***	***	***	***	***	***	***	***
HYDROGRAPH AT STATION CP7DB FOR PLAN 1, RATIO = .73							
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW	
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR	
+	484.	4.67	(CFS)	333.	224.	215.	215.
			(INCHES)	.277	.744	.744	.744
			(AC-FT)	165.	443.	443.	443.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE	
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR	
+	27.	4.67		21.	16.	15.	15.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE	
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR	
+	2224.61	4.67		2223.92	2223.19	2223.07	2223.07
CUMULATIVE AREA =				11.18	SQ MI		
***	***	***	***	***	***	***	***
HYDROGRAPH AT STATION CP7DB FOR PLAN 1, RATIO = .57							
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW	
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR	
+	323.	5.42	(CFS)	248.	166.	160.	160.
			(INCHES)	.207	.551	.551	.551
			(AC-FT)	123.	329.	329.	329.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE	
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR	
+	21.	5.42		18.	13.	13.	13.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE	
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR	
+	2223.91	5.42		2223.51	2222.83	2222.73	2222.73
CUMULATIVE AREA =				11.18	SQ MI		
***	***	***	***	***	***	***	***
HYDROGRAPH AT STATION CP7DB FOR PLAN 1, RATIO = .44							
PEAK FLOW	TIME			6-HR	MAXIMUM AVERAGE	FLOW	
+	(CFS)	(HR)		24-HR	72-HR	24.92-HR	
+	217.	5.75	(CFS)	183.	98.	94.	94.
			(INCHES)	.152	.325	.325	.325
			(AC-FT)	91.	194.	194.	194.
PEAK STORAGE	TIME			6-HR	MAXIMUM AVERAGE	STORAGE	
+	(AC-FT)	(HR)		24-HR	72-HR	24.92-HR	
+	16.	5.75		15.	9.	8.	8.
PEAK STAGE	TIME			6-HR	MAXIMUM AVERAGE	STAGE	
+	(FEET)	(HR)		24-HR	72-HR	24.92-HR	
+	2223.35	5.75		2223.16	2222.12	2222.04	2222.04
CUMULATIVE AREA =				11.18	SQ MI		
***	***	***	***	***	***	***	***
HYDROGRAPH AT STATION CP7DB FOR PLAN 1, RATIO = .26							

SDN3.OUT

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)					
+ 93.	6.83	(CFS)	72.	22.	22.	22.
		(INCHES)	.060	.075	.075	.075
		(AC-FT)	36.	45.	45.	45.

PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	24.92-HR
+ (AC-FT)	(HR)					
+ 9.	6.75		8.	2.	2.	2.

PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	24.92-HR
+ (FEET)	(HR)					
+ 2222.48	6.83		2222.30	2220.86	2220.83	2220.83

CUMULATIVE AREA = 11.18 SQ MI

*** HEC-1 ERROR 1 *** INVALID CARD IDENTIFICATION CODE OR CARD OUT OF SEQUENCE
CARD NO. 341

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890 KK * DB4 *
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895 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA
896 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP STOP TYPE OF INITIAL CONDITION
RSVRIC .00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

897 SV	STORAGE	229.0	261.0	13.0	31.0	61.0	97.0	118.0	140.0	171.0	200.0
				290.0	315.0	344.0	379.0	409.0	437.0	470.0	504.0
899 SE	ELEVATION	2048.00	2050.00	2052.00	2054.00	2056.00	2058.00	2059.00	2060.00	2061.00	2062.00
		2063.00	2064.00	2065.00	2066.00	2067.00	2068.00	2069.00	2070.00	2071.00	2072.00
901 SQ	DISCHARGE	0.	37.	80.	117.	142.	163.	173.	182.	191.	198.
		206.	213.	221.	228.	235.	242.	248.	255.	261.	267.
903 SS	SPILLWAY										
	CREL	2069.00	SPILLWAY CREST ELEVATION								
	SPWID	900.00	SPILLWAY WIDTH								
	COCW	3.00	WEIR COEFFICIENT								
	EXPW	1.50	EXPONENT OF HEAD								

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	229.0	261.0	290.0	315.0	344.0	379.0	409.0	437.0	470.0	504.0
OUTFLOW	0.	37.00	80.00	117.00	142.00	163.00	173.00	182.00	191.00	198.00
ELEVATION	2048.00	2050.00	2052.00	2054.00	2056.00	2058.00	2059.00	2060.00	2061.00	2062.00
STORAGE	229.00	261.00	290.00	315.00	344.00	379.00	409.00	437.00	470.00	504.00
OUTFLOW	0.00	213.00	221.00	228.00	235.00	242.00	248.00	255.00	261.00	267.00
ELEVATION	2063.00	2064.00	2065.00	2066.00	2067.00	2068.00	2069.00	2070.00	2071.00	2072.00

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HYDROGRAPH AT STATION DB4
FOR PLAN 1, RATIO = .95

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)					
+ 1713.	5.00	(CFS)	454.	248.	239.	239.
		(INCHES)	.629	1.374	1.375	1.375
		(AC-FT)	225.	491.	492.	492.

PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	24.92-HR
+ (AC-FT)	(HR)					
+ 425.	5.00		387.	233.	224.	224.

PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	24.92-HR
+ (FEET)	(HR)					
+ 2069.58	5.00		2068.32	2062.57	2062.04	2062.04

CUMULATIVE AREA = 6.71 SQ MI

*** **

HYDROGRAPH AT STATION DB4
FOR PLAN 1, RATIO = .88

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+ (CFS)	(HR)					
+ 933.	5.42	(CFS)	304.	209.	201.	201.
		(INCHES)	.422	1.159	1.160	1.160
		(AC-FT)	151.	415.	415.	415.

PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	24.92-HR
+ (AC-FT)	(HR)					
+ 417.	5.42		379.	229.	221.	221.

PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	24.92-HR
+ (FEET)	(HR)					
+ 2069.27	5.42		2068.07	2062.41	2061.88	2061.88

CUMULATIVE AREA = 6.71 SQ MI

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HYDROGRAPH AT STATION DB4 FOR PLAN 1, RATIO = .83					
PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR
+ (CFS)	(HR)				24.92-HR
+ 245.	6.08	(CFS)	238.	190.	183.
		(INCHES)	.330	1.051	1.051
		(AC-FT)	118.	376.	376.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR
+ (AC-FT)	(HR)				24.92-HR
+ 395.	6.08		361.	216.	208.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR
+ (FEET)	(HR)				24.92-HR
+ 2068.55	6.08		2067.48	2061.93	2061.42
		CUMULATIVE AREA = 6.71 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION DB4 FOR PLAN 1, RATIO = .80					
PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR
+ (CFS)	(HR)				24.92-HR
+ 240.	6.00	(CFS)	233.	184.	177.
		(INCHES)	.323	1.019	1.019
		(AC-FT)	115.	365.	365.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR
+ (AC-FT)	(HR)				24.92-HR
+ 370.	6.00		337.	197.	190.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR
+ (FEET)	(HR)				24.92-HR
+ 2067.75	6.00		2066.70	2061.24	2060.75
		CUMULATIVE AREA = 6.71 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION DB4 FOR PLAN 1, RATIO = .76					
PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR
+ (CFS)	(HR)				24.92-HR
+ 233.	6.00	(CFS)	225.	175.	169.
		(INCHES)	.312	.973	.973
		(AC-FT)	111.	348.	348.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR
+ (AC-FT)	(HR)				24.92-HR
+ 336.	6.00		304.	173.	166.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR
+ (FEET)	(HR)				24.92-HR
+ 2066.73	6.00		2065.57	2060.27	2059.82
		CUMULATIVE AREA = 6.71 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION DB4 FOR PLAN 1, RATIO = .73					
PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR
+ (CFS)	(HR)				24.92-HR
+ 224.	6.00	(CFS)	216.	166.	160.
		(INCHES)	.300	.921	.921
		(AC-FT)	107.	329.	329.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR
+ (AC-FT)	(HR)				24.92-HR
+ 302.	6.00		271.	148.	142.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR
+ (FEET)	(HR)				24.92-HR
+ 2065.48	6.00		2064.39	2059.24	2058.82
		CUMULATIVE AREA = 6.71 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION DB4 FOR PLAN 1, RATIO = .57					
PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR
+ (CFS)	(HR)				24.92-HR
+ 193.	6.00	(CFS)	186.	114.	110.
		(INCHES)	.257	.631	.631
		(AC-FT)	92.	226.	226.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR
+ (AC-FT)	(HR)				24.92-HR
+ 179.	6.00		154.	66.	64.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR
+ (FEET)	(HR)				24.92-HR
+ 2061.26	6.00		2060.42	2054.91	2054.66
		CUMULATIVE AREA = 6.71 SQ MI			

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***          ***          ***          ***          ***
HYDROGRAPH AT STATION      DB4
FOR PLAN 1, RATIO = .44

PEAK FLOW    TIME          6-HR    MAXIMUM AVERAGE FLOW    24.92-HR
+ (CFS)      (HR)                                     24-HR    72-HR
+ 160.      5.92      (CFS)      149.      65.      63.      63.
                  (INCHES)      .207      .360      .360      .360
                  (AC-FT)      74.      129.      129.      129.

PEAK STORAGE  TIME          6-HR    MAXIMUM AVERAGE STORAGE    24.92-HR
+ (AC-FT)     (HR)                                     24-HR    72-HR
+ 92.         5.92      74.      25.      24.      24.

PEAK STAGE    TIME          6-HR    MAXIMUM AVERAGE STAGE    24.92-HR
+ (FEET)      (HR)                                     24-HR    72-HR
+ 2057.72     5.92      2056.69  2051.61  2051.48  2051.48

CUMULATIVE AREA = 6.71 SQ MI

***          ***          ***          ***          ***
HYDROGRAPH AT STATION      DB4
FOR PLAN 1, RATIO = .26

PEAK FLOW    TIME          6-HR    MAXIMUM AVERAGE FLOW    24.92-HR
+ (CFS)      (HR)                                     24-HR    72-HR
+ 83.        5.50      (CFS)      63.      16.      16.      16.
                  (INCHES)      .087      .091      .091      .091
                  (AC-FT)      31.      33.      33.      33.

PEAK STORAGE  TIME          6-HR    MAXIMUM AVERAGE STORAGE    24.92-HR
+ (AC-FT)     (HR)                                     24-HR    72-HR
+ 15.         5.50      9.      2.      2.      2.

PEAK STAGE    TIME          6-HR    MAXIMUM AVERAGE STAGE    24.92-HR
+ (FEET)      (HR)                                     24-HR    72-HR
+ 2052.18     5.50      2051.20  2048.84  2048.81  2048.81

CUMULATIVE AREA = 6.71 SQ MI

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*****
1013 KK      *
              * DB5 *
              *
*****

1018 KO      OUTPUT CONTROL VARIABLES
              IPRNT      3 PRINT CONTROL
              IPLOT      0 PLOT CONTROL
              QSCAL      0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

1019 RS      STORAGE ROUTING
              NSTPS      1 NUMBER OF SUBREACHES
              ITYP      STOR TYPE OF INITIAL CONDITION
              RSVRIC      -1.00 INITIAL CONDITION
              X          .00 WORKING R AND D COEFFICIENT

1020 SV      STORAGE      1.2      3.3      12.1      28.0      49.0      79.8      115.0      166.1      232.2      320.1
                  418.8      534.5      605.5      681.1      765.1      846.8      943.4      1044.8      1261.8      1426.1

1022 SE      ELEVATION    2446.00  2450.00  2454.00  2458.00  2462.00  2466.00  2470.00  2474.00  2478.00  2482.00
                  2486.00  2490.00  2492.00  2494.00  2496.00  2498.00  2500.00  2502.00  2506.00  2510.00

1024 SQ      DISCHARGE    1.      23.      36.      46.      54.      60.      67.      72.      78.      82.
                  87.      91.      94.      96.      98.      100.      101.      103.      107.      111.

1026 SE      ELEVATION    2446.00  2450.00  2454.00  2458.00  2462.00  2466.00  2470.00  2474.00  2478.00  2482.00
                  2486.00  2490.00  2492.00  2494.00  2496.00  2498.00  2500.00  2502.00  2506.00  2510.00

***

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE      1.20      3.30      12.10      28.00      49.00      79.80      115.00      166.10      232.20      320.10
OUTFLOW      .50      22.90      36.10      45.70      53.60      60.40      66.50      72.30      77.50      82.40
ELEVATION    2446.00  2450.00  2454.00  2458.00  2462.00  2466.00  2470.00  2474.00  2478.00  2482.00

STORAGE      418.80  534.50      605.50      681.10      765.10      846.80      943.40      1044.80      1261.80      1426.10
OUTFLOW      87.00      91.20      93.50      95.60      97.60      99.50      101.40      103.40      107.20      110.70
ELEVATION    2486.00  2490.00  2492.00  2494.00  2496.00  2498.00  2500.00  2502.00  2506.00  2510.00

***          ***          ***          ***          ***
HYDROGRAPH AT STATION      DB5
FOR PLAN 1, RATIO = .95

PEAK FLOW    TIME          6-HR    MAXIMUM AVERAGE FLOW    24.92-HR
+ (CFS)      (HR)                                     24-HR    72-HR
+ 90.        6.00      (CFS)      89.      82.      79.      79.
                  (INCHES)      .153      .562      .563      .563
                  (AC-FT)      44.      162.      162.      162.

PEAK STORAGE  TIME          6-HR    MAXIMUM AVERAGE STORAGE    24.92-HR
+ (AC-FT)     (HR)                                     24-HR    72-HR
+ 496.        6.00      481.      385.      371.      371.

PEAK STAGE    TIME          6-HR    MAXIMUM AVERAGE STAGE    24.92-HR
+ (FEET)      (HR)                                     24-HR    72-HR
+ 2488.66     6.00      2488.14  2482.96  2481.62  2481.62

CUMULATIVE AREA = 5.41 SQ MI

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HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .88

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+	(CFS)	(HR)					
+	88.	6.00	(CFS)	87.	79.	76.	76.
			(INCHES)	.150	.545	.545	.545
			(AC-FT)	43.	157.	157.	157.
PEAK STORAGE	TIME						
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	438.	6.00	424.	335.	323.		323.
PEAK STAGE	TIME						
+	(FEET)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	2486.67	6.00	2486.16	2480.94	2479.66		2479.66
CUMULATIVE AREA =			5.41 SQ MI				

HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .83

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+	(CFS)	(HR)					
+	86.	6.00	(CFS)	85.	77.	75.	75.
			(INCHES)	.147	.532	.532	.532
			(AC-FT)	42.	154.	154.	154.
PEAK STORAGE	TIME						
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	400.	6.00	386.	302.	291.		291.
PEAK STAGE	TIME						
+	(FEET)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	2485.22	6.00	2484.65	2479.48	2478.25		2478.25
CUMULATIVE AREA =			5.41 SQ MI				

HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .80

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+	(CFS)	(HR)					
+	85.	5.92	(CFS)	84.	76.	73.	73.
			(INCHES)	.145	.525	.525	.525
			(AC-FT)	42.	151.	151.	151.
PEAK STORAGE	TIME						
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	377.	6.00	364.	283.	272.		272.
PEAK STAGE	TIME						
+	(FEET)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	2484.32	6.00	2483.76	2478.62	2477.42		2477.42
CUMULATIVE AREA =			5.41 SQ MI				

HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .76

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+	(CFS)	(HR)					
+	84.	5.83	(CFS)	83.	75.	72.	72.
			(INCHES)	.143	.514	.514	.514
			(AC-FT)	41.	148.	148.	148.
PEAK STORAGE	TIME						
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	347.	5.92	333.	256.	247.		247.
PEAK STAGE	TIME						
+	(FEET)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	2483.07	5.92	2482.53	2477.40	2476.24		2476.24
CUMULATIVE AREA =			5.41 SQ MI				

HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .73

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
+	(CFS)	(HR)					
+	82.	5.83	(CFS)	81.	73.	70.	70.
			(INCHES)	.140	.501	.502	.502
			(AC-FT)	40.	145.	145.	145.
PEAK STORAGE	TIME						
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	316.	5.83	303.	230.	222.		222.
PEAK STAGE	TIME						
+	(FEET)	(HR)	6-HR	24-HR	72-HR		24.92-HR
	2481.80	5.83	2481.20	2476.07	2474.97		2474.97
CUMULATIVE AREA =			5.41 SQ MI				

HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .57

PEAK FLOW + (CFS)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
75.	5.50	(CFS)	74.	64.	62.
		(INCHES)	.128	.441	.441
		(AC-FT)	37.	127.	127.
PEAK STORAGE + (AC-FT)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
203.	5.50	191.	135.	130.	130.
PEAK STAGE + (FEET)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
2476.22	5.50	2475.51	2470.02	2469.14	2469.14
CUMULATIVE AREA =		5.41 SQ MI			

HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .44

PEAK FLOW + (CFS)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
67.	5.42	(CFS)	65.	53.	51.
		(INCHES)	.112	.363	.363
		(AC-FT)	32.	105.	105.
PEAK STORAGE + (AC-FT)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
119.	5.42	109.	67.	64.	64.
PEAK STAGE + (FEET)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
2470.33	5.42	2469.24	2463.09	2462.46	2462.46
CUMULATIVE AREA =		5.41 SQ MI			

HYDROGRAPH AT STATION DB5
FOR PLAN 1, RATIO = .26

PEAK FLOW + (CFS)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
46.	5.17	(CFS)	43.	18.	18.
		(INCHES)	.073	.127	.127
		(AC-FT)	21.	37.	37.
PEAK STORAGE + (AC-FT)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
30.	5.17	23.	8.	8.	8.
PEAK STAGE + (FEET)	TIME (HR)	6-HR	MAXIMUM 24-HR	AVERAGE 72-HR	24.92-HR
2458.34	5.17	2456.75	2450.22	2450.07	2450.07
CUMULATIVE AREA =		5.41 SQ MI			

*** HEC-1 ERROR 1 *** INVALID CARD IDENTIFICATION CODE OR CARD OUT OF SEQUENCE
CARD NO. 1121

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION										
				RATIO 1 .95	RATIO 2 .88	RATIO 3 .83	RATIO 4 .80	RATIO 5 .76	RATIO 6 .73	RATIO 7 .57	RATIO 8 .44	RATIO 9 .26		
HYDROGRAPH AT														
+	C1H	4.01	1	FLOW TIME	5490. 3.58	4881. 3.58	4468. 3.58	4229. 3.58	3899. 3.58	3563. 3.58	2311. 3.58	1350. 3.58	279. 3.58	
ROUTED TO														
+	DB1	4.01	1	FLOW TIME	198. 5.33	190. 5.33	184. 5.33	180. 5.33	175. 5.33	169. 5.33	142. 5.25	114. 5.25	61. 5.17	
				** PEAK STAGES IN FEET **										
			1	STAGE TIME	2588.10 5.33	2585.67 5.33	2583.94 5.33	2582.91 5.33	2581.46 5.33	2579.94 5.33	2574.00 5.25	2568.87 5.25	2562.37 5.17	
ROUTED TO														
+	RDB1	4.01	1	FLOW TIME	198. 5.50	190. 5.50	184. 5.50	180. 5.50	175. 5.42	169. 5.42	142. 5.42	114. 5.42	62. 5.33	
HYDROGRAPH AT														
+	C1HB1	.45	1	FLOW TIME	305. 4.00	268. 4.00	243. 4.00	228. 4.00	208. 4.00	188. 4.00	114. 4.00	60. 4.00	9. 4.17	
2 COMBINED AT														
+	CP2	4.46	1	FLOW TIME	481. 4.00	434. 4.00	403. 4.00	384. 4.00	360. 4.00	334. 4.00	236. 4.08	160. 4.08	70. 5.17	
ROUTED TO														
+	RCP2	4.46	1	FLOW TIME	478. 4.00	432. 4.00	400. 4.00	382. 4.00	357. 4.00	331. 4.00	236. 4.08	159. 4.08	70. 5.25	
HYDROGRAPH AT														
+	C1G3A	.27	1	FLOW TIME	358. 3.58	318. 3.58	291. 3.58	275. 3.58	253. 3.58	231. 3.58	149. 3.58	86. 3.58	19. 3.67	
2 COMBINED AT														
+	CP3	4.73	1	FLOW TIME	637. 3.75	571. 3.75	526. 3.83	500. 3.83	465. 3.83	428. 3.83	291. 3.83	186. 4.00	76. 5.00	
ROUTED TO														
+	RCP3	4.73	1	FLOW TIME	635. 3.75	571. 3.83	525. 3.83	499. 3.83	462. 3.83	426. 3.92	291. 3.92	186. 4.08	76. 5.08	

SDN3.OUT												
HYDROGRAPH AT												
+ C1G3B	.73	1	FLOW TIME	1014.3.58	901.3.58	824.3.58	780.3.58	719.3.58	657.3.58	425.3.58	247.3.58	49.3.58
2 COMBINED AT												
+ CP4	5.46	1	FLOW TIME	1517.3.58	1343.3.58	1226.3.58	1156.3.58	1063.3.58	967.3.58	595.3.58	310.3.58	95.4.92
ROUTED TO												
+ RCP4	5.46	1	FLOW TIME	1497.3.67	1287.3.67	1173.3.67	1156.3.67	1073.3.67	977.3.67	600.3.67	296.3.67	94.5.00
HYDROGRAPH AT												
+ C1G3C	1.05	1	FLOW TIME	1372.3.58	1218.3.58	1114.3.58	1053.3.58	970.3.58	886.3.58	571.3.58	331.3.67	76.3.67
2 COMBINED AT												
+ CP5	6.51	1	FLOW TIME	2792.3.67	2442.3.67	2232.3.67	2159.3.67	2000.3.67	1826.3.67	1158.3.67	627.3.67	127.3.75
HYDROGRAPH AT												
+ C1G3D	.84	1	FLOW TIME	1246.3.58	1113.3.58	1022.3.58	970.3.58	897.3.58	824.3.58	546.3.58	330.3.58	82.3.58
2 COMBINED AT												
+ CP6A	7.35	1	FLOW TIME	4005.3.58	3515.3.58	3206.3.58	3053.3.58	2811.3.58	2556.3.58	1635.3.67	922.3.67	196.3.75
HYDROGRAPH AT												
+ C51CB	.73	1	FLOW TIME	850.3.58	741.3.58	667.3.58	625.3.58	567.3.58	509.3.58	297.3.58	144.3.58	14.3.83
ROUTED TO												
+ C51CB	.73	1	FLOW TIME	799.3.67	719.3.67	652.3.67	594.3.67	539.3.67	489.3.67	291.3.67	138.3.75	18.4.00
HYDROGRAPH AT												
+ C51ZA	1.40	1	FLOW TIME	1698.3.58	1485.3.58	1342.3.58	1260.3.58	1147.3.58	1034.3.58	618.3.58	314.3.58	35.3.75
2 COMBINED AT												
+ CP6B	2.13	1	FLOW TIME	2448.3.58	2133.3.58	1921.3.58	1790.3.58	1629.3.58	1459.3.58	841.3.58	421.3.67	42.4.92
2 COMBINED AT												
+ CP6	9.48	1	FLOW TIME	6453.3.58	5648.3.58	5126.3.58	4844.3.58	4440.3.58	4015.3.58	2469.3.67	1343.3.67	231.3.75
ROUTED TO												
+ DB2	9.48	1	FLOW TIME	308.6.08	294.6.08	284.6.08	278.6.08	269.6.08	259.6.08	217.6.00	177.5.75	101.5.42
** PEAK STAGES IN FEET **												
ROUTED TO												
+ RDB2	9.48	1	FLOW TIME	308.6.17	294.6.17	284.6.17	278.6.17	269.6.08	259.6.08	217.6.00	177.5.83	101.5.50
HYDROGRAPH AT												
+ C1G2C	.29	1	FLOW TIME	210.3.75	180.3.75	160.3.75	149.3.75	133.3.75	117.3.75	62.3.75	26.3.83	2.5.00
HYDROGRAPH AT												
+ C1G2D	.22	1	FLOW TIME	153.3.67	129.3.67	113.3.67	104.3.67	91.3.67	79.3.67	38.3.75	13.3.83	1.5.00
3 COMBINED AT												
+ CP7A	10.00	1	FLOW TIME	583.3.75	518.3.75	475.3.75	450.3.75	416.3.75	381.3.75	261.3.83	194.5.00	102.5.42
HYDROGRAPH AT												
+ C1G2B1	.52	1	FLOW TIME	260.3.92	220.3.92	193.3.92	178.3.92	157.3.92	137.3.92	67.4.00	25.4.08	1.5.17
ROUTED TO												
+ RG2B1	.52	1	FLOW TIME	267.4.08	219.4.08	192.4.08	173.4.17	157.4.08	132.4.25	91.4.17	34.4.58	2.7.00
HYDROGRAPH AT												
+ C1G2B2	.31	1	FLOW TIME	230.3.75	198.3.75	177.3.75	165.3.75	148.3.75	131.3.75	71.3.75	31.3.83	3.5.00
2 COMBINED AT												
+ CP7B	.83	1	FLOW TIME	403.3.92	325.4.00	284.4.08	263.4.00	243.4.00	211.4.00	125.4.17	46.4.58	3.5.00
HYDROGRAPH AT												
+ C1G2A	.35	1	FLOW TIME	309.3.67	267.3.67	240.3.67	224.3.67	203.3.67	181.3.67	103.3.67	49.3.75	5.4.92
ROUTED TO												
+ RC1G2A	.35	1	FLOW TIME	308.3.83	270.3.83	234.3.83	224.3.83	199.3.83	176.3.83	105.3.92	38.4.17	5.5.50
2 COMBINED AT												
+ CP7C	1.18	1	FLOW TIME	671.3.92	560.3.92	487.3.92	438.4.00	404.4.00	357.4.00	194.4.17	65.4.58	7.5.08
2 COMBINED AT												
+ CP7	11.18	1	FLOW TIME	1188.3.83	1026.3.92	920.3.92	848.3.92	766.4.00	695.4.00	430.3.83	245.5.00	108.5.50
ROUTED TO												
+ CP7DB	11.18	1	FLOW TIME	1009.4.08	886.4.08	803.4.08	757.4.08	695.4.08	629.4.08	393.4.25	243.5.08	108.5.58
** PEAK STAGES IN FEET **												
ROUTED TO												
+ CP7DB	11.18	1	FLOW TIME	811.4.50	706.4.50	635.4.58	595.4.58	538.4.58	484.4.67	323.5.42	217.5.75	93.6.83
** PEAK STAGES IN FEET **												
ROUTED TO												
+ RCP7	11.18	1	FLOW TIME	809.4.50	705.4.58	634.4.58	593.4.58	538.4.67	484.4.75	323.5.42	217.5.83	93.6.92
HYDROGRAPH AT												
+ C1NA	.41	1	FLOW TIME	744.3.50	662.3.50	606.3.50	574.3.50	530.3.50	484.3.50	315.3.50	184.3.50	38.3.50

SDN3. OUT												
ROUTED TO												
+ RC1NA	.41	1	FLOW TIME	675.	597.	542.	519.	469.	431.	264.	155.	36.
				3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.58	3.58
2 COMBINED AT												
+ CP8	11.59	1	FLOW TIME	948.	833.	753.	706.	643.	576.	367.	223.	93.
				4.58	4.58	4.58	4.58	4.58	4.58	4.92	5.83	6.92
ROUTED TO												
+ RCP8	11.59	1	FLOW TIME	938.	821.	740.	695.	635.	572.	358.	221.	93.
				4.58	4.58	4.67	4.67	4.67	4.67	4.92	5.92	7.00
HYDROGRAPH AT												
+ C5GC	.11	1	FLOW TIME	223.	199.	183.	173.	160.	147.	97.	58.	14.
				3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
ROUTED TO												
+ RC5GC	.11	1	FLOW TIME	187.	164.	150.	142.	133.	123.	84.	55.	11.
				3.50	3.50	3.50	3.50	3.58	3.58	3.58	3.58	3.67
HYDROGRAPH AT												
+ C5GB	.32	1	FLOW TIME	451.	399.	364.	344.	316.	287.	182.	103.	20.
				3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.67
2 COMBINED AT												
+ CP9	.44	1	FLOW TIME	626.	558.	510.	485.	448.	410.	267.	158.	31.
				3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.67
ROUTED TO												
+ RCP9	.44	1	FLOW TIME	598.	526.	481.	453.	414.	379.	248.	150.	31.
				3.58	3.58	3.58	3.58	3.58	3.67	3.67	3.67	3.75
HYDROGRAPH AT												
+ C5GA	.27	1	FLOW TIME	109.	88.	75.	67.	57.	47.	17.	5.	0.
				3.83	3.83	3.83	3.83	3.83	3.83	3.92	5.00	.00
2 COMBINED AT												
+ CP10	.71	1	FLOW TIME	665.	579.	527.	497.	456.	414.	257.	150.	31.
				3.58	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
ROUTED TO												
+ RCP10	.71	1	FLOW TIME	660.	582.	529.	491.	452.	405.	255.	141.	22.
				3.67	3.67	3.67	3.67	3.67	3.75	3.75	3.75	4.25
ROUTED TO												
+ RCP10	.71	1	FLOW TIME	642.	575.	518.	485.	437.	395.	273.	152.	26.
				3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.83	4.33
HYDROGRAPH AT												
+ C5GD	.44	1	FLOW TIME	163.	133.	113.	102.	88.	74.	29.	10.	0.
				4.00	4.00	4.00	4.00	4.00	4.00	4.08	5.08	.00
DIVERSION TO												
+ DIVER1	.44	1	FLOW TIME	23.	20.	19.	17.	16.	14.	8.	3.	0.
				4.00	4.00	4.00	4.00	4.00	4.00	4.08	5.08	.00
HYDROGRAPH AT												
+ DIVER1	.44	1	FLOW TIME	140.	112.	95.	85.	72.	60.	21.	7.	0.
				4.00	4.00	4.00	4.00	4.00	4.00	4.08	5.08	.00
ROUTED TO												
+ RC5GD	.44	1	FLOW TIME	139.	112.	94.	85.	72.	59.	21.	7.	0.
				4.08	4.08	4.08	4.08	4.17	4.17	4.33	5.42	.00
HYDROGRAPH AT												
+ C5I1E	.16	1	FLOW TIME	266.	233.	211.	199.	181.	163.	99.	51.	4.
				3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.75
3 COMBINED AT												
+ CP11	1.32	1	FLOW TIME	798.	697.	618.	570.	509.	458.	313.	163.	28.
				3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.83	4.33
ROUTED TO												
+ RCP11	1.32	1	FLOW TIME	780.	671.	591.	552.	495.	441.	299.	151.	33.
				3.75	3.75	3.75	3.75	3.75	3.83	3.83	3.92	4.50
HYDROGRAPH AT												
+ C1HF	.10	1	FLOW TIME	90.	79.	71.	66.	60.	54.	31.	15.	2.
				3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.75	5.00
2 COMBINED AT												
+ CP12	1.42	1	FLOW TIME	870.	750.	662.	619.	555.	494.	328.	164.	34.
				3.75	3.75	3.75	3.75	3.75	3.75	3.83	3.92	4.50
ROUTED TO												
+ RCP12	1.42	1	FLOW TIME	847.	728.	660.	616.	556.	499.	320.	175.	43.
				3.83	3.83	3.83	3.83	3.83	3.92	4.00	4.08	4.83
HYDROGRAPH AT												
+ C5I1B	.52	1	FLOW TIME	479.	401.	350.	321.	281.	242.	109.	33.	1.
				3.50	3.50	3.50	3.50	3.50	3.50	3.58	3.58	4.92
ROUTED TO												
+ RC5I1B	.52	1	FLOW TIME	447.	387.	333.	307.	272.	235.	110.	32.	1.
				3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.75	5.42
HYDROGRAPH AT												
+ C5I1D	.12	1	FLOW TIME	126.	109.	98.	91.	82.	73.	41.	18.	2.
				3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.67	4.92
2 COMBINED AT												
+ CP13	.63	1	FLOW TIME	574.	496.	431.	398.	354.	308.	151.	49.	2.
				3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.67	4.92
ROUTED TO												
+ RCP13	.63	1	FLOW TIME	548.	470.	404.	378.	334.	295.	139.	51.	2.
				3.67	3.67	3.67	3.67	3.67	3.67	3.75	3.83	5.25
HYDROGRAPH AT												
+ C1HE	.15	1	FLOW TIME	115.	96.	84.	77.	68.	58.	26.	8.	0.
				3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.75	4.92
3 COMBINED AT												
+ CP14	2.20	1	FLOW TIME	1315.	1115.	995.	924.	825.	733.	433.	214.	44.
				3.75	3.75	3.75	3.75	3.83	3.83	3.92	4.08	4.83
DIVERSION TO												
+ DIVER2	2.20	1	FLOW TIME	179.	103.	92.	85.	76.	68.	40.	20.	4.
				3.75	3.75	3.75	3.75	3.83	3.83	3.92	4.08	4.83
HYDROGRAPH AT												
+ DIVER2	2.20	1	FLOW TIME	1136.	1012.	903.	839.	748.	665.	393.	194.	40.
				3.67	3.75	3.75	3.75	3.83	3.83	3.92	4.08	4.83
ROUTED TO												
+ RCP14	2.20	1	FLOW TIME	1135.	999.	889.	828.	742.	652.	382.	185.	32.
				3.75	3.75	3.83	3.83	3.83	3.83	4.00	4.17	5.00
HYDROGRAPH AT												

+		C1HD	.07	1	FLOW TIME	72. 3.58	62. 3.58	55. 3.58	SDW3, OUT 52. 3.58	46. 3.58	41. 3.58	23. 3.58	10. 3.67	1. 4.92
+	2 COMBINED AT	CP15	2.27	1	FLOW TIME	1185. 3.75	1043. 3.75	920. 3.75	858. 3.83	768. 3.83	676. 3.83	391. 4.00	188. 4.17	32. 5.00
+	ROUTED TO	RCP15	2.27	1	FLOW TIME	1176. 3.75	1033. 3.83	923. 3.83	858. 3.83	754. 3.92	666. 3.92	370. 4.08	180. 4.25	28. 5.25
+	DIVERSION TO	DIVER3	2.27	1	FLOW TIME	221. 3.75	191. 3.83	171. 3.83	159. 3.83	140. 3.92	123. 3.92	69. 4.08	33. 4.25	5. 5.25
+	HYDROGRAPH AT	DIVER3	2.27	1	FLOW TIME	955. 3.75	842. 3.83	752. 3.83	699. 3.83	614. 3.92	543. 3.92	302. 4.08	147. 4.25	22. 5.25
+	HYDROGRAPH AT	C511	.24	1	FLOW TIME	238. 3.58	205. 3.58	182. 3.58	169. 3.58	152. 3.58	134. 3.58	73. 3.67	32. 3.67	3. 4.92
+	HYDROGRAPH AT	C511C	.06	1	FLOW TIME	68. 3.67	59. 3.67	54. 3.67	50. 3.67	46. 3.67	41. 3.67	25. 3.67	13. 3.75	2. 3.83
+	ROUTED TO	RC511C	.06	1	FLOW TIME	66. 3.75	58. 3.75	53. 3.75	49. 3.75	44. 3.75	40. 3.75	24. 3.75	13. 3.83	2. 4.08
+	2 COMBINED AT	CP16	.31	1	FLOW TIME	291. 3.58	251. 3.67	224. 3.67	209. 3.67	189. 3.67	168. 3.67	94. 3.67	42. 3.75	4. 4.92
+	ROUTED TO	RCP16	.31	1	FLOW TIME	291. 3.67	252. 3.67	226. 3.67	210. 3.67	188. 3.67	166. 3.67	92. 3.75	42. 3.83	4. 5.17
+	HYDROGRAPH AT	C1G1B	.14	1	FLOW TIME	200. 3.58	179. 3.58	164. 3.58	156. 3.58	144. 3.58	133. 3.58	88. 3.58	54. 3.58	15. 3.67
+	2 COMBINED AT	CP17	.45	1	FLOW TIME	478. 3.67	420. 3.67	381. 3.67	357. 3.67	325. 3.67	292. 3.67	173. 3.67	86. 3.75	15. 3.67
+	ROUTED TO	RCP17	.45	1	FLOW TIME	472. 3.67	401. 3.75	380. 3.75	357. 3.75	326. 3.75	293. 3.75	167. 3.75	87. 3.83	16. 3.92
+	HYDROGRAPH AT	C1HC8	.18	1	FLOW TIME	249. 3.50	217. 3.50	195. 3.50	182. 3.50	165. 3.50	148. 3.50	85. 3.50	40. 3.50	3. 4.83
+	2 COMBINED AT	CP18A	.63	1	FLOW TIME	589. 3.67	495. 3.67	464. 3.67	434. 3.67	394. 3.75	355. 3.75	206. 3.75	98. 3.83	18. 3.92
+	2 COMBINED AT	CP18	2.90	1	FLOW TIME	1522. 3.75	1306. 3.75	1159. 3.75	1075. 3.75	946. 3.75	820. 3.75	428. 4.00	194. 4.25	32. 5.25
+	DIVERSION TO	DIVER4	2.90	1	FLOW TIME	446. 3.75	195. 3.75	104. 3.75	97. 3.75	85. 3.75	74. 3.75	39. 4.00	17. 4.25	3. 5.25
+	HYDROGRAPH AT	DIVER4	2.90	1	FLOW TIME	1115. 3.92	1121. 3.83	1055. 3.75	978. 3.75	861. 3.75	747. 3.75	390. 4.00	176. 4.25	29. 5.25
+	ROUTED TO	RCP18	2.90	1	FLOW TIME	1106. 3.92	1120. 3.83	1035. 3.83	966. 3.83	855. 3.83	747. 3.83	386. 4.00	165. 4.33	28. 5.33
+	HYDROGRAPH AT	C1G1A	.22	1	FLOW TIME	255. 3.67	226. 3.67	206. 3.67	195. 3.67	179. 3.67	163. 3.67	104. 3.67	59. 3.67	12. 3.75
+	ROUTED TO	RC1G1A	.22	1	FLOW TIME	258. 3.75	227. 3.75	198. 3.75	187. 3.83	178. 3.83	164. 3.83	102. 3.83	58. 3.83	14. 4.17
+	HYDROGRAPH AT	C1HB	.15	1	FLOW TIME	278. 3.50	249. 3.50	228. 3.50	217. 3.50	200. 3.50	184. 3.50	122. 3.50	73. 3.50	18. 3.50
+	2 COMBINED AT	CP19A	.37	1	FLOW TIME	348. 3.75	308. 3.75	273. 3.75	257. 3.75	243. 3.75	221. 3.75	137. 3.75	73. 3.50	18. 3.50
+	2 COMBINED AT	CP19	3.27	1	FLOW TIME	1431. 3.75	1412. 3.75	1281. 3.75	1186. 3.75	1061. 3.83	936. 3.83	491. 4.00	202. 4.17	35. 5.33
+	DIVERSION TO	DIVER5	3.27	1	FLOW TIME	544. 3.75	530. 3.75	431. 3.75	360. 3.75	267. 3.83	173. 3.83	43. 4.00	18. 4.17	3. 5.33
+	HYDROGRAPH AT	DIVER5	3.27	1	FLOW TIME	887. 3.75	882. 3.75	849. 3.75	825. 3.75	794. 3.83	763. 3.83	448. 4.00	185. 4.17	32. 5.33
+	ROUTED TO	RCP19	3.27	1	FLOW TIME	890. 3.83	881. 3.83	844. 3.83	832. 3.83	823. 3.83	759. 3.92	454. 4.08	187. 4.33	32. 5.58
+	HYDROGRAPH AT	C1HA	.07	1	FLOW TIME	27. 3.67	21. 3.67	18. 3.75	16. 3.75	13. 3.75	11. 3.75	3. 3.83	1. 4.92	0. .00
+	2 COMBINED AT	CP20A	3.35	1	FLOW TIME	913. 3.83	899. 3.83	860. 3.83	847. 3.83	835. 3.83	767. 3.92	457. 4.08	187. 4.33	32. 5.58
+	2 COMBINED AT	CP20	14.94	1	FLOW TIME	1499. 4.33	1350. 4.17	1247. 4.08	1193. 4.08	1110. 4.08	1025. 4.08	601. 4.08	315. 5.25	105. 6.83
+	ROUTED TO	RCP20	14.94	1	FLOW TIME	1498. 4.33	1349. 4.17	1245. 4.17	1187. 4.17	1106. 4.08	1020. 4.08	590. 4.08	314. 5.25	105. 6.83
+	HYDROGRAPH AT	C1D	.40	1	FLOW TIME	338. 3.67	291. 3.67	261. 3.67	243. 3.67	219. 3.67	194. 3.67	107. 3.67	48. 3.75	5. 4.92
+	ROUTED TO	RC1D	.40	1	FLOW	341. 3.67	288. 3.67	257. 3.67	240. 3.67	216. 3.67	192. 3.67	104. 3.67	48. 3.75	4. 4.92

				TIME	3.75	3.75	3.75	SDN3_OUT 3.75	3.75	3.75	3.83	3.83	5.17
HYDROGRAPH AT													
+	C1C	.23	1	FLOW TIME	213. 3.58	184. 3.67	166. 3.67	156. 3.67	141. 3.67	127. 3.67	74. 3.67	36. 3.67	4. 4.92
2 COMBINED AT													
+	CP21	.63	1	FLOW TIME	531. 3.67	447. 3.75	402. 3.75	375. 3.75	339. 3.75	303. 3.75	171. 3.75	77. 3.83	7. 5.00
ROUTED TO													
+	RCP21	.63	1	FLOW TIME	541. 3.83	459. 3.83	412. 3.83	384. 3.83	345. 3.83	294. 3.83	169. 3.92	77. 4.00	7. 5.33
HYDROGRAPH AT													
+	C1B	.38	1	FLOW TIME	450. 3.67	401. 3.67	368. 3.67	349. 3.67	322. 3.67	295. 3.67	194. 3.67	116. 3.67	27. 3.75
HYDROGRAPH AT													
+	C4A1D	.06	1	FLOW TIME	52. 3.67	45. 3.67	41. 3.67	38. 3.67	34. 3.67	30. 3.67	17. 3.67	7. 3.67	1. 4.92
ROUTED TO													
+	RC4A1D	.06	1	FLOW TIME	52. 3.67	45. 3.67	40. 3.67	37. 3.67	34. 3.67	30. 3.67	16. 3.67	7. 3.75	1. 5.00
4 COMBINED AT													
+	CP22	16.01	1	FLOW TIME	2296. 3.75	2072. 3.75	1889. 3.83	1804. 3.83	1693. 3.83	1502. 3.83	802. 4.08	375. 5.08	107. 6.00
ROUTED TO													
+	RCP22	16.01	1	FLOW TIME	2285. 3.75	2055. 3.83	1883. 3.83	1789. 3.83	1666. 3.83	1478. 3.92	801. 4.08	375. 5.08	107. 5.75
HYDROGRAPH AT													
+	C1A	.15	1	FLOW TIME	149. 3.67	131. 3.67	119. 3.67	112. 3.67	103. 3.67	94. 3.67	59. 3.67	32. 3.67	6. 3.75
2 COMBINED AT													
+	CP23	16.15	1	FLOW TIME	2419. 3.75	2166. 3.75	1973. 3.83	1875. 3.83	1745. 3.83	1535. 3.83	828. 4.00	384. 5.08	107. 5.75
ROUTED TO													
+	RCP23	16.15	1	FLOW TIME	2410. 3.75	2155. 3.83	1969. 3.83	1866. 3.83	1729. 3.83	1534. 3.92	825. 4.00	383. 5.08	107. 6.17
HYDROGRAPH AT													
+	C5CC	.33	1	FLOW TIME	286. 3.75	249. 3.75	224. 3.75	210. 3.75	190. 3.75	170. 3.75	99. 3.75	47. 3.83	5. 5.00
HYDROGRAPH AT													
+	RET4	.00	1	FLOW TIME	446. 3.75	195. 3.75	104. 3.75	97. 3.75	85. 3.75	74. 3.75	39. 4.00	17. 4.25	3. 5.25
ROUTED TO													
+	RDIV4	.00	1	FLOW TIME	416. 3.75	170. 3.83	103. 3.83	95. 3.83	86. 3.83	73. 3.83	39. 4.00	17. 4.25	3. 5.50
ROUTED TO													
+	RDIV4	.00	1	FLOW TIME	406. 3.83	149. 3.92	104. 3.92	96. 3.92	88. 3.92	74. 3.92	40. 4.08	18. 4.42	3. 5.83
2 COMBINED AT													
+	CP24A	.33	1	FLOW TIME	669. 3.83	371. 3.83	306. 3.83	283. 3.83	252. 3.83	217. 3.83	106. 3.83	47. 3.83	7. 4.75
HYDROGRAPH AT													
+	RET3	.00	1	FLOW TIME	221. 3.75	191. 3.83	171. 3.83	159. 3.83	140. 3.92	123. 3.92	69. 4.08	33. 4.25	5. 5.25
ROUTED TO													
+	RDIV3	.00	1	FLOW TIME	222. 3.83	192. 3.92	169. 4.00	159. 3.83	138. 4.00	124. 3.92	69. 4.08	36. 4.33	7. 5.67
ROUTED TO													
+	RDIV3	.00	1	FLOW TIME	220. 3.92	189. 3.92	167. 3.92	158. 3.92	139. 3.92	119. 4.08	66. 4.17	35. 4.42	6. 5.83
2 COMBINED AT													
+	CP24B	.33	1	FLOW TIME	886. 3.83	549. 3.83	452. 3.83	420. 3.92	378. 3.92	326. 3.92	154. 4.08	68. 4.42	10. 5.83
HYDROGRAPH AT													
+	RET2	.00	1	FLOW TIME	179. 3.75	103. 3.75	92. 3.75	85. 3.75	76. 3.83	68. 3.83	40. 3.92	20. 4.08	4. 4.83
ROUTED TO													
+	RDIV2	.00	1	FLOW TIME	185. 3.83	104. 3.83	93. 3.83	89. 3.83	79. 3.83	68. 3.92	40. 4.00	20. 4.50	3. 5.50
ROUTED TO													
+	RDIV2	.00	1	FLOW TIME	173. 3.83	102. 3.92	90. 3.92	84. 3.92	74. 4.00	67. 3.92	39. 4.08	18. 4.50	3. 5.67
2 COMBINED AT													
+	CP24C	.33	1	FLOW TIME	1059. 3.83	650. 3.83	539. 3.83	504. 3.92	453. 3.92	393. 3.92	192. 4.08	85. 4.42	11. 5.83
HYDROGRAPH AT													
+	C5CA	.30	1	FLOW TIME	185. 3.67	153. 3.67	132. 3.67	121. 3.67	105. 3.67	89. 3.67	40. 3.75	12. 3.83	0. 5.25
ROUTED TO													
+	RC5CA	.30	1	FLOW TIME	182. 3.75	152. 3.75	131. 3.75	120. 3.75	104. 3.75	88. 3.75	40. 3.83	12. 4.00	0. 6.42
HYDROGRAPH AT													
+	C5CF	.32	1	FLOW TIME	228. 3.50	185. 3.50	157. 3.50	142. 3.50	121. 3.50	100. 3.50	34. 3.58	9. 4.83	0. .00
2 COMBINED AT													
+	CP25	.62	1	FLOW TIME	307. 3.58	249. 3.75	217. 3.75	199. 3.75	173. 3.75	149. 3.75	64. 3.75	19. 4.83	0. 6.42
ROUTED TO													
+	RCP25	.62	1	FLOW TIME	306. 3.58	247. 3.75	215. 3.75	196. 3.75	169. 3.75	144. 3.83	64. 3.83	18. 5.00	0. 8.33
HYDROGRAPH AT													
+	C5CE	.32	1	FLOW TIME	221. 3.50	180. 3.50	152. 3.50	137. 3.50	116. 3.50	96. 3.50	37. 3.58	9. 4.83	0. .00
2 COMBINED AT													
+	CP26	.95	1	FLOW TIME	508. 3.58	408. 3.58	343. 3.58	307. 3.58	258. 3.58	209. 3.58	85. 3.83	23. 5.00	0. 8.33
ROUTED TO													
+	RCP26	.95	1	FLOW TIME	487. 3.58	385. 3.58	321. 3.67	290. 3.67	248. 3.67	206. 3.75	83. 3.83	23. 5.00	0. 9.58

SDM3.OUT													
HYDROGRAPH AT +	C5CD	.27	1	FLOW TIME	153. 3.83	130. 3.83	114. 3.83	105. 3.83	93. 3.83	81. 3.83	39. 3.92	14. 3.92	1. 5.08
HYDROGRAPH AT +	RET1	.00	1	FLOW TIME	23. 4.00	20. 4.00	19. 4.00	17. 4.00	16. 4.00	14. 4.00	8. 4.08	3. 5.08	0. .00
ROUTED TO +	RDIV1	.00	1	FLOW TIME	23. 4.08	21. 4.25	20. 4.25	20. 4.17	20. 4.08	17. 4.33	9. 4.33	3. 5.75	0. .00
ROUTED TO +	RDIV1	.00	1	FLOW TIME	23. 4.17	21. 4.33	20. 4.25	20. 4.25	23. 4.17	16. 4.33	8. 4.42	5. 5.83	0. .00
ROUTED TO +	RDIV1	.00	1	FLOW TIME	26. 4.25	21. 4.50	23. 4.33	19. 4.42	23. 4.33	17. 4.58	8. 4.67	3. 6.00	0. .00
3 COMBINED AT +	CP27	1.21	1	FLOW TIME	589. 3.67	483. 3.67	419. 3.75	382. 3.75	331. 3.75	282. 3.75	122. 3.83	34. 5.00	1. 5.08
ROUTED TO +	RCP27	1.21	1	FLOW TIME	588. 3.67	484. 3.75	421. 3.75	380. 3.75	332. 3.75	280. 3.83	121. 3.92	34. 4.17	1. 5.42
2 COMBINED AT +	CP24D	1.55	1	FLOW TIME	1599. 3.83	1107. 3.83	942. 3.83	852. 3.83	747. 3.92	650. 3.92	295. 4.08	111. 4.42	11. 5.83
HYDROGRAPH AT +	C5CB	.14	1	FLOW TIME	127. 3.75	111. 3.75	101. 3.75	95. 3.75	86. 3.75	78. 3.75	47. 3.75	24. 3.83	3. 3.92
2 COMBINED AT +	CP24E	1.69	1	FLOW TIME	1719. 3.83	1212. 3.83	1038. 3.83	941. 3.83	819. 3.92	716. 3.92	324. 4.08	119. 4.42	12. 5.83
HYDROGRAPH AT +	C5FD	.17	1	FLOW TIME	294. 3.50	261. 3.50	238. 3.50	225. 3.50	207. 3.50	189. 3.50	122. 3.50	70. 3.50	13. 3.50
ROUTED TO +	RC5FD	.17	1	FLOW TIME	259. 3.58	228. 3.58	209. 3.58	200. 3.58	180. 3.67	167. 3.67	113. 3.67	68. 3.67	15. 3.83
HYDROGRAPH AT +	C5FA	.51	1	FLOW TIME	1125. 3.50	1013. 3.50	937. 3.50	893. 3.50	831. 3.50	769. 3.50	529. 3.50	338. 3.50	106. 3.50
ROUTED TO +	RC5FA	.51	1	FLOW TIME	1021. 3.58	870. 3.58	812. 3.58	747. 3.58	694. 3.58	634. 3.58	442. 3.58	289. 3.67	122. 3.75
HYDROGRAPH AT +	C5FB	.26	1	FLOW TIME	167. 3.58	137. 3.58	118. 3.67	108. 3.67	94. 3.67	80. 3.67	34. 3.67	9. 3.83	0. .00
3 COMBINED AT +	CP28	.94	1	FLOW TIME	1447. 3.58	1235. 3.58	1137. 3.58	1053. 3.58	964. 3.58	876. 3.58	577. 3.67	364. 3.67	122. 3.75
ROUTED TO +	RCP28	.94	1	FLOW TIME	1315. 3.58	1135. 3.67	1064. 3.67	1006. 3.67	932. 3.67	849. 3.67	575. 3.67	334. 3.75	85. 3.92
HYDROGRAPH AT +	C5FC	.22	1	FLOW TIME	191. 3.58	161. 3.58	142. 3.58	131. 3.58	116. 3.58	101. 3.58	50. 3.67	18. 3.67	1. 4.92
2 COMBINED AT +	CP29	1.16	1	FLOW TIME	1506. 3.58	1285. 3.67	1197. 3.67	1130. 3.67	1042. 3.67	945. 3.67	624. 3.67	352. 3.75	85. 3.92
ROUTED TO +	RCP29	1.16	1	FLOW TIME	1497. 3.67	1266. 3.67	1192. 3.67	1080. 3.67	1007. 3.67	903. 3.67	625. 3.75	373. 3.83	65. 4.08
HYDROGRAPH AT +	C5EA	.49	1	FLOW TIME	690. 3.58	611. 3.58	557. 3.58	526. 3.58	483. 3.58	439. 3.58	278. 3.58	156. 3.58	25. 3.58
2 COMBINED AT +	CP30	1.65	1	FLOW TIME	2023. 3.67	1733. 3.67	1619. 3.67	1484. 3.67	1379. 3.67	1243. 3.67	797. 3.75	451. 3.83	76. 4.08
ROUTED TO +	RCP30	1.65	1	FLOW TIME	2027. 3.67	1711. 3.67	1567. 3.67	1444. 3.67	1322. 3.75	1191. 3.75	743. 3.75	435. 3.92	79. 4.25
HYDROGRAPH AT +	C5EB	.55	1	FLOW TIME	806. 3.67	726. 3.67	671. 3.67	640. 3.67	596. 3.67	551. 3.67	379. 3.67	243. 3.67	77. 3.67
ROUTED TO +	RC5EB	.55	1	FLOW TIME	781. 3.67	703. 3.75	652. 3.75	643. 3.75	600. 3.75	556. 3.75	387. 3.75	247. 3.75	74. 3.83
HYDROGRAPH AT +	C5EC	.22	1	FLOW TIME	179. 3.58	150. 3.58	131. 3.58	120. 3.58	105. 3.58	91. 3.58	41. 3.58	13. 3.75	0. 4.92
3 COMBINED AT +	CP31	2.41	1	FLOW TIME	2964. 3.67	2542. 3.67	2327. 3.67	2186. 3.67	1999. 3.75	1815. 3.75	1165. 3.75	639. 3.92	115. 4.25
ROUTED TO +	RCP31	2.41	1	FLOW TIME	2865. 3.75	2478. 3.75	2301. 3.75	2180. 3.75	1998. 3.75	1797. 3.75	1129. 3.83	598. 3.92	104. 4.42
HYDROGRAPH AT +	C5ED	.16	1	FLOW TIME	178. 3.58	154. 3.58	139. 3.58	130. 3.58	118. 3.58	106. 3.58	61. 3.58	31. 3.67	3. 3.83
2 COMBINED AT +	CP32	2.57	1	FLOW TIME	3001. 3.75	2597. 3.75	2409. 3.75	2281. 3.75	2091. 3.75	1881. 3.75	1171. 3.83	615. 3.92	105. 4.42
ROUTED TO +	RCP32	2.57	1	FLOW TIME	2990. 3.75	2578. 3.75	2370. 3.75	2246. 3.75	2036. 3.75	1821. 3.75	1142. 3.83	606. 4.00	107. 4.00
HYDROGRAPH AT +	C5DA	1.06	1	FLOW TIME	2210. 3.50	1984. 3.50	1830. 3.50	1740. 3.50	1616. 3.50	1489. 3.50	1009. 3.50	629. 3.50	179. 3.50

SDN3.OUT													
HYDROGRAPH AT	C5DB	.53	1	FLOW	1079.	973.	900.	858.	800.	740.	511.	328.	105.
+				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
3 COMBINED AT	CP33	4.17	1	FLOW	4356.	3797.	3411.	3193.	2920.	2638.	1651.	980.	285.
+				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
ROUTED TO	RCP33	4.17	1	FLOW	4193.	3631.	3315.	3146.	2865.	2576.	1491.	857.	283.
+				TIME	3.67	3.75	3.75	3.75	3.75	3.75	3.83	3.58	3.58
2 COMBINED AT	CP24	5.85	1	FLOW	5742.	4748.	4227.	3948.	3545.	3142.	1756.	900.	284.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.83	3.58	3.58
ROUTED TO	RCP24	5.85	1	FLOW	5646.	4681.	4158.	3871.	3476.	3074.	1736.	870.	261.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.83	3.58	3.67
HYDROGRAPH AT	C5DC	.33	1	FLOW	601.	534.	488.	462.	425.	388.	251.	145.	28.
+				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
ROUTED TO	RC5DC	.33	1	FLOW	515.	462.	405.	381.	355.	346.	192.	142.	22.
+				TIME	3.67	3.67	3.75	3.75	3.75	3.75	3.75	3.92	4.50
HYDROGRAPH AT	C4BD	.52	1	FLOW	409.	359.	325.	306.	280.	253.	156.	83.	13.
+				TIME	3.83	3.83	3.92	3.92	3.92	3.92	3.92	3.92	4.08
2 COMBINED AT	CP34A	.85	1	FLOW	843.	750.	705.	661.	610.	575.	339.	226.	30.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.83	3.92	4.50
2 COMBINED AT	CP34B	6.71	1	FLOW	6489.	5431.	4863.	4533.	4086.	3650.	2075.	1038.	265.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.83	3.92	3.67
ROUTED TO	DB4	6.71	1	FLOW	1713.	933.	245.	240.	233.	224.	193.	160.	83.
+				TIME	5.00	5.42	6.08	6.00	6.00	6.00	6.00	5.92	5.50
** PEAK STAGES IN FEET **													
1	STAGE			TIME	2069.58	2069.27	2068.55	2067.75	2066.73	2065.48	2061.26	2057.72	2052.18
					5.00	5.42	6.08	6.00	6.00	6.00	6.00	5.92	5.50
HYDROGRAPH AT	C4BF	.28	1	FLOW	417.	366.	332.	312.	285.	258.	158.	83.	8.
+				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.75
ROUTED TO	RC4BF	.28	1	FLOW	353.	314.	290.	276.	250.	233.	149.	70.	8.
+				TIME	3.58	3.58	3.67	3.67	3.67	3.67	3.67	3.67	5.08
HYDROGRAPH AT	C4BC	.24	1	FLOW	255.	223.	202.	190.	173.	156.	96.	51.	7.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.67	3.67	3.67	3.75
3 COMBINED AT	CP34	7.22	1	FLOW	1841.	960.	657.	626.	577.	538.	366.	210.	94.
+				TIME	5.00	5.42	3.67	3.67	3.67	3.67	3.67	3.67	5.08
ROUTED TO	RCP34	7.22	1	FLOW	1822.	1057.	663.	633.	593.	552.	381.	234.	93.
+				TIME	5.08	5.42	3.75	3.75	3.75	3.75	3.83	3.92	5.33
HYDROGRAPH AT	C4A1C	.52	1	FLOW	481.	420.	380.	357.	325.	292.	175.	93.	13.
+				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.75	3.75	3.83
HYDROGRAPH AT	RET5	.00	1	FLOW	544.	530.	431.	360.	267.	173.	43.	18.	3.
+				TIME	3.75	3.75	3.75	3.75	3.83	3.83	4.00	4.17	5.33
ROUTED TO	RDIV5	.00	1	FLOW	584.	575.	492.	429.	295.	197.	46.	19.	3.
+				TIME	3.83	3.83	3.92	3.92	4.00	4.00	4.17	4.58	5.08
3 COMBINED AT	CP35A	7.74	1	FLOW	1977.	1541.	1285.	1143.	943.	861.	542.	307.	98.
+				TIME	5.08	3.83	3.83	3.92	3.92	3.75	3.83	3.92	5.33
HYDROGRAPH AT	C4A1	.35	1	FLOW	248.	214.	191.	178.	160.	143.	81.	38.	4.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.83	3.83	5.00
2 COMBINED AT	CP35	8.09	1	FLOW	2047.	1751.	1474.	1303.	1103.	1004.	623.	344.	101.
+				TIME	5.08	3.83	3.83	3.92	3.75	3.75	3.83	3.92	5.33
ROUTED TO	RCP35	8.09	1	FLOW	2078.	1669.	1440.	1282.	1126.	1018.	639.	341.	106.
+				TIME	5.17	3.92	3.92	4.00	3.83	3.83	3.92	4.00	5.25
HYDROGRAPH AT	C4BE	.22	1	FLOW	241.	214.	196.	185.	170.	155.	99.	58.	13.
+				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75	3.83
ROUTED TO	RC4BE	.22	1	FLOW	241.	215.	197.	187.	173.	158.	101.	58.	18.
+				TIME	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.92	4.08
HYDROGRAPH AT	C4BB	.35	1	FLOW	377.	337.	309.	294.	272.	250.	166.	101.	26.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.83
2 COMBINED AT	CP36	.57	1	FLOW	615.	546.	499.	472.	435.	396.	256.	152.	35.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.83	3.83	4.08
ROUTED TO	RCP36	.57	1	FLOW	599.	535.	491.	463.	430.	396.	257.	154.	32.
+				TIME	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.92	4.25
HYDROGRAPH AT	C4A2B	.25	1	FLOW	203.	173.	153.	142.	126.	111.	56.	20.	1.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	4.92
2 COMBINED AT	CP37	.82	1	FLOW	704.	616.	560.	527.	485.	445.	285.	163.	32.
+				TIME	3.75	3.75	3.75	3.75	3.83	3.83	3.83	3.92	4.25
ROUTED TO	RCP37	.82	1	FLOW	695.	614.	559.	527.	479.	432.	278.	161.	31.
+				TIME	3.83	3.83	3.83	3.83	3.83	3.83	3.92	4.00	4.33
2 COMBINED AT													

+	CP38A	8.91	1	FLOW TIME	2644. 3.83	2251. 3.92	1977. 3.92	SDN3.OUT 1784. 3.83	1605. 3.83	1450. 3.83	917. 3.92	502. 4.00	122. 5.25
+	HYDROGRAPH AT												
+	C4A1B	.25	1	FLOW TIME	134. 3.67	110. 3.67	95. 3.67	87. 3.67	75. 3.67	64. 3.67	27. 3.75	7. 3.83	0. .00
+	3 COMBINED AT												
+	CP38	25.31	1	FLOW TIME	5128. 3.83	4464. 3.83	3968. 3.83	3719. 3.83	3396. 3.83	3019. 3.83	1738. 3.92	851. 4.00	212. 5.75
+	ROUTED TO												
+	RCP38	25.31	1	FLOW TIME	5089. 3.83	4425. 3.83	3941. 3.92	3681. 3.83	3349. 3.83	2965. 3.83	1707. 3.92	836. 4.08	210. 5.83
+	HYDROGRAPH AT												
+	C4CB	5.41	1	FLOW TIME	10493. 3.50	9383. 3.50	8626. 3.50	8188. 3.50	7580. 3.50	6962. 3.50	4634. 3.50	2816. 3.50	710. 3.50
+	ROUTED TO												
+	DB5	5.41	1	FLOW TIME	90. 6.00	88. 6.00	86. 6.00	85. 5.92	84. 5.83	82. 5.83	75. 5.50	67. 5.42	46. 5.17
				** PEAK STAGES IN FEET **									
			1	STAGE TIME	2488.66 6.00	2486.67 6.00	2485.22 6.00	2484.32 6.00	2483.07 5.92	2481.80 5.83	2476.22 5.50	2470.33 5.42	2458.34 5.17
+	ROUTED TO												
+	RDB5	5.41	1	FLOW TIME	90. 6.08	88. 6.08	86. 6.08	85. 6.08	84. 6.08	82. 6.08	75. 5.67	67. 5.50	47. 4.08
+	HYDROGRAPH AT												
+	C4CA	.20	1	FLOW TIME	237. 3.67	211. 3.67	193. 3.67	183. 3.67	169. 3.67	154. 3.67	101. 3.75	61. 3.75	15. 3.83
+	HYDROGRAPH AT												
+	C3B3E	.22	1	FLOW TIME	396. 3.58	359. 3.58	333. 3.58	318. 3.58	298. 3.58	277. 3.58	195. 3.58	130. 3.58	47. 3.58
+	3 COMBINED AT												
+	CP39	5.83	1	FLOW TIME	670. 3.58	607. 3.58	563. 3.58	538. 3.58	502. 3.58	466. 3.58	329. 3.67	217. 3.67	81. 3.83
+	ROUTED TO												
+	RCP39	5.83	1	FLOW TIME	667. 3.67	606. 3.67	556. 3.67	530. 3.67	504. 3.67	459. 3.67	321. 3.67	219. 3.67	83. 4.00
+	HYDROGRAPH AT												
+	C3B3D	.26	1	FLOW TIME	455. 3.58	411. 3.58	381. 3.58	364. 3.58	340. 3.58	315. 3.58	220. 3.58	144. 3.58	49. 3.58
+	2 COMBINED AT												
+	CP40	6.08	1	FLOW TIME	1059. 3.58	953. 3.58	883. 3.58	841. 3.58	785. 3.58	721. 3.58	503. 3.67	340. 3.67	99. 4.00
+	ROUTED TO												
+	RCP40	6.08	1	FLOW TIME	1043. 3.67	943. 3.67	869. 3.67	829. 3.67	780. 3.67	717. 3.67	498. 3.67	330. 3.67	94. 4.08
+	HYDROGRAPH AT												
+	C3B3C	1.24	1	FLOW TIME	2610. 3.50	2355. 3.50	2181. 3.50	2080. 3.50	1939. 3.50	1795. 3.50	1246. 3.50	805. 3.50	264. 3.50
+	ROUTED TO												
+	RC3B3C	1.24	1	FLOW TIME	2331. 3.50	2090. 3.50	1918. 3.58	1839. 3.58	1720. 3.58	1604. 3.58	1142. 3.58	753. 3.58	254. 3.58
+	HYDROGRAPH AT												
+	C3B3B	.32	1	FLOW TIME	508. 3.58	456. 3.58	420. 3.58	399. 3.58	371. 3.58	341. 3.58	231. 3.58	143. 3.58	41. 3.67
+	2 COMBINED AT												
+	CP41	1.56	1	FLOW TIME	2788. 3.58	2529. 3.58	2338. 3.58	2238. 3.58	2090. 3.58	1945. 3.58	1373. 3.58	896. 3.58	294. 3.58
+	ROUTED TO												
+	RCP41	1.56	1	FLOW TIME	2678. 3.67	2409. 3.58	2250. 3.67	2113. 3.67	2004. 3.67	1913. 3.67	1287. 3.67	811. 3.67	360. 3.75
+	HYDROGRAPH AT												
+	C3B3A	.51	1	FLOW TIME	838. 3.50	746. 3.50	684. 3.50	648. 3.50	598. 3.50	548. 3.50	359. 3.50	216. 3.58	56. 3.58
+	3 COMBINED AT												
+	CP42	8.15	1	FLOW TIME	4487. 3.58	4037. 3.58	3687. 3.58	3477. 3.58	3221. 3.58	3042. 3.58	2035. 3.67	1296. 3.67	492. 3.75
+	ROUTED TO												
+	RCP42	8.15	1	FLOW TIME	4538. 3.67	4097. 3.67	3705. 3.67	3481. 3.67	3226. 3.75	3060. 3.75	2114. 3.75	1346. 3.83	467. 4.00
+	HYDROGRAPH AT												
+	C4BA2	.14	1	FLOW TIME	123. 3.58	104. 3.58	92. 3.58	85. 3.58	76. 3.58	66. 3.58	34. 3.67	13. 3.67	1. 4.92
+	2 COMBINED AT												
+	CP43A	8.29	1	FLOW TIME	4651. 3.67	4194. 3.67	3791. 3.67	3561. 3.67	3291. 3.67	3113. 3.75	2143. 3.75	1357. 3.83	467. 4.00
+	ROUTED TO												
+	RCP43	8.29	1	FLOW TIME	5326. 3.92	4905. 3.92	4303. 3.92	3894. 4.00	3840. 4.00	3871. 4.00	2747. 4.08	1799. 4.25	660. 4.67
+	HYDROGRAPH AT												
+	C4BA3	.41	1	FLOW TIME	296. 3.83	256. 3.83	230. 3.92	216. 3.92	195. 3.92	175. 3.92	101. 3.92	48. 3.92	6. 5.08
+	ROUTED TO												
+	RC4BA3	.41	1	FLOW TIME	299. 4.00	260. 4.00	233. 4.00	218. 4.00	197. 4.00	176. 4.00	100. 4.08	45. 4.25	6. 5.58
+	HYDROGRAPH AT												
+	C4A2A	.26	1	FLOW TIME	322. 3.50	278. 3.50	249. 3.50	232. 3.50	208. 3.50	185. 3.50	102. 3.50	43. 3.50	3. 4.83
+	3 COMBINED AT												
+	CP44	8.96	1	FLOW TIME	5671. 3.92	5202. 3.92	4568. 3.92	4155. 4.00	4076. 4.00	4082. 4.00	2858. 4.08	1849. 4.25	662. 4.67
+	ROUTED TO												
+	RCP44	8.96	1	FLOW TIME	5372. 3.92	4754. 3.92	4232. 4.00	4134. 4.00	3964. 4.00	3787. 4.00	2539. 4.08	1708. 4.25	503. 4.67
+	HYDROGRAPH AT												
+	C4A1A	.25	1	FLOW TIME	109. 4.17	94. 4.17	83. 4.17	78. 4.17	70. 4.17	62. 4.17	34. 4.25	15. 4.25	2. 5.25
+	3 COMBINED AT												
+	CP45	34.52	1	FLOW	10360.	9220.	8070.	7729.	7177.	6645.	4142.	2441.	664.

				TIME	3.92	3.92	4.00	SDN3.OUT 4.00	4.00	4.00	4.08	4.25	4.67
ROUTED TO													
+	RCP45	34.52	1	FLOW TIME	10134. 3.92	8908. 3.92	8064. 4.00	7661. 4.00	7065. 4.00	6431. 4.00	3923. 4.08	2303. 4.25	614. 4.75
HYDROGRAPH AT													
+	C3A2B	.51	1	FLOW TIME	769. 3.58	687. 3.58	632. 3.58	599. 3.58	555. 3.58	509. 3.58	339. 3.58	205. 3.58	52. 3.58
ROUTED TO													
+	RC3A2B	.51	1	FLOW TIME	764. 3.67	683. 3.67	628. 3.67	595. 3.67	550. 3.67	481. 3.67	320. 3.67	196. 3.75	69. 3.83
HYDROGRAPH AT													
+	C4BA1	.48	1	FLOW TIME	289. 3.67	242. 3.67	211. 3.67	194. 3.67	170. 3.67	147. 3.67	69. 3.75	23. 3.83	1. 5.00
2 COMBINED AT													
+	CP46	.99	1	FLOW TIME	1052. 3.67	925. 3.67	839. 3.67	789. 3.67	721. 3.67	628. 3.67	387. 3.67	219. 3.75	69. 3.83
ROUTED TO													
+	RCP46	.99	1	FLOW TIME	1018. 3.75	879. 3.75	797. 3.75	755. 3.75	692. 3.75	608. 3.75	396. 3.75	229. 3.83	44. 4.17
HYDROGRAPH AT													
+	C3B1D	.25	1	FLOW TIME	215. 3.50	180. 3.50	157. 3.50	144. 3.50	127. 3.50	109. 3.50	48. 3.50	11. 3.75	0. 5.75
2 COMBINED AT													
+	CP47	1.24	1	FLOW TIME	1104. 3.75	953. 3.75	863. 3.75	816. 3.75	747. 3.75	657. 3.75	423. 3.75	234. 3.83	44. 4.17
ROUTED TO													
+	RCP47	1.24	1	FLOW TIME	1098. 3.75	935. 3.75	840. 3.75	789. 3.75	717. 3.83	634. 3.83	433. 3.83	220. 3.92	42. 4.25
HYDROGRAPH AT													
+	C3B1C	.24	1	FLOW TIME	374. 3.50	331. 3.50	302. 3.50	285. 3.50	262. 3.50	238. 3.50	151. 3.50	85. 3.50	13. 3.50
3 COMBINED AT													
+	CP48	36.00	1	FLOW TIME	11007. 3.92	9699. 3.92	8664. 4.00	8235. 4.00	7601. 4.00	6932. 4.00	4194. 4.08	2427. 4.25	636. 4.75
ROUTED TO													
+	RCP48	36.00	1	FLOW TIME	10796. 3.92	9417. 3.92	8629. 4.00	8154. 4.00	7483. 4.00	6731. 4.00	4001. 4.08	2281. 4.25	605. 4.75
HYDROGRAPH AT													
+	C3B1B	.21	1	FLOW TIME	139. 3.67	118. 3.67	104. 3.67	96. 3.67	85. 3.67	74. 3.67	37. 3.67	14. 3.75	1. 5.00
ROUTED TO													
+	RC3B1B	.21	1	FLOW TIME	137. 3.75	117. 3.75	102. 3.75	94. 3.75	85. 3.75	73. 3.75	36. 3.83	14. 3.92	1. 5.25
HYDROGRAPH AT													
+	C3B1A	.24	1	FLOW TIME	170. 3.67	146. 3.67	129. 3.67	120. 3.67	107. 3.67	94. 3.67	49. 3.67	21. 3.75	2. 4.92
3 COMBINED AT													
+	CP49	36.46	1	FLOW TIME	11001. 3.92	9594. 3.92	8756. 4.00	8273. 4.00	7590. 4.00	6827. 4.00	4046. 4.08	2297. 4.25	606. 4.75
ROUTED TO													
+	RCP49	36.46	1	FLOW TIME	10681. 3.92	9463. 4.00	8677. 4.00	8134. 4.00	7387. 4.00	6542. 4.00	3959. 4.17	2151. 4.33	564. 4.83
HYDROGRAPH AT													
+	C3A2A	.47	1	FLOW TIME	825. 3.50	741. 3.50	684. 3.50	651. 3.50	605. 3.50	558. 3.50	380. 3.50	239. 3.50	72. 3.58
ROUTED TO													
+	RC3A2A	.47	1	FLOW TIME	774. 3.83	702. 3.83	661. 3.83	622. 3.83	571. 3.83	523. 3.83	365. 3.92	235. 3.92	100. 4.08
HYDROGRAPH AT													
+	C3A1B	1.02	1	FLOW TIME	1403. 3.50	1230. 3.50	1114. 3.50	1047. 3.50	954. 3.50	861. 3.50	520. 3.50	269. 3.50	31. 3.75
2 COMBINED AT													
+	CP50	1.49	1	FLOW TIME	1434. 3.50	1259. 3.50	1139. 3.50	1074. 3.50	979. 3.50	884. 3.50	536. 3.50	306. 3.92	113. 4.08
ROUTED TO													
+	RCP50	1.49	1	FLOW TIME	1369. 3.58	1191. 3.58	1071. 3.58	1004. 3.58	913. 3.58	818. 3.58	514. 3.58	292. 4.00	122. 4.17
HYDROGRAPH AT													
+	C3A1A	.37	1	FLOW TIME	433. 3.50	377. 3.50	339. 3.50	317. 3.50	288. 3.50	258. 3.50	150. 3.50	72. 3.50	6. 4.83
3 COMBINED AT													
+	CP51	38.32	1	FLOW TIME	11769. 3.92	10276. 4.00	9440. 4.00	8873. 4.00	8089. 4.00	7200. 4.00	4232. 4.17	2290. 4.33	608. 4.83

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SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR PLAN = 1	RATIO=	.00							
RDB1	MANE	5.00	198.15	330.00	1.35	5.00	198.15	330.00	1.35

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2901E+03 EXCESS= .0000E+00 OUTFLOW= .2882E+03 BASIN STORAGE= .1925E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RDB1	MANE	5.00	189.58	330.00	1.25	5.00	189.58	330.00	1.25

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2687E+03 EXCESS= .0000E+00 OUTFLOW= .2670E+03 BASIN STORAGE= .1688E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RDB1	MANE	5.00	183.52	330.00	1.17	5.00	183.52	330.00	1.17

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2527E+03 EXCESS= .0000E+00 OUTFLOW= .2513E+03 BASIN STORAGE= .1503E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00

RDB1	MANE	5.00	179.83	330.00	1.13	5.00	SDN3.OUT 179.83	330.00	1.13
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .2428E+03 EXCESS= .0000E+00 OUTFLOW= .2415E+03 BASIN STORAGE= .1371E+01 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RDB1	MANE	5.00	174.55	325.00	1.06	5.00	174.55	325.00	1.06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2282E+03 EXCESS= .0000E+00 OUTFLOW= .2272E+03 BASIN STORAGE= .1133E+01 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RDB1	MANE	5.00	168.69	325.00	.98	5.00	168.69	325.00	.98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2112E+03 EXCESS= .0000E+00 OUTFLOW= .2106E+03 BASIN STORAGE= .7315E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RDB1	MANE	5.00	141.81	325.00	.64	5.00	141.81	325.00	.64

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1375E+03 EXCESS= .0000E+00 OUTFLOW= .1375E+03 BASIN STORAGE= .6901E-01 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RDB1	MANE	5.00	113.87	325.00	.38	5.00	113.87	325.00	.38

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8080E+02 EXCESS= .0000E+00 OUTFLOW= .8079E+02 BASIN STORAGE= .5011E-01 PERCENT ERROR= -.1

FOR PLAN	= 1	RATIO=	.00						
RDB1	MANE	5.00	61.59	320.00	.10	5.00	61.59	320.00	.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2042E+02 EXCESS= .0000E+00 OUTFLOW= .2042E+02 BASIN STORAGE= .3159E-01 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.46	480.08	241.54	1.35	5.00	478.34	240.00	1.35

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3212E+03 EXCESS= .0000E+00 OUTFLOW= .3208E+03 BASIN STORAGE= .3452E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.49	433.67	241.80	1.24	5.00	432.00	240.00	1.24

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2959E+03 EXCESS= .0000E+00 OUTFLOW= .2956E+03 BASIN STORAGE= .3032E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.52	402.19	241.86	1.17	5.00	400.32	240.00	1.17

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2773E+03 EXCESS= .0000E+00 OUTFLOW= .2771E+03 BASIN STORAGE= .2709E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.54	384.30	241.60	1.12	5.00	382.03	240.00	1.12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2661E+03 EXCESS= .0000E+00 OUTFLOW= .2659E+03 BASIN STORAGE= .2471E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.56	358.96	242.52	1.05	5.00	357.10	240.00	1.05

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2496E+03 EXCESS= .0000E+00 OUTFLOW= .2494E+03 BASIN STORAGE= .2088E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.59	333.49	242.33	.97	5.00	331.41	240.00	.97

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2309E+03 EXCESS= .0000E+00 OUTFLOW= .2308E+03 BASIN STORAGE= .1360E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.74	236.24	246.84	.63	5.00	235.93	245.00	.63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1501E+03 EXCESS= .0000E+00 OUTFLOW= .1501E+03 BASIN STORAGE= .1248E-01 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	1.92	160.01	247.23	.37	5.00	158.70	245.00	.37

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8774E+02 EXCESS= .0000E+00 OUTFLOW= .8774E+02 BASIN STORAGE= .9090E-02 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP2	MANE	2.36	69.60	314.21	.09	5.00	69.56	315.00	.09

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2179E+02 EXCESS= .0000E+00 OUTFLOW= .2179E+02 BASIN STORAGE= .5748E-02 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP3	MANE	3.93	635.79	228.00	1.36	5.00	635.28	225.00	1.36

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3444E+03 EXCESS= .0000E+00 OUTFLOW= .3435E+03 BASIN STORAGE= .1006E+01 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP3	MANE	4.04	571.78	230.39	1.25	5.00	571.12	230.00	1.25

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3162E+03 EXCESS= .0000E+00 OUTFLOW= .3154E+03 BASIN STORAGE= .8864E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP3	MANE	4.13	526.86	231.06	1.17	5.00	524.86	230.00	1.17

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2962E+03 EXCESS= .0000E+00 OUTFLOW= .2954E+03 BASIN STORAGE= .7924E+00 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP3	MANE	4.18	498.96	229.80	1.12	5.00	498.94	230.00	1.12

										SDN3.OUT
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2836E+03 EXCESS= .0000E+00 OUTFLOW= .2829E+03 BASIN STORAGE= .7255E+00 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP3	MANE	4.26	463.22	234.07	1.05	5.00	462.37	230.00	1.05	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2659E+03 EXCESS= .0000E+00 OUTFLOW= .2654E+03 BASIN STORAGE= .6257E+00 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP3	MANE	4.34	426.96	234.57	.97	5.00	426.22	235.00	.97	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2458E+03 EXCESS= .0000E+00 OUTFLOW= .2455E+03 BASIN STORAGE= .4070E+00 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP3	MANE	4.78	291.16	234.41	.63	5.00	291.00	235.00	.63	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1598E+03 EXCESS= .0000E+00 OUTFLOW= .1598E+03 BASIN STORAGE= .3686E-01 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP3	MANE	4.75	185.86	247.00	.37	5.00	185.51	245.00	.37	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9342E+02 EXCESS= .0000E+00 OUTFLOW= .9341E+02 BASIN STORAGE= .2671E-01 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP3	MANE	5.00	75.86	305.00	.09	5.00	75.86	305.00	.09	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2327E+02 EXCESS= .0000E+00 OUTFLOW= .2326E+02 BASIN STORAGE= .1687E-01 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	4.67	1519.65	219.37	1.38	5.00	1496.99	220.00	1.38	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4046E+03 EXCESS= .0000E+00 OUTFLOW= .4033E+03 BASIN STORAGE= .1489E+01 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	4.81	1296.36	221.33	1.26	5.00	1287.32	220.00	1.26	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3690E+03 EXCESS= .0000E+00 OUTFLOW= .3679E+03 BASIN STORAGE= .1316E+01 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	4.92	1184.04	221.53	1.18	5.00	1173.01	220.00	1.18	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3441E+03 EXCESS= .0000E+00 OUTFLOW= .3431E+03 BASIN STORAGE= .1180E+01 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	5.00	1161.03	219.81	1.13	5.00	1155.95	220.00	1.13	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3292E+03 EXCESS= .0000E+00 OUTFLOW= .3283E+03 BASIN STORAGE= .1078E+01 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	5.00	1072.87	220.00	1.05	5.00	1072.87	220.00	1.05	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3077E+03 EXCESS= .0000E+00 OUTFLOW= .3070E+03 BASIN STORAGE= .9432E+00 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	5.00	977.17	220.00	.97	5.00	977.17	220.00	.97	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2839E+03 EXCESS= .0000E+00 OUTFLOW= .2835E+03 BASIN STORAGE= .6249E+00 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	5.00	600.48	220.00	.63	5.00	600.48	220.00	.63	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1843E+03 EXCESS= .0000E+00 OUTFLOW= .1843E+03 BASIN STORAGE= .5627E-01 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	3.75	310.14	221.25	.37	5.00	295.76	220.00	.37	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1076E+03 EXCESS= .0000E+00 OUTFLOW= .1076E+03 BASIN STORAGE= .3975E-01 PERCENT ERROR= .0										
FOR PLAN = 1 RATIO= .00										
RCP4	MANE	3.75	94.30	300.00	.09	5.00	94.30	300.00	.09	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2667E+02 EXCESS= .0000E+00 OUTFLOW= .2667E+02 BASIN STORAGE= .2527E-01 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
CSICB	MANE	3.95	810.67	217.01	1.34	5.00	799.18	220.00	1.34	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5231E+02 EXCESS= .0000E+00 OUTFLOW= .5235E+02 BASIN STORAGE= .6127E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
CSICB	MANE	4.15	719.90	219.95	1.16	5.00	718.93	220.00	1.17	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4552E+02 EXCESS= .0000E+00 OUTFLOW= .4556E+02 BASIN STORAGE= .5705E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
CSICB	MANE	4.31	653.22	219.92	1.05	5.00	651.81	220.00	1.05	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4100E+02 EXCESS= .0000E+00 OUTFLOW= .4104E+02 BASIN STORAGE= .6286E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
CSICB	MANE	4.42	599.48	220.83	.98	5.00	594.39	220.00	.98	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3830E+02 EXCESS= .0000E+00 OUTFLOW= .3834E+02 BASIN STORAGE= .5643E-02 PERCENT ERROR= -.1										

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FOR PLAN = 1	RATIO=	.00							
CSICB	MANE	3.75	542.44	217.50	.89	5.00	539.00	220.00	.89
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3478E+02 EXCESS= .0000E+00 OUTFLOW= .3482E+02 BASIN STORAGE= .5931E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
CSICB	MANE	3.50	492.01	220.50	.80	5.00	489.46	220.00	.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3128E+02 EXCESS= .0000E+00 OUTFLOW= .3131E+02 BASIN STORAGE= .4294E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
CSICB	MANE	2.75	291.25	220.00	.48	5.00	291.25	220.00	.48
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1866E+02 EXCESS= .0000E+00 OUTFLOW= .1869E+02 BASIN STORAGE= .5355E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
CSICB	MANE	1.25	144.56	222.50	.25	5.00	138.48	225.00	.25
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9804E+01 EXCESS= .0000E+00 OUTFLOW= .9818E+01 BASIN STORAGE= .4604E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
CSICB	MANE	1.25	18.30	240.00	.04	5.00	18.30	240.00	.04
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1546E+01 EXCESS= .0000E+00 OUTFLOW= .1559E+01 BASIN STORAGE= .5281E-02 PERCENT ERROR= -1.2									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	3.70	308.00	369.71	1.01	5.00	308.00	370.00	1.01
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5124E+03 EXCESS= .0000E+00 OUTFLOW= .5110E+03 BASIN STORAGE= .1430E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	3.73	294.23	369.37	.95	5.00	294.22	370.00	.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4822E+03 EXCESS= .0000E+00 OUTFLOW= .4809E+03 BASIN STORAGE= .1342E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	3.76	283.80	368.29	.91	5.00	283.80	370.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4603E+03 EXCESS= .0000E+00 OUTFLOW= .4591E+03 BASIN STORAGE= .1271E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	3.77	277.69	369.90	.88	5.00	277.69	370.00	.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4476E+03 EXCESS= .0000E+00 OUTFLOW= .4464E+03 BASIN STORAGE= .1228E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	3.80	269.41	368.35	.84	5.00	269.40	365.00	.84
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4279E+03 EXCESS= .0000E+00 OUTFLOW= .4267E+03 BASIN STORAGE= .1169E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	3.83	259.15	367.39	.80	5.00	259.15	365.00	.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4071E+03 EXCESS= .0000E+00 OUTFLOW= .4061E+03 BASIN STORAGE= .1091E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	3.96	217.18	360.78	.61	5.00	217.18	360.00	.61
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3086E+03 EXCESS= .0000E+00 OUTFLOW= .3081E+03 BASIN STORAGE= .4811E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	4.13	176.95	346.96	.36	5.00	176.95	350.00	.36
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1805E+03 EXCESS= .0000E+00 OUTFLOW= .1804E+03 BASIN STORAGE= .1616E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB2	MANE	4.62	101.03	328.02	.09	5.00	101.03	330.00	.09
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4343E+02 EXCESS= .0000E+00 OUTFLOW= .4342E+02 BASIN STORAGE= .9988E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RG2B1	MANE	5.00	267.24	245.00	.92	5.00	267.24	245.00	.92
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2554E+02 EXCESS= .0000E+00 OUTFLOW= .2564E+02 BASIN STORAGE= .1537E-01 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO=	.00							
RG2B1	MANE	4.25	221.60	246.50	.78	5.00	218.75	245.00	.78
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2170E+02 EXCESS= .0000E+00 OUTFLOW= .2179E+02 BASIN STORAGE= .1525E-01 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO=	.00							
RG2B1	MANE	4.00	192.30	248.00	.69	5.00	191.70	245.00	.69
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1917E+02 EXCESS= .0000E+00 OUTFLOW= .1927E+02 BASIN STORAGE= .1626E-01 PERCENT ERROR= -.6									
FOR PLAN = 1	RATIO=	.00							
RG2B1	MANE	3.75	184.71	247.50	.64	5.00	173.12	250.00	.64
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1774E+02 EXCESS= .0000E+00 OUTFLOW= .1784E+02 BASIN STORAGE= .1806E-01 PERCENT ERROR= -.7									
FOR PLAN = 1	RATIO=	.00							
RG2B1	MANE	3.00	172.02	246.00	.57	5.00	156.97	245.00	.57

SDN3.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1581E+02 EXCESS= .0000E+00 OUTFLOW= .1590E+02 BASIN STORAGE= .1754E-01 PERCENT ERROR= -.7

FOR PLAN = 1 RATIO= .00
RG2B1 MANE 2.75 155.74 247.50 .50 5.00 132.04 255.00 .50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1390E+02 EXCESS= .0000E+00 OUTFLOW= .1400E+02 BASIN STORAGE= .1723E-01 PERCENT ERROR= -.8

FOR PLAN = 1 RATIO= .00
RG2B1 MANE 2.50 90.63 250.00 .27 5.00 90.63 250.00 .27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7366E+01 EXCESS= .0000E+00 OUTFLOW= .7463E+01 BASIN STORAGE= .1619E-01 PERCENT ERROR= -1.5

FOR PLAN = 1 RATIO= .00
RG2B1 MANE 2.25 42.09 267.75 .12 5.00 33.56 275.00 .12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3178E+01 EXCESS= .0000E+00 OUTFLOW= .3251E+01 BASIN STORAGE= .1770E-01 PERCENT ERROR= -2.9

FOR PLAN = 1 RATIO= .00
RG2B1 MANE 3.50 2.39 420.00 .00 5.00 2.39 420.00 .00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1133E+00 EXCESS= .0000E+00 OUTFLOW= .1274E+00 BASIN STORAGE= .1527E-01 PERCENT ERROR= -25.9

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 5.00 308.14 230.00 1.20 5.00 308.14 230.00 1.20

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2214E+02 EXCESS= .0000E+00 OUTFLOW= .2220E+02 BASIN STORAGE= .1420E-01 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 5.00 269.57 230.00 1.04 5.00 269.57 230.00 1.04

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1918E+02 EXCESS= .0000E+00 OUTFLOW= .1926E+02 BASIN STORAGE= .1322E-01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 4.75 236.68 228.00 .93 5.00 233.52 230.00 .93

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1720E+02 EXCESS= .0000E+00 OUTFLOW= .1726E+02 BASIN STORAGE= .1338E-01 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 4.50 225.60 229.50 .87 5.00 223.96 230.00 .88

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1611E+02 EXCESS= .0000E+00 OUTFLOW= .1618E+02 BASIN STORAGE= .1269E-01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 4.25 199.84 229.50 .79 5.00 199.21 230.00 .79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1456E+02 EXCESS= .0000E+00 OUTFLOW= .1462E+02 BASIN STORAGE= .1239E-01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 4.25 177.14 233.75 .71 5.00 175.56 230.00 .71

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1304E+02 EXCESS= .0000E+00 OUTFLOW= .1310E+02 BASIN STORAGE= .1197E-01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 2.25 116.52 234.00 .42 5.00 105.21 235.00 .41

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7646E+01 EXCESS= .0000E+00 OUTFLOW= .7704E+01 BASIN STORAGE= .1491E-01 PERCENT ERROR= -.9

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 1.75 61.30 236.25 .22 5.00 37.84 250.00 .20

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3913E+01 EXCESS= .0000E+00 OUTFLOW= .3978E+01 BASIN STORAGE= .1253E-01 PERCENT ERROR= -2.0

FOR PLAN = 1 RATIO= .00
RC1G2A MANE 2.50 6.80 287.50 .03 5.00 5.44 330.00 .03

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5365E+00 EXCESS= .0000E+00 OUTFLOW= .5574E+00 BASIN STORAGE= .1328E-01 PERCENT ERROR= -6.4

FOR PLAN = 1 RATIO= .00
RCP7 MANE 3.45 809.92 272.64 .98 5.00 808.54 270.00 .98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5857E+03 EXCESS= .0000E+00 OUTFLOW= .5836E+03 BASIN STORAGE= .2403E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP7 MANE 3.65 706.01 273.55 .91 5.00 705.33 275.00 .91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5426E+03 EXCESS= .0000E+00 OUTFLOW= .5407E+03 BASIN STORAGE= .2298E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP7 MANE 3.81 634.59 277.80 .86 5.00 634.50 275.00 .86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5130E+03 EXCESS= .0000E+00 OUTFLOW= .5111E+03 BASIN STORAGE= .2208E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP7 MANE 3.91 594.24 277.34 .83 5.00 593.23 275.00 .83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4953E+03 EXCESS= .0000E+00 OUTFLOW= .4935E+03 BASIN STORAGE= .2154E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP7 MANE 4.07 538.01 280.50 .78 5.00 537.90 280.00 .79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4699E+03 EXCESS= .0000E+00 OUTFLOW= .4682E+03 BASIN STORAGE= .2079E+01 PERCENT ERROR= -.1

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FOR PLAN = 1	RATIO=	.00							
RCP7	MANE	4.24	484.25	284.15	.74	5.00	484.05	285.00	.74

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4434E+03 EXCESS= .0000E+00 OUTFLOW= .4417E+03 BASIN STORAGE= .1982E+01 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCP7	MANE	4.99	323.13	329.01	.55	5.00	323.09	325.00	.55

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3283E+03 EXCESS= .0000E+00 OUTFLOW= .3272E+03 BASIN STORAGE= .1280E+01 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCP7	MANE	5.00	217.00	350.00	.33	5.00	217.00	350.00	.33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1940E+03 EXCESS= .0000E+00 OUTFLOW= .1940E+03 BASIN STORAGE= .1029E+00 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP7	MANE	5.00	92.80	415.00	.07	5.00	92.80	415.00	.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4460E+02 EXCESS= .0000E+00 OUTFLOW= .4460E+02 BASIN STORAGE= .6035E-01 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	1.79	702.28	210.68	1.53	5.00	675.31	210.00	1.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3385E+02 EXCESS= .0000E+00 OUTFLOW= .3387E+02 BASIN STORAGE= .3174E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	1.87	633.34	211.42	1.35	5.00	596.99	210.00	1.35

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2984E+02 EXCESS= .0000E+00 OUTFLOW= .2986E+02 BASIN STORAGE= .3696E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	1.94	576.19	211.24	1.23	5.00	541.54	210.00	1.23

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2713E+02 EXCESS= .0000E+00 OUTFLOW= .2715E+02 BASIN STORAGE= .3634E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	1.98	554.47	211.95	1.16	5.00	518.81	210.00	1.16

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2565E+02 EXCESS= .0000E+00 OUTFLOW= .2567E+02 BASIN STORAGE= .3154E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	2.05	491.43	210.74	1.06	5.00	469.10	210.00	1.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2347E+02 EXCESS= .0000E+00 OUTFLOW= .2349E+02 BASIN STORAGE= .3021E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	2.12	467.08	212.06	.97	5.00	431.06	210.00	.97

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2139E+02 EXCESS= .0000E+00 OUTFLOW= .2141E+02 BASIN STORAGE= .3763E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	2.52	291.93	211.63	.61	5.00	263.57	210.00	.61

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1356E+02 EXCESS= .0000E+00 OUTFLOW= .1357E+02 BASIN STORAGE= .3062E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	2.50	178.06	212.50	.36	5.00	155.27	215.00	.35

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7830E+01 EXCESS= .0000E+00 OUTFLOW= .7844E+01 BASIN STORAGE= .4090E-02 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO=	.00							
RCINA	MANE	.75	36.67	214.50	.08	5.00	36.14	215.00	.08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1868E+01 EXCESS= .0000E+00 OUTFLOW= .1872E+01 BASIN STORAGE= .3132E-02 PERCENT ERROR= -.4

FOR PLAN = 1	RATIO=	.00							
RCP8	MANE	2.05	942.27	276.25	1.00	5.00	938.07	275.00	1.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6170E+03 EXCESS= .0000E+00 OUTFLOW= .6158E+03 BASIN STORAGE= .1518E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP8	MANE	2.15	827.93	277.97	.92	5.00	821.20	275.00	.92

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5707E+03 EXCESS= .0000E+00 OUTFLOW= .5695E+03 BASIN STORAGE= .1452E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP8	MANE	2.24	748.50	278.22	.87	5.00	739.83	280.00	.87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5387E+03 EXCESS= .0000E+00 OUTFLOW= .5375E+03 BASIN STORAGE= .1394E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP8	MANE	2.30	701.91	278.54	.84	5.00	695.17	280.00	.84

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5194E+03 EXCESS= .0000E+00 OUTFLOW= .5182E+03 BASIN STORAGE= .1360E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP8	MANE	2.39	641.12	277.31	.79	5.00	635.06	280.00	.79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4921E+03 EXCESS= .0000E+00 OUTFLOW= .4909E+03 BASIN STORAGE= .1313E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP8	MANE	2.50	574.17	277.30	.75	5.00	572.43	280.00	.75

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4631E+03 EXCESS= .0000E+00 OUTFLOW= .4621E+03 BASIN STORAGE= .1253E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP8 MANE 2.99 360.34 296.28 .55 5.00 357.65 295.00 .55

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3411E+03 EXCESS= .0000E+00 OUTFLOW= .3404E+03 BASIN STORAGE= .8138E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP8 MANE 3.65 221.81 354.40 .33 5.00 221.46 355.00 .33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2018E+03 EXCESS= .0000E+00 OUTFLOW= .2018E+03 BASIN STORAGE= .6901E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP8 MANE 5.00 92.80 420.00 .08 5.00 92.80 420.00 .08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4647E+02 EXCESS= .0000E+00 OUTFLOW= .4646E+02 BASIN STORAGE= .3867E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCSGC MANE 2.97 198.58 211.16 1.73 5.00 186.52 210.00 1.73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1020E+02 EXCESS= .0000E+00 OUTFLOW= .1022E+02 BASIN STORAGE= .2913E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCSGC MANE 3.11 178.59 211.63 1.53 5.00 164.03 210.00 1.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9006E+01 EXCESS= .0000E+00 OUTFLOW= .9020E+01 BASIN STORAGE= .3281E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCSGC MANE 3.22 169.15 212.54 1.40 5.00 149.69 210.00 1.40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8265E+01 EXCESS= .0000E+00 OUTFLOW= .8279E+01 BASIN STORAGE= .3143E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCSGC MANE 3.29 157.79 213.81 1.32 5.00 142.21 210.00 1.32

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7805E+01 EXCESS= .0000E+00 OUTFLOW= .7819E+01 BASIN STORAGE= .4020E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCSGC MANE 3.39 146.80 213.83 1.22 5.00 132.71 215.00 1.22

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7172E+01 EXCESS= .0000E+00 OUTFLOW= .7184E+01 BASIN STORAGE= .3065E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCSGC MANE 3.51 130.35 214.33 1.11 5.00 122.70 215.00 1.11

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6530E+01 EXCESS= .0000E+00 OUTFLOW= .6543E+01 BASIN STORAGE= .3303E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCSGC MANE 3.75 90.57 213.75 .72 5.00 84.45 215.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4248E+01 EXCESS= .0000E+00 OUTFLOW= .4258E+01 BASIN STORAGE= .3279E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCSGC MANE 2.50 55.39 215.00 .42 5.00 55.39 215.00 .42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2478E+01 EXCESS= .0000E+00 OUTFLOW= .2483E+01 BASIN STORAGE= .3757E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCSGC MANE .75 15.39 216.00 .11 5.00 11.46 220.00 .11

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6382E+00 EXCESS= .0000E+00 OUTFLOW= .6419E+00 BASIN STORAGE= .2846E-02 PERCENT ERROR= -1.0

FOR PLAN = 1 RATIO= .00
RCP9 MANE 3.04 610.87 216.10 1.68 5.00 597.64 215.00 1.68

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3891E+02 EXCESS= .0000E+00 OUTFLOW= .3894E+02 BASIN STORAGE= .5978E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP9 MANE 3.19 543.36 216.62 1.48 5.00 526.14 215.00 1.48

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3438E+02 EXCESS= .0000E+00 OUTFLOW= .3441E+02 BASIN STORAGE= .5831E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP9 MANE 3.30 498.01 217.99 1.35 5.00 481.37 215.00 1.35

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3129E+02 EXCESS= .0000E+00 OUTFLOW= .3131E+02 BASIN STORAGE= .4458E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP9 MANE 3.37 462.75 215.64 1.27 5.00 452.88 215.00 1.27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2954E+02 EXCESS= .0000E+00 OUTFLOW= .2956E+02 BASIN STORAGE= .5664E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP9 MANE 3.48 426.16 219.13 1.17 5.00 414.43 215.00 1.17

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2713E+02 EXCESS= .0000E+00 OUTFLOW= .2715E+02 BASIN STORAGE= .5964E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP9 MANE 3.60 389.60 216.28 1.06 5.00 379.35 220.00 1.06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2468E+02 EXCESS= .0000E+00 OUTFLOW= .2471E+02 BASIN STORAGE= .5665E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00								
RCP9	MANE	4.28	257.06	218.31	.68	5.00	247.53	220.00	.68	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1577E+02 EXCESS= .0000E+00 OUTFLOW= .1580E+02 BASIN STORAGE= .5589E-02 PERCENT ERROR= -.2										
FOR PLAN = 1	RATIO=	.00								
RCP9	MANE	3.25	152.12	221.00	.39	5.00	149.54	220.00	.39	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9127E+01 EXCESS= .0000E+00 OUTFLOW= .9147E+01 BASIN STORAGE= .5226E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RCP9	MANE	1.25	33.49	227.50	.10	5.00	30.78	225.00	.10	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2224E+01 EXCESS= .0000E+00 OUTFLOW= .2233E+01 BASIN STORAGE= .4714E-02 PERCENT ERROR= -.6										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	3.64	661.85	218.13	1.28	5.00	660.04	220.00	1.28	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4839E+02 EXCESS= .0000E+00 OUTFLOW= .4843E+02 BASIN STORAGE= .5715E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	3.84	584.76	219.02	1.12	5.00	582.49	220.00	1.12	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4226E+02 EXCESS= .0000E+00 OUTFLOW= .4230E+02 BASIN STORAGE= .6080E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	3.99	530.15	219.36	1.01	5.00	528.92	220.00	1.01	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3803E+02 EXCESS= .0000E+00 OUTFLOW= .3807E+02 BASIN STORAGE= .5563E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	4.08	497.43	220.47	.95	5.00	490.79	220.00	.95	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3564E+02 EXCESS= .0000E+00 OUTFLOW= .3569E+02 BASIN STORAGE= .6116E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	4.23	452.51	219.73	.86	5.00	452.37	220.00	.86	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3248E+02 EXCESS= .0000E+00 OUTFLOW= .3252E+02 BASIN STORAGE= .6539E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	4.39	409.42	224.01	.78	5.00	405.45	220.00	.78	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2932E+02 EXCESS= .0000E+00 OUTFLOW= .2936E+02 BASIN STORAGE= .6479E-02 PERCENT ERROR= -.2										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	5.00	255.39	225.00	.47	5.00	255.39	225.00	.47	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1772E+02 EXCESS= .0000E+00 OUTFLOW= .1776E+02 BASIN STORAGE= .7716E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	3.75	141.34	225.00	.26	5.00	141.34	225.00	.26	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9686E+01 EXCESS= .0000E+00 OUTFLOW= .9732E+01 BASIN STORAGE= .5452E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	1.50	51.54	238.50	.06	5.00	22.36	255.00	.06	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2288E+01 EXCESS= .0000E+00 OUTFLOW= .2327E+01 BASIN STORAGE= .5964E-02 PERCENT ERROR= -2.0										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	3.75	642.67	225.10	1.28	5.00	642.39	225.00	1.28	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4841E+02 EXCESS= .0000E+00 OUTFLOW= .4846E+02 BASIN STORAGE= .6251E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	3.94	576.54	224.81	1.12	5.00	574.53	225.00	1.12	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4226E+02 EXCESS= .0000E+00 OUTFLOW= .4232E+02 BASIN STORAGE= .6382E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	4.10	521.75	225.46	1.01	5.00	518.01	225.00	1.01	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3804E+02 EXCESS= .0000E+00 OUTFLOW= .3810E+02 BASIN STORAGE= .5903E-02 PERCENT ERROR= -.2										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	4.22	490.42	223.86	.95	5.00	485.30	225.00	.95	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3574E+02 EXCESS= .0000E+00 OUTFLOW= .3579E+02 BASIN STORAGE= .7173E-02 PERCENT ERROR= -.2										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	4.36	444.27	226.92	.86	5.00	436.68	225.00	.86	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3250E+02 EXCESS= .0000E+00 OUTFLOW= .3255E+02 BASIN STORAGE= .6309E-02 PERCENT ERROR= -.2										
FOR PLAN = 1	RATIO=	.00								
RCP10	MANE	4.56	397.81	227.96	.78	5.00	395.14	225.00	.78	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2940E+02 EXCESS= .0000E+00 OUTFLOW= .2945E+02 BASIN STORAGE= .7586E-02 PERCENT ERROR= -.2										
FOR PLAN = 1 RATIO= .00										

	RCPI0	MANE					SDN3.OUT		
			5.00	273.08	225.00	.47	5.00	273.08	225.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1776E+02	EXCESS=	.0000E+00	OUTFLOW=	.1784E+02	BASIN STORAGE=	.5982E-02	PERCENT ERROR=	-.4
FOR PLAN = 1	RATIO=	.00							
RCPI0	MANE	4.25	154.30	229.50	.26	5.00	152.30	230.00	.26
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.9775E+01	EXCESS=	.0000E+00	OUTFLOW=	.9835E+01	BASIN STORAGE=	.6678E-02	PERCENT ERROR=	-.7
FOR PLAN = 1	RATIO=	.00							
RCPI0	MANE	3.00	28.40	261.00	.06	5.00	26.18	260.00	.06
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2130E+01	EXCESS=	.0000E+00	OUTFLOW=	.2158E+01	BASIN STORAGE=	.6480E-02	PERCENT ERROR=	-1.7
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	3.00	139.09	243.00	.60	5.00	138.97	245.00	.60
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1422E+02	EXCESS=	.0000E+00	OUTFLOW=	.1423E+02	BASIN STORAGE=	.6050E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	2.75	111.77	244.75	.49	5.00	111.63	245.00	.49
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1159E+02	EXCESS=	.0000E+00	OUTFLOW=	.1160E+02	BASIN STORAGE=	.6812E-02	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	2.75	94.21	244.75	.42	5.00	94.14	245.00	.42
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.9904E+01	EXCESS=	.0000E+00	OUTFLOW=	.9917E+01	BASIN STORAGE=	.6022E-02	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	2.50	84.60	245.00	.38	5.00	84.60	245.00	.38
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.8969E+01	EXCESS=	.0000E+00	OUTFLOW=	.8981E+01	BASIN STORAGE=	.5735E-02	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	2.50	71.64	250.00	.33	5.00	71.64	250.00	.33
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.7720E+01	EXCESS=	.0000E+00	OUTFLOW=	.7732E+01	BASIN STORAGE=	.6425E-02	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	2.50	59.45	247.50	.28	5.00	59.18	250.00	.28
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.6513E+01	EXCESS=	.0000E+00	OUTFLOW=	.6523E+01	BASIN STORAGE=	.5914E-02	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	2.25	21.78	256.50	.12	5.00	21.00	260.00	.12
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2852E+01	EXCESS=	.0000E+00	OUTFLOW=	.2860E+01	BASIN STORAGE=	.5542E-02	PERCENT ERROR=	-.5
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	3.75	7.14	322.50	.04	5.00	7.12	325.00	.04
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.9147E+00	EXCESS=	.0000E+00	OUTFLOW=	.9201E+00	BASIN STORAGE=	.5835E-02	PERCENT ERROR=	-1.2
FOR PLAN = 1	RATIO=	.00							
RC5GD	MANE	5.00	.00	.00	.00	5.00	.00	325.00	.00
FOR PLAN = 1	RATIO=	.00							
RCPI1	MANE	2.32	787.98	227.36	1.07	5.00	779.56	225.00	1.07
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.7487E+02	EXCESS=	.0000E+00	OUTFLOW=	.7488E+02	BASIN STORAGE=	.4001E-02	PERCENT ERROR=	.0
FOR PLAN = 1	RATIO=	.00							
RCPI1	MANE	2.45	684.25	227.79	.92	5.00	671.05	225.00	.92
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.6449E+02	EXCESS=	.0000E+00	OUTFLOW=	.6450E+02	BASIN STORAGE=	.4568E-02	PERCENT ERROR=	.0
FOR PLAN = 1	RATIO=	.00							
RCPI1	MANE	2.57	603.01	226.20	.82	5.00	591.45	225.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5751E+02	EXCESS=	.0000E+00	OUTFLOW=	.5752E+02	BASIN STORAGE=	.4382E-02	PERCENT ERROR=	.0
FOR PLAN = 1	RATIO=	.00							
RCPI1	MANE	2.65	557.64	228.26	.77	5.00	552.32	225.00	.77
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5378E+02	EXCESS=	.0000E+00	OUTFLOW=	.5379E+02	BASIN STORAGE=	.4400E-02	PERCENT ERROR=	.0
FOR PLAN = 1	RATIO=	.00							
RCPI1	MANE	2.78	502.25	227.74	.69	5.00	495.18	225.00	.69
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.4831E+02	EXCESS=	.0000E+00	OUTFLOW=	.4832E+02	BASIN STORAGE=	.4483E-02	PERCENT ERROR=	.0
FOR PLAN = 1	RATIO=	.00							
RCPI1	MANE	2.90	448.57	226.00	.62	5.00	440.91	230.00	.62
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.4321E+02	EXCESS=	.0000E+00	OUTFLOW=	.4322E+02	BASIN STORAGE=	.4463E-02	PERCENT ERROR=	.0
FOR PLAN = 1	RATIO=	.00							
RCPI1	MANE	3.37	304.27	229.44	.36	5.00	299.08	230.00	.36
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2507E+02	EXCESS=	.0000E+00	OUTFLOW=	.2509E+02	BASIN STORAGE=	.3912E-02	PERCENT ERROR=	-.1

SDN3.OUT

FOR PLAN = 1	RATIO=	.00							
RCP11	MANE	4.25	166.65	238.00	.19	5.00	151.37	235.00	.19
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1306E+02 EXCESS= .0000E+00 OUTFLOW= .1309E+02 BASIN STORAGE= .3772E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP11	MANE	1.75	38.71	269.50	.04	5.00	32.68	270.00	.04
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2522E+01 EXCESS= .0000E+00 OUTFLOW= .2539E+01 BASIN STORAGE= .4601E-02 PERCENT ERROR= -.9									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	4.66	848.47	228.38	1.09	5.00	846.81	230.00	1.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8195E+02 EXCESS= .0000E+00 OUTFLOW= .8201E+02 BASIN STORAGE= .8791E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	4.95	737.24	232.49	.94	5.00	727.63	230.00	.94
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7073E+02 EXCESS= .0000E+00 OUTFLOW= .7078E+02 BASIN STORAGE= .8159E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	5.00	660.28	230.00	.83	5.00	660.28	230.00	.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6303E+02 EXCESS= .0000E+00 OUTFLOW= .6308E+02 BASIN STORAGE= .9913E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	5.00	615.88	230.00	.78	5.00	615.88	230.00	.78
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5898E+02 EXCESS= .0000E+00 OUTFLOW= .5904E+02 BASIN STORAGE= .7857E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	5.00	555.93	230.00	.70	5.00	555.93	230.00	.70
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5308E+02 EXCESS= .0000E+00 OUTFLOW= .5313E+02 BASIN STORAGE= .9825E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	5.00	498.79	235.00	.63	5.00	498.79	235.00	.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4741E+02 EXCESS= .0000E+00 OUTFLOW= .4745E+02 BASIN STORAGE= .8380E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	5.00	320.49	240.00	.37	5.00	320.49	240.00	.37
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2763E+02 EXCESS= .0000E+00 OUTFLOW= .2767E+02 BASIN STORAGE= .7970E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	5.00	175.22	245.00	.19	5.00	175.22	245.00	.19
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1433E+02 EXCESS= .0000E+00 OUTFLOW= .1438E+02 BASIN STORAGE= .1010E-01 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RCP12	MANE	2.50	42.53	290.00	.04	5.00	42.53	290.00	.04
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2798E+01 EXCESS= .0000E+00 OUTFLOW= .2826E+01 BASIN STORAGE= .7781E-02 PERCENT ERROR= -1.3									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	2.49	467.03	213.80	.91	5.00	447.42	215.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2526E+02 EXCESS= .0000E+00 OUTFLOW= .2528E+02 BASIN STORAGE= .3981E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	2.50	401.05	212.50	.77	5.00	387.15	215.00	.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2132E+02 EXCESS= .0000E+00 OUTFLOW= .2134E+02 BASIN STORAGE= .3876E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	1.75	350.58	213.50	.68	5.00	332.97	215.00	.68
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1876E+02 EXCESS= .0000E+00 OUTFLOW= .1877E+02 BASIN STORAGE= .3804E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	1.50	321.30	213.00	.63	5.00	306.62	215.00	.62
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1730E+02 EXCESS= .0000E+00 OUTFLOW= .1731E+02 BASIN STORAGE= .3330E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	1.50	281.58	213.00	.55	5.00	271.57	215.00	.55
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1534E+02 EXCESS= .0000E+00 OUTFLOW= .1535E+02 BASIN STORAGE= .4397E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	1.25	243.61	213.75	.48	5.00	234.87	215.00	.48
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1340E+02 EXCESS= .0000E+00 OUTFLOW= .1341E+02 BASIN STORAGE= .4321E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	1.00	110.25	215.00	.25	5.00	110.25	215.00	.25
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6859E+01 EXCESS= .0000E+00 OUTFLOW= .6867E+01 BASIN STORAGE= .3292E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RC5I1B	MANE	.75	36.14	221.25	.10	5.00	32.24	225.00	.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2775E+01 EXCESS= .0000E+00 OUTFLOW= .2785E+01 BASIN STORAGE= .4086E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCP13 MANE 1.25 1.22 321.25 .00 5.00 1.20 325.00 .00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3730E-01 EXCESS= .0000E+00 OUTFLOW= .3940E-01 BASIN STORAGE= .3297E-02 PERCENT ERROR= -14.5

FOR PLAN = 1 RATIO= .00
RCP13 MANE 4.22 564.82 219.24 .98 5.00 547.85 220.00 .98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3313E+02 EXCESS= .0000E+00 OUTFLOW= .3318E+02 BASIN STORAGE= .6895E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP13 MANE 4.47 488.01 218.91 .83 5.00 470.11 220.00 .83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2809E+02 EXCESS= .0000E+00 OUTFLOW= .2816E+02 BASIN STORAGE= .8933E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP13 MANE 3.75 419.86 217.50 .73 5.00 403.66 220.00 .73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2468E+02 EXCESS= .0000E+00 OUTFLOW= .2474E+02 BASIN STORAGE= .7920E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP13 MANE 3.50 378.33 220.50 .68 5.00 377.85 220.00 .68

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2284E+02 EXCESS= .0000E+00 OUTFLOW= .2289E+02 BASIN STORAGE= .7026E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP13 MANE 3.75 334.03 221.25 .60 5.00 333.75 220.00 .60

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2032E+02 EXCESS= .0000E+00 OUTFLOW= .2037E+02 BASIN STORAGE= .7890E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP13 MANE 3.50 298.15 220.50 .53 5.00 295.29 220.00 .53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1789E+02 EXCESS= .0000E+00 OUTFLOW= .1795E+02 BASIN STORAGE= .6126E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP13 MANE 1.75 155.46 222.25 .28 5.00 139.07 225.00 .28

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9534E+01 EXCESS= .0000E+00 OUTFLOW= .9559E+01 BASIN STORAGE= .6892E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP13 MANE 1.50 57.29 231.00 .12 5.00 50.58 230.00 .12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4060E+01 EXCESS= .0000E+00 OUTFLOW= .4071E+01 BASIN STORAGE= .7316E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCP13 MANE 2.25 1.90 276.75 .01 5.00 1.65 315.00 .01

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2118E+00 EXCESS= .0000E+00 OUTFLOW= .2162E+00 BASIN STORAGE= .6301E-02 PERCENT ERROR= -5.1

FOR PLAN = 1 RATIO= .00
RCP14 MANE 1.53 1139.67 222.86 .94 5.00 1135.03 225.00 .94

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1100E+03 EXCESS= .0000E+00 OUTFLOW= .1100E+03 BASIN STORAGE= .3264E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP14 MANE 1.60 1007.49 227.06 .81 5.00 999.42 225.00 .81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9509E+02 EXCESS= .0000E+00 OUTFLOW= .9509E+02 BASIN STORAGE= .2963E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP14 MANE 1.67 900.57 227.57 .72 5.00 888.60 230.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8440E+02 EXCESS= .0000E+00 OUTFLOW= .8441E+02 BASIN STORAGE= .2904E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP14 MANE 1.72 837.93 227.50 .67 5.00 828.24 230.00 .67

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7864E+02 EXCESS= .0000E+00 OUTFLOW= .7865E+02 BASIN STORAGE= .2923E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP14 MANE 1.80 742.62 230.90 .60 5.00 741.63 230.00 .60

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7051E+02 EXCESS= .0000E+00 OUTFLOW= .7052E+02 BASIN STORAGE= .2847E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP14 MANE 1.89 657.78 232.63 .53 5.00 651.79 230.00 .53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6259E+02 EXCESS= .0000E+00 OUTFLOW= .6259E+02 BASIN STORAGE= .2844E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP14 MANE 2.33 392.23 238.00 .30 5.00 382.32 240.00 .30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3541E+02 EXCESS= .0000E+00 OUTFLOW= .3543E+02 BASIN STORAGE= .2980E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP14 MANE 3.10 185.76 247.63 .15 5.00 185.28 250.00 .15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1744E+02 EXCESS= .0000E+00 OUTFLOW= .1745E+02 BASIN STORAGE= .2833E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCPI4	MANE	4.75	35.72	299.25	.02	5.00	31.54	300.00	.02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2763E+01 EXCESS= .0000E+00 OUTFLOW= .2774E+01 BASIN STORAGE= .3044E-02 PERCENT ERROR= -.5

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	3.19	1189.53	226.44	.95	5.00	1175.69	225.00	.95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1145E+03 EXCESS= .0000E+00 OUTFLOW= .1146E+03 BASIN STORAGE= .6520E-02 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	3.36	1046.61	228.24	.82	5.00	1033.39	230.00	.82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9896E+02 EXCESS= .0000E+00 OUTFLOW= .9900E+02 BASIN STORAGE= .7015E-02 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	3.53	925.46	229.42	.73	5.00	923.48	230.00	.73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8782E+02 EXCESS= .0000E+00 OUTFLOW= .8786E+02 BASIN STORAGE= .6553E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	3.63	860.50	228.70	.68	5.00	857.97	230.00	.68

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8188E+02 EXCESS= .0000E+00 OUTFLOW= .8192E+02 BASIN STORAGE= .7062E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	3.79	754.04	231.38	.61	5.00	753.61	235.00	.61

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7338E+02 EXCESS= .0000E+00 OUTFLOW= .7342E+02 BASIN STORAGE= .7883E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	3.99	667.80	235.58	.54	5.00	666.32	235.00	.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6518E+02 EXCESS= .0000E+00 OUTFLOW= .6522E+02 BASIN STORAGE= .6852E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	4.97	384.23	243.63	.30	5.00	370.08	245.00	.30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3685E+02 EXCESS= .0000E+00 OUTFLOW= .3691E+02 BASIN STORAGE= .7985E-02 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	5.00	179.93	255.00	.15	5.00	179.93	255.00	.15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1817E+02 EXCESS= .0000E+00 OUTFLOW= .1820E+02 BASIN STORAGE= .7967E-02 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RCPI5	MANE	3.75	32.42	311.25	.02	5.00	27.61	315.00	.02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2861E+01 EXCESS= .0000E+00 OUTFLOW= .2870E+01 BASIN STORAGE= .6574E-02 PERCENT ERROR= -.6

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	3.73	67.70	223.57	1.45	5.00	66.14	225.00	1.45

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4962E+01 EXCESS= .0000E+00 OUTFLOW= .4965E+01 BASIN STORAGE= .2346E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	3.93	59.20	224.06	1.26	5.00	58.29	225.00	1.27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4335E+01 EXCESS= .0000E+00 OUTFLOW= .4338E+01 BASIN STORAGE= .2329E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	4.09	52.79	225.14	1.14	5.00	52.75	225.00	1.14

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3913E+01 EXCESS= .0000E+00 OUTFLOW= .3915E+01 BASIN STORAGE= .2848E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	4.20	49.46	222.51	1.07	5.00	48.72	225.00	1.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3671E+01 EXCESS= .0000E+00 OUTFLOW= .3674E+01 BASIN STORAGE= .2343E-02 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	4.36	44.72	222.32	.97	5.00	44.40	225.00	.97

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3341E+01 EXCESS= .0000E+00 OUTFLOW= .3343E+01 BASIN STORAGE= .2484E-02 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	4.55	40.45	222.72	.88	5.00	40.04	225.00	.88

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3012E+01 EXCESS= .0000E+00 OUTFLOW= .3015E+01 BASIN STORAGE= .2468E-02 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	3.50	24.45	227.50	.54	5.00	24.34	225.00	.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1836E+01 EXCESS= .0000E+00 OUTFLOW= .1838E+01 BASIN STORAGE= .2806E-02 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC5I1C	MANE	2.00	12.79	228.00	.29	5.00	12.62	230.00	.29

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9953E+00 EXCESS= .0000E+00 OUTFLOW= .9967E+00 BASIN STORAGE= .2220E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00

RCS11C	MANE	1.50	2.11	237.00	.05	5.00	SDN3.OUT 1.74	245.00	.05
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .1820E+00 EXCESS= .0000E+00 OUTFLOW= .1833E+00 BASIN STORAGE= .2256E-02 PERCENT ERROR= -1.9

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		2.51	292.60	218.36	1.25	5.00	291.11	220.00
									1.25

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2044E+02 EXCESS= .0000E+00 OUTFLOW= .2044E+02 BASIN STORAGE= .3237E-02 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		2.66	252.01	220.83	1.08	5.00	251.71	220.00
									1.08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1766E+02 EXCESS= .0000E+00 OUTFLOW= .1767E+02 BASIN STORAGE= .2693E-02 PERCENT ERROR= .0

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		2.78	226.28	219.94	.97	5.00	226.14	220.00
									.97

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1582E+02 EXCESS= .0000E+00 OUTFLOW= .1583E+02 BASIN STORAGE= .3112E-02 PERCENT ERROR= -.1

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		2.86	211.00	220.34	.90	5.00	210.06	220.00
									.90

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1477E+02 EXCESS= .0000E+00 OUTFLOW= .1478E+02 BASIN STORAGE= .3054E-02 PERCENT ERROR= -.1

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		2.98	189.86	220.78	.81	5.00	188.18	220.00
									.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1334E+02 EXCESS= .0000E+00 OUTFLOW= .1334E+02 BASIN STORAGE= .2935E-02 PERCENT ERROR= -.1

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		3.12	167.94	221.85	.73	5.00	166.05	220.00
									.73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1191E+02 EXCESS= .0000E+00 OUTFLOW= .1192E+02 BASIN STORAGE= .3420E-02 PERCENT ERROR= -.1

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		3.75	92.29	221.25	.42	5.00	91.82	225.00
									.42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6901E+01 EXCESS= .0000E+00 OUTFLOW= .6909E+01 BASIN STORAGE= .2942E-02 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		2.25	42.95	227.25	.21	5.00	41.57	230.00
									.21

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3472E+01 EXCESS= .0000E+00 OUTFLOW= .3477E+01 BASIN STORAGE= .2816E-02 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP16	MANE		3.50	4.09	308.00	.03	5.00	3.94	310.00
									.03

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4372E+00 EXCESS= .0000E+00 OUTFLOW= .4386E+00 BASIN STORAGE= .2820E-02 PERCENT ERROR= -1.0

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		4.58	474.02	224.63	1.42	5.00	471.80	220.00
									1.43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3411E+02 EXCESS= .0000E+00 OUTFLOW= .3414E+02 BASIN STORAGE= .7837E-02 PERCENT ERROR= -.1

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		4.83	414.59	222.21	1.24	5.00	401.10	225.00
									1.24

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2972E+02 EXCESS= .0000E+00 OUTFLOW= .2976E+02 BASIN STORAGE= .8453E-02 PERCENT ERROR= -.1

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		5.00	379.74	225.00	1.12	5.00	379.74	225.00
									1.12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2691E+02 EXCESS= .0000E+00 OUTFLOW= .2695E+02 BASIN STORAGE= .8259E-02 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		5.00	356.99	225.00	1.05	5.00	356.99	225.00
									1.05

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2528E+02 EXCESS= .0000E+00 OUTFLOW= .2531E+02 BASIN STORAGE= .8401E-02 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		5.00	325.73	225.00	.96	5.00	325.73	225.00
									.96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2304E+02 EXCESS= .0000E+00 OUTFLOW= .2307E+02 BASIN STORAGE= .8520E-02 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		5.00	293.39	225.00	.87	5.00	293.39	225.00
									.87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2081E+02 EXCESS= .0000E+00 OUTFLOW= .2084E+02 BASIN STORAGE= .6368E-02 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		4.75	168.86	228.00	.53	5.00	167.45	225.00
									.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1279E+02 EXCESS= .0000E+00 OUTFLOW= .1282E+02 BASIN STORAGE= .6948E-02 PERCENT ERROR= -.2

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		4.25	87.06	229.50	.30	5.00	86.77	230.00
									.30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7099E+01 EXCESS= .0000E+00 OUTFLOW= .7110E+01 BASIN STORAGE= .7290E-02 PERCENT ERROR= -.3

FOR PLAN	= 1	RATIO=	.00						
RCP17	MANE		1.50	21.27	231.00	.06	5.00	16.14	235.00
									.06

SDN3.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1514E+01 EXCESS= .0000E+00 OUTFLOW= .1528E+01 BASIN STORAGE= .6939E-02 PERCENT ERROR= -1.4

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 2.35 1107.12 235.38 .78 5.00 1106.01 235.00 .78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1215E+03 EXCESS= .0000E+00 OUTFLOW= .1215E+03 BASIN STORAGE= .4562E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 2.35 1120.15 230.13 .71 5.00 1119.59 230.00 .71

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1092E+03 EXCESS= .0000E+00 OUTFLOW= .1092E+03 BASIN STORAGE= .4288E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 2.41 1046.07 228.60 .63 5.00 1034.52 230.00 .63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9802E+02 EXCESS= .0000E+00 OUTFLOW= .9802E+02 BASIN STORAGE= .4425E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 2.48 971.73 228.15 .59 5.00 965.64 230.00 .59

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9153E+02 EXCESS= .0000E+00 OUTFLOW= .9153E+02 BASIN STORAGE= .4368E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 2.61 857.57 229.73 .53 5.00 855.30 230.00 .53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8260E+02 EXCESS= .0000E+00 OUTFLOW= .8261E+02 BASIN STORAGE= .5212E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 2.76 749.02 229.34 .48 5.00 746.90 230.00 .48

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7362E+02 EXCESS= .0000E+00 OUTFLOW= .7363E+02 BASIN STORAGE= .4616E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 3.58 388.14 243.72 .28 5.00 386.24 240.00 .28

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4267E+02 EXCESS= .0000E+00 OUTFLOW= .4268E+02 BASIN STORAGE= .4836E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 4.92 165.58 260.84 .14 5.00 165.17 260.00 .14

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2184E+02 EXCESS= .0000E+00 OUTFLOW= .2186E+02 BASIN STORAGE= .5003E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCPI8 MANE 3.00 29.99 321.00 .02 5.00 28.17 320.00 .02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3796E+01 EXCESS= .0000E+00 OUTFLOW= .3803E+01 BASIN STORAGE= .4564E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 5.00 257.88 225.00 1.55 5.00 257.88 225.00 1.55

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1853E+02 EXCESS= .0000E+00 OUTFLOW= .1858E+02 BASIN STORAGE= .1215E-01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 5.00 227.05 225.00 1.37 5.00 227.05 225.00 1.37

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1634E+02 EXCESS= .0000E+00 OUTFLOW= .1639E+02 BASIN STORAGE= .1164E-01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 4.75 204.60 228.00 1.25 5.00 197.61 225.00 1.24

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1486E+02 EXCESS= .0000E+00 OUTFLOW= .1490E+02 BASIN STORAGE= .1256E-01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 4.75 193.58 228.00 1.17 5.00 186.66 230.00 1.17

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1402E+02 EXCESS= .0000E+00 OUTFLOW= .1405E+02 BASIN STORAGE= .1230E-01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 5.00 178.41 230.00 1.08 5.00 178.41 230.00 1.08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1287E+02 EXCESS= .0000E+00 OUTFLOW= .1290E+02 BASIN STORAGE= .1074E-01 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 5.00 163.58 230.00 .98 5.00 163.58 230.00 .98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1170E+02 EXCESS= .0000E+00 OUTFLOW= .1174E+02 BASIN STORAGE= .1040E-01 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 4.50 101.68 229.50 .63 5.00 101.68 230.00 .63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7450E+01 EXCESS= .0000E+00 OUTFLOW= .7483E+01 BASIN STORAGE= .9573E-02 PERCENT ERROR= -.6

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 3.00 61.60 237.00 .36 5.00 57.83 230.00 .36

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4303E+01 EXCESS= .0000E+00 OUTFLOW= .4340E+01 BASIN STORAGE= .1164E-01 PERCENT ERROR= -1.1

FOR PLAN = 1 RATIO= .00
RCIGIA MANE 1.50 20.17 249.00 .09 5.00 14.17 250.00 .09

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1033E+01 EXCESS= .0000E+00 OUTFLOW= .1064E+01 BASIN STORAGE= .9827E-02 PERCENT ERROR= -4.0

SDN3.OUT									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	4.48	903.73	228.41	.71	5.00	889.99	230.00	.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1231E+03 EXCESS= .0000E+00 OUTFLOW= .1231E+03 BASIN STORAGE= .8839E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	4.49	883.48	228.90	.64	5.00	880.63	230.00	.64
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1123E+03 EXCESS= .0000E+00 OUTFLOW= .1123E+03 BASIN STORAGE= .1012E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	4.56	845.41	232.42	.59	5.00	843.78	230.00	.59
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1035E+03 EXCESS= .0000E+00 OUTFLOW= .1035E+03 BASIN STORAGE= .7602E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	4.61	836.61	230.47	.56	5.00	832.42	230.00	.57
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9851E+02 EXCESS= .0000E+00 OUTFLOW= .9855E+02 BASIN STORAGE= .7718E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	4.68	831.46	229.39	.52	5.00	823.00	230.00	.52
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9155E+02 EXCESS= .0000E+00 OUTFLOW= .9158E+02 BASIN STORAGE= .8047E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	4.76	761.21	233.13	.48	5.00	758.73	235.00	.48
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8356E+02 EXCESS= .0000E+00 OUTFLOW= .8361E+02 BASIN STORAGE= .7805E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	5.00	454.08	245.00	.29	5.00	454.08	245.00	.29
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5062E+02 EXCESS= .0000E+00 OUTFLOW= .5067E+02 BASIN STORAGE= .8731E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	5.00	186.94	260.00	.15	5.00	186.94	260.00	.15
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2667E+02 EXCESS= .0000E+00 OUTFLOW= .2670E+02 BASIN STORAGE= .8611E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP19	MANE	2.25	33.32	265.50	.03	5.00	31.91	335.00	.03
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5178E+01 EXCESS= .0000E+00 OUTFLOW= .5199E+01 BASIN STORAGE= .7715E-02 PERCENT ERROR= -.6									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	.96	1497.61	259.80	.93	5.00	1497.56	260.00	.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7413E+03 EXCESS= .0000E+00 OUTFLOW= .7406E+03 BASIN STORAGE= .7647E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	1.00	1349.94	250.79	.86	5.00	1349.29	250.00	.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6839E+03 EXCESS= .0000E+00 OUTFLOW= .6833E+03 BASIN STORAGE= .7290E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	1.02	1247.72	246.79	.80	5.00	1245.21	250.00	.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6421E+03 EXCESS= .0000E+00 OUTFLOW= .6415E+03 BASIN STORAGE= .6984E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	1.04	1192.68	246.60	.77	5.00	1187.49	250.00	.78
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6180E+03 EXCESS= .0000E+00 OUTFLOW= .6174E+03 BASIN STORAGE= .6803E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	1.07	1108.27	246.64	.73	5.00	1106.02	245.00	.73
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5837E+03 EXCESS= .0000E+00 OUTFLOW= .5832E+03 BASIN STORAGE= .6551E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	1.10	1023.51	246.12	.69	5.00	1020.33	245.00	.69
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5464E+03 EXCESS= .0000E+00 OUTFLOW= .5459E+03 BASIN STORAGE= .6231E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	1.33	599.61	246.24	.49	5.00	589.71	245.00	.49
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3915E+03 EXCESS= .0000E+00 OUTFLOW= .3911E+03 BASIN STORAGE= .3943E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	1.68	314.06	315.67	.29	5.00	313.60	315.00	.29
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2286E+03 EXCESS= .0000E+00 OUTFLOW= .2286E+03 BASIN STORAGE= .2926E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP20	MANE	2.49	104.74	411.13	.06	5.00	104.70	410.00	.06
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5165E+02 EXCESS= .0000E+00 OUTFLOW= .5165E+02 BASIN STORAGE= .1532E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC1D	MANE	5.00	341.08	225.00	1.12	5.00	341.08	225.00	1.12

SDN3.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2385E+02 EXCESS= .0000E+00 OUTFLOW= .2386E+02 BASIN STORAGE= .1200E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC1D MANE 4.25 288.69 225.25 .96 5.00 287.86 225.00 .96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2057E+02 EXCESS= .0000E+00 OUTFLOW= .2058E+02 BASIN STORAGE= .1210E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RC1D MANE 4.25 258.22 225.25 .86 5.00 257.33 225.00 .86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1840E+02 EXCESS= .0000E+00 OUTFLOW= .1840E+02 BASIN STORAGE= .1834E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RC1D MANE 4.25 240.71 225.25 .80 5.00 239.79 225.00 .81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1716E+02 EXCESS= .0000E+00 OUTFLOW= .1717E+02 BASIN STORAGE= .1774E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC1D MANE 4.25 216.68 225.25 .73 5.00 215.72 225.00 .73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1548E+02 EXCESS= .0000E+00 OUTFLOW= .1549E+02 BASIN STORAGE= .1688E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC1D MANE 4.00 192.56 224.00 .65 5.00 192.02 225.00 .65

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1382E+02 EXCESS= .0000E+00 OUTFLOW= .1383E+02 BASIN STORAGE= .1700E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC1D MANE 2.00 106.51 228.00 .37 5.00 104.48 230.00 .37

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7930E+01 EXCESS= .0000E+00 OUTFLOW= .7934E+01 BASIN STORAGE= .1416E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC1D MANE 1.75 48.17 231.00 .18 5.00 47.69 230.00 .18

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3923E+01 EXCESS= .0000E+00 OUTFLOW= .3926E+01 BASIN STORAGE= .1180E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC1D MANE 3.00 4.46 309.00 .02 5.00 4.46 310.00 .02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4424E+00 EXCESS= .0000E+00 OUTFLOW= .4434E+00 BASIN STORAGE= .1273E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCP21 MANE 5.00 541.43 230.00 1.15 5.00 541.43 230.00 1.15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3857E+02 EXCESS= .0000E+00 OUTFLOW= .3860E+02 BASIN STORAGE= .2422E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP21 MANE 5.00 459.25 230.00 .99 5.00 459.25 230.00 .99

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3337E+02 EXCESS= .0000E+00 OUTFLOW= .3339E+02 BASIN STORAGE= .3021E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP21 MANE 5.00 411.94 230.00 .89 5.00 411.94 230.00 .89

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2990E+02 EXCESS= .0000E+00 OUTFLOW= .2993E+02 BASIN STORAGE= .2000E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP21 MANE 5.00 383.76 230.00 .83 5.00 383.76 230.00 .83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2793E+02 EXCESS= .0000E+00 OUTFLOW= .2796E+02 BASIN STORAGE= .3052E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP21 MANE 5.00 344.70 230.00 .75 5.00 344.70 230.00 .75

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2525E+02 EXCESS= .0000E+00 OUTFLOW= .2527E+02 BASIN STORAGE= .2886E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP21 MANE 4.75 300.96 232.75 .67 5.00 293.77 230.00 .67

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2255E+02 EXCESS= .0000E+00 OUTFLOW= .2257E+02 BASIN STORAGE= .2145E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP21 MANE 2.50 169.35 235.00 .39 5.00 169.35 235.00 .39

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1310E+02 EXCESS= .0000E+00 OUTFLOW= .1311E+02 BASIN STORAGE= .2022E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP21 MANE 2.25 76.97 238.50 .20 5.00 76.69 240.00 .20

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6614E+01 EXCESS= .0000E+00 OUTFLOW= .6622E+01 BASIN STORAGE= .2015E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP21 MANE 3.25 7.52 318.50 .03 5.00 7.50 320.00 .02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8408E+00 EXCESS= .0000E+00 OUTFLOW= .8434E+00 BASIN STORAGE= .2172E-02 PERCENT ERROR= -.6

FOR PLAN = 1 RATIO= .00
RC41D MANE 1.45 52.58 217.24 1.10 5.00 52.35 220.00 1.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3626E+01 EXCESS= .0000E+00 OUTFLOW= .3626E+01 BASIN STORAGE= .5432E-03 PERCENT ERROR= .0

SDN3.OUT

FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	1.53	45.33	218.27	.95	5.00	44.96	220.00	.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3126E+01 EXCESS= .0000E+00 OUTFLOW= .3126E+01 BASIN STORAGE= .5549E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	1.59	40.35	220.82	.85	5.00	40.27	220.00	.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2794E+01 EXCESS= .0000E+00 OUTFLOW= .2795E+01 BASIN STORAGE= .5830E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	1.63	37.74	221.54	.79	5.00	37.32	220.00	.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2607E+01 EXCESS= .0000E+00 OUTFLOW= .2608E+01 BASIN STORAGE= .5308E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	1.69	33.95	221.53	.71	5.00	33.63	220.00	.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2350E+01 EXCESS= .0000E+00 OUTFLOW= .2351E+01 BASIN STORAGE= .5857E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	1.76	30.03	218.66	.63	5.00	29.86	220.00	.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2096E+01 EXCESS= .0000E+00 OUTFLOW= .2096E+01 BASIN STORAGE= .5603E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	2.00	16.72	222.00	.36	5.00	16.43	220.00	.36
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1199E+01 EXCESS= .0000E+00 OUTFLOW= .1199E+01 BASIN STORAGE= .6021E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	1.25	7.48	222.50	.18	5.00	7.36	225.00	.18
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5901E+00 EXCESS= .0000E+00 OUTFLOW= .5902E+00 BASIN STORAGE= .5261E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC4A1D	MANE	3.25	.68	302.25	.02	5.00	.67	300.00	.02
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6447E-01 EXCESS= .0000E+00 OUTFLOW= .6456E-01 BASIN STORAGE= .6137E-03 PERCENT ERROR= -1.1									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	1.68	2295.24	226.55	.95	5.00	2284.65	225.00	.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8154E+03 EXCESS= .0000E+00 OUTFLOW= .8142E+03 BASIN STORAGE= .1561E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	1.74	2068.01	228.10	.88	5.00	2054.87	230.00	.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7487E+03 EXCESS= .0000E+00 OUTFLOW= .7475E+03 BASIN STORAGE= .1488E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	1.80	1888.47	228.61	.82	5.00	1883.02	230.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7008E+03 EXCESS= .0000E+00 OUTFLOW= .6997E+03 BASIN STORAGE= .1426E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	1.83	1790.11	230.59	.79	5.00	1789.29	230.00	.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6729E+03 EXCESS= .0000E+00 OUTFLOW= .6719E+03 BASIN STORAGE= .1389E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	1.87	1681.44	232.16	.74	5.00	1666.31	230.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6338E+03 EXCESS= .0000E+00 OUTFLOW= .6328E+03 BASIN STORAGE= .1338E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	1.95	1498.44	232.55	.69	5.00	1477.59	235.00	.69
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5919E+03 EXCESS= .0000E+00 OUTFLOW= .5909E+03 BASIN STORAGE= .1273E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	2.45	800.93	244.78	.49	5.00	800.65	245.00	.49
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4191E+03 EXCESS= .0000E+00 OUTFLOW= .4185E+03 BASIN STORAGE= .8138E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	3.22	375.87	305.46	.29	5.00	375.50	305.00	.29
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2440E+03 EXCESS= .0000E+00 OUTFLOW= .2440E+03 BASIN STORAGE= .6359E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP22	MANE	5.00	106.89	345.00	.06	5.00	106.89	345.00	.06
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5477E+02 EXCESS= .0000E+00 OUTFLOW= .5477E+02 BASIN STORAGE= .3152E-01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP23	MANE	.84	2415.53	226.19	.96	5.00	2409.55	225.00	.96
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8252E+03 EXCESS= .0000E+00 OUTFLOW= .8246E+03 BASIN STORAGE= .8003E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP23	MANE	.88	2165.60	226.58	.88	5.00	2154.93	230.00	.88

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7571E+03 EXCESS= .0000E+00 OUTFLOW= .7565E+03 BASIN STORAGE= .7629E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP23 MANE .91 1970.33 230.65 .82 5.00 1969.18 230.00 .82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7084E+03 EXCESS= .0000E+00 OUTFLOW= .7078E+03 BASIN STORAGE= .7311E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP23 MANE .92 1868.66 230.31 .79 5.00 1865.84 230.00 .79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6802E+03 EXCESS= .0000E+00 OUTFLOW= .6796E+03 BASIN STORAGE= .7122E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP23 MANE .95 1738.74 230.62 .74 5.00 1729.44 230.00 .74

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6402E+03 EXCESS= .0000E+00 OUTFLOW= .6397E+03 BASIN STORAGE= .6859E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP23 MANE .99 1536.29 231.56 .69 5.00 1533.51 235.00 .69

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5974E+03 EXCESS= .0000E+00 OUTFLOW= .5969E+03 BASIN STORAGE= .6527E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP23 MANE 1.24 827.87 241.83 .49 5.00 825.29 240.00 .49

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4228E+03 EXCESS= .0000E+00 OUTFLOW= .4225E+03 BASIN STORAGE= .4196E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP23 MANE 1.63 383.52 307.21 .29 5.00 382.94 305.00 .29

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2464E+03 EXCESS= .0000E+00 OUTFLOW= .2463E+03 BASIN STORAGE= .3380E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP23 MANE 2.58 107.04 369.48 .06 5.00 106.99 370.00 .06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5530E+02 EXCESS= .0000E+00 OUTFLOW= .5530E+02 BASIN STORAGE= .1630E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 2.32 427.71 227.47 -1.00 5.00 415.98 225.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 3.20 170.71 227.10 -1.00 5.00 169.75 230.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 4.08 104.11 228.25 -1.00 5.00 102.74 230.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 4.20 95.86 230.82 -1.00 5.00 95.28 230.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 4.41 87.07 229.36 -1.00 5.00 86.43 230.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 4.66 73.57 228.37 -1.00 5.00 73.40 230.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 5.00 38.87 240.00 -1.00 5.00 38.87 240.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 5.00 17.18 255.00 -1.00 5.00 17.18 255.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 3.00 3.02 327.00 -1.00 5.00 2.73 330.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 3.24 408.25 229.86 -1.00 5.00 406.10 230.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 4.57 160.60 233.12 -1.00 5.00 149.48 235.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 5.00 103.57 235.00 -1.00 5.00 103.57 235.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 5.00 96.01 235.00 -1.00 5.00 96.01 235.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 5.00 87.93 235.00 -1.00 5.00 87.93 235.00 -1.00

FOR PLAN = 1 RATIO= .00
RDIV4 MANE 5.00 73.87 235.00 -1.00 5.00 73.87 235.00 -1.00

SDN3.OUT									
FOR PLAN = 1 RDIV4 MANE	RATIO=	.00	40.33	245.00	-1.00	5.00	40.33	245.00	-1.00
		5.00							
FOR PLAN = 1 RDIV4 MANE	RATIO=	.00	18.07	265.00	-1.00	5.00	18.07	265.00	-1.00
		5.00							
FOR PLAN = 1 RDIV4 MANE	RATIO=	.00	2.93	348.50	-1.00	5.00	2.71	350.00	-1.00
		4.25							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	222.44	230.00	-1.00	5.00	222.44	230.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	191.85	235.00	-1.00	5.00	191.85	235.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	169.48	240.00	-1.00	5.00	169.48	240.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	158.52	230.00	-1.00	5.00	158.52	230.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	138.13	240.00	-1.00	5.00	138.13	240.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	123.82	235.00	-1.00	5.00	123.82	235.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	69.25	245.00	-1.00	5.00	69.25	245.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	35.84	260.00	-1.00	5.00	35.84	260.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	7.10	340.00	-1.00	5.00	7.10	340.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	221.08	234.56	-1.00	5.00	220.20	235.00	-1.00
		2.67							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	191.64	237.01	-1.00	5.00	189.21	235.00	-1.00
		2.82							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	169.33	236.75	-1.00	5.00	167.47	235.00	-1.00
		2.96							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	157.77	242.93	-1.00	5.00	157.66	235.00	-1.00
		3.04							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	140.10	236.94	-1.00	5.00	138.71	235.00	-1.00
		3.20							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	122.83	237.10	-1.00	5.00	119.48	245.00	-1.00
		3.34							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	71.19	246.41	-1.00	5.00	65.75	250.00	-1.00
		4.18							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	35.50	265.00	-1.00	5.00	35.50	265.00	-1.00
		5.00							
FOR PLAN = 1 RDIV3 MANE	RATIO=	.00	6.15	350.00	-1.00	5.00	6.15	350.00	-1.00
		5.00							
FOR PLAN = 1 RDIV2 MANE	RATIO=	.00	185.13	230.00	-1.00	5.00	185.13	230.00	-1.00
		5.00							
FOR PLAN = 1 RDIV2 MANE	RATIO=	.00	103.88	230.00	-1.00	5.00	103.88	230.00	-1.00
		5.00							
FOR PLAN = 1 RDIV2 MANE	RATIO=	.00	92.99	230.00	-1.00	5.00	92.99	230.00	-1.00
		5.00							
FOR PLAN = 1 RDIV2 MANE	RATIO=	.00	88.77	230.00	-1.00	5.00	88.77	230.00	-1.00
		5.00							
FOR PLAN = 1 RDIV2 MANE	RATIO=	.00	79.31	230.00	-1.00	5.00	79.31	230.00	-1.00
		5.00							

SDN3.OUT									
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	5.00	67.81	235.00	-1.00	5.00	67.81	235.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	5.00	40.43	240.00	-1.00	5.00	40.43	240.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	5.00	19.68	270.00	-1.00	5.00	19.68	270.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	4.75	3.81	332.50	-1.00	5.00	2.80	330.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	1.56	179.96	230.93	-1.00	5.00	172.82	230.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	1.95	103.33	233.87	-1.00	5.00	101.87	235.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	2.03	92.53	233.88	-1.00	5.00	90.26	235.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	2.07	87.24	231.89	-1.00	5.00	84.22	235.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	2.16	77.72	233.52	-1.00	5.00	74.29	240.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	2.30	66.76	234.24	-1.00	5.00	66.59	235.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	2.80	41.60	243.78	-1.00	5.00	38.69	245.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	3.70	18.77	262.48	-1.00	5.00	17.58	270.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV2	MANE	5.00	3.50	340.00	-1.00	5.00	3.50	340.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	3.25	182.79	224.25	.85	5.00	181.78	225.00	.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1350E+02 EXCESS= .0000E+00 OUTFLOW= .1350E+02 BASIN STORAGE= .1022E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	2.25	151.96	225.00	.71	5.00	151.96	225.00	.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1134E+02 EXCESS= .0000E+00 OUTFLOW= .1134E+02 BASIN STORAGE= .9292E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	2.00	132.73	226.00	.63	5.00	131.50	225.00	.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9924E+01 EXCESS= .0000E+00 OUTFLOW= .9926E+01 BASIN STORAGE= .9986E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	2.00	121.28	226.00	.58	5.00	119.86	225.00	.58
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9129E+01 EXCESS= .0000E+00 OUTFLOW= .9132E+01 BASIN STORAGE= .9420E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	1.75	105.00	227.50	.51	5.00	103.80	225.00	.51
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8059E+01 EXCESS= .0000E+00 OUTFLOW= .8061E+01 BASIN STORAGE= .9204E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	1.75	90.18	227.50	.44	5.00	88.26	225.00	.44
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7011E+01 EXCESS= .0000E+00 OUTFLOW= .7014E+01 BASIN STORAGE= .8323E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	1.50	40.01	232.50	.22	5.00	39.81	230.00	.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3485E+01 EXCESS= .0000E+00 OUTFLOW= .3487E+01 BASIN STORAGE= .8342E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	1.50	11.80	238.50	.08	5.00	11.70	240.00	.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1331E+01 EXCESS= .0000E+00 OUTFLOW= .1332E+01 BASIN STORAGE= .9216E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC5CA	MANE	1.50	.05	346.50	.00	5.00	.03	385.00	.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3189E-02 EXCESS= .0000E+00 OUTFLOW= .3521E-02 BASIN STORAGE= .8075E-03 PERCENT ERROR= -35.7									

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FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	3.25	305.65	214.50	.76	5.00	305.65	215.00	.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2506E+02 EXCESS= .0000E+00 OUTFLOW= .2509E+02 BASIN STORAGE= .4370E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	2.75	251.06	222.75	.63	5.00	246.95	225.00	.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2092E+02 EXCESS= .0000E+00 OUTFLOW= .2094E+02 BASIN STORAGE= .4627E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	2.25	215.55	227.25	.55	5.00	215.48	225.00	.55
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1821E+02 EXCESS= .0000E+00 OUTFLOW= .1822E+02 BASIN STORAGE= .4203E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	2.25	197.07	227.25	.50	5.00	195.90	225.00	.50
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1668E+02 EXCESS= .0000E+00 OUTFLOW= .1670E+02 BASIN STORAGE= .4058E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	2.25	171.59	227.25	.44	5.00	169.13	225.00	.44
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1465E+02 EXCESS= .0000E+00 OUTFLOW= .1466E+02 BASIN STORAGE= .3978E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	2.25	146.44	227.25	.38	5.00	143.57	230.00	.38
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1265E+02 EXCESS= .0000E+00 OUTFLOW= .1267E+02 BASIN STORAGE= .4831E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	1.25	64.11	230.00	.18	5.00	64.11	230.00	.18
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6026E+01 EXCESS= .0000E+00 OUTFLOW= .6037E+01 BASIN STORAGE= .4628E-02 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	2.50	18.34	300.00	.06	5.00	18.34	300.00	.07
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2136E+01 EXCESS= .0000E+00 OUTFLOW= .2142E+01 BASIN STORAGE= .4648E-02 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO=	.00							
RCP25	MANE	4.00	.04	516.00	.00	5.00	.04	500.00	.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3322E-02 EXCESS= .0000E+00 OUTFLOW= .4370E-02 BASIN STORAGE= .4129E-02 PERCENT ERROR=-155.9									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	1.43	500.01	216.84	.74	5.00	487.39	215.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3710E+02 EXCESS= .0000E+00 OUTFLOW= .3710E+02 BASIN STORAGE= .1951E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	1.56	406.13	216.39	.61	5.00	385.03	215.00	.61
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3087E+02 EXCESS= .0000E+00 OUTFLOW= .3088E+02 BASIN STORAGE= .2227E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	1.67	343.33	216.88	.53	5.00	321.34	220.00	.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2678E+02 EXCESS= .0000E+00 OUTFLOW= .2678E+02 BASIN STORAGE= .2333E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	1.74	303.08	218.08	.49	5.00	289.84	220.00	.49
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2453E+02 EXCESS= .0000E+00 OUTFLOW= .2454E+02 BASIN STORAGE= .2340E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	1.75	258.20	217.00	.43	5.00	247.94	220.00	.43
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2152E+02 EXCESS= .0000E+00 OUTFLOW= .2152E+02 BASIN STORAGE= .2381E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	1.75	210.18	218.75	.37	5.00	205.67	225.00	.37
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1853E+02 EXCESS= .0000E+00 OUTFLOW= .1854E+02 BASIN STORAGE= .2019E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	1.50	83.81	232.50	.17	5.00	83.07	230.00	.17
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8636E+01 EXCESS= .0000E+00 OUTFLOW= .8641E+01 BASIN STORAGE= .2066E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	2.75	23.48	297.00	.06	5.00	23.33	300.00	.06
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3007E+01 EXCESS= .0000E+00 OUTFLOW= .3009E+01 BASIN STORAGE= .2365E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP26	MANE	5.00	.03	575.00	.00	5.00	.03	575.00	.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4370E-02 EXCESS= .0000E+00 OUTFLOW= .4966E-02 BASIN STORAGE= .1904E-02 PERCENT ERROR= -57.2									
FOR PLAN = 1	RATIO=	.00							
RDIV1	MANE	3.00	24.86	246.00	-1.00	5.00	23.06	245.00	-1.00

SDN3.OUT

FOR PLAN = 1 RDIV1 MANE	RATIO= 2.75	.00	23.55	247.50	-1.00	5.00	20.62	255.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 2.75	.00	21.24	242.00	-1.00	5.00	19.52	255.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 2.50	.00	20.76	242.50	-1.00	5.00	20.10	250.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 2.50	.00	20.02	245.00	-1.00	5.00	20.02	245.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 2.50	.00	17.33	247.50	-1.00	5.00	16.55	260.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 2.25	.00	9.98	265.50	-1.00	5.00	9.11	260.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.75	.00	2.90	292.50	-1.00	5.00	2.77	345.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 5.00	.00	.00	.00	-1.00	5.00	.00	345.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.25	.00	22.63	250.25	-1.00	5.00	22.54	250.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.25	.00	20.84	260.00	-1.00	5.00	20.84	260.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.50	.00	20.71	255.50	-1.00	5.00	19.97	255.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.00	.00	20.36	255.00	-1.00	5.00	20.36	255.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 2.75	.00	23.71	250.25	-1.00	5.00	22.61	250.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.25	.00	16.45	260.00	-1.00	5.00	16.45	260.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.25	.00	11.64	266.50	-1.00	5.00	7.99	265.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 5.00	.00	3.08	350.00	-1.00	5.00	3.08	350.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 5.00	.00	.00	.00	-1.00	5.00	.00	350.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.75	.00	25.51	255.00	-1.00	5.00	25.51	255.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.75	.00	22.52	258.75	-1.00	5.00	21.06	270.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 4.00	.00	23.03	260.00	-1.00	5.00	23.03	260.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.50	.00	22.21	262.50	-1.00	5.00	19.27	265.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.25	.00	22.73	260.00	-1.00	5.00	22.73	260.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.50	.00	18.89	273.00	-1.00	5.00	16.52	275.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 3.50	.00	10.81	283.50	-1.00	5.00	8.22	280.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 5.00	.00	3.23	360.00	-1.00	5.00	3.23	360.00	-1.00
FOR PLAN = 1 RDIV1 MANE	RATIO= 5.00	.00	.00	.00	-1.00	5.00	.00	360.00	-1.00

FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	2.18	591.10	218.30	.83	5.00	587.78	220.00	.83	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5382E+02 EXCESS= .0000E+00 OUTFLOW= .5384E+02 BASIN STORAGE= .3646E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	2.36	486.31	224.50	.70	5.00	483.50	225.00	.70	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4521E+02 EXCESS= .0000E+00 OUTFLOW= .4522E+02 BASIN STORAGE= .3153E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	2.50	422.11	225.15	.61	5.00	421.39	225.00	.61	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3953E+02 EXCESS= .0000E+00 OUTFLOW= .3955E+02 BASIN STORAGE= .3099E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	2.59	383.29	225.74	.56	5.00	380.30	225.00	.56	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3631E+02 EXCESS= .0000E+00 OUTFLOW= .3633E+02 BASIN STORAGE= .3350E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	2.50	332.11	225.00	.50	5.00	332.11	225.00	.50	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3218E+02 EXCESS= .0000E+00 OUTFLOW= .3220E+02 BASIN STORAGE= .3754E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	2.50	279.92	230.00	.43	5.00	279.92	230.00	.43	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2790E+02 EXCESS= .0000E+00 OUTFLOW= .2792E+02 BASIN STORAGE= .3714E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	2.00	121.76	234.00	.21	5.00	121.14	235.00	.21	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1357E+02 EXCESS= .0000E+00 OUTFLOW= .1358E+02 BASIN STORAGE= .3256E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	3.00	34.46	249.00	.08	5.00	34.02	250.00	.08	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5010E+01 EXCESS= .0000E+00 OUTFLOW= .5015E+01 BASIN STORAGE= .3120E-02 PERCENT ERROR= -.2										
FOR PLAN = 1	RATIO=	.00								
RCP27	MANE	3.00	.91	333.00	.00	5.00	.81	325.00	.00	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5939E-01 EXCESS= .0000E+00 OUTFLOW= .6076E-01 BASIN STORAGE= .3101E-02 PERCENT ERROR= -7.5										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	4.50	265.74	216.00	1.66	5.00	258.56	215.00	1.66	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1506E+02 EXCESS= .0000E+00 OUTFLOW= .1510E+02 BASIN STORAGE= .5688E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	4.50	235.13	216.00	1.46	5.00	227.91	215.00	1.46	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1328E+02 EXCESS= .0000E+00 OUTFLOW= .1332E+02 BASIN STORAGE= .5195E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	4.00	215.51	216.00	1.33	5.00	208.54	215.00	1.33	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1207E+02 EXCESS= .0000E+00 OUTFLOW= .1211E+02 BASIN STORAGE= .6596E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	5.75	213.04	217.50	1.26	5.00	200.50	215.00	1.26	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1146E+02 EXCESS= .0000E+00 OUTFLOW= .1149E+02 BASIN STORAGE= .6273E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	4.00	186.04	216.00	1.15	5.00	180.01	220.00	1.15	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1044E+02 EXCESS= .0000E+00 OUTFLOW= .1047E+02 BASIN STORAGE= .5259E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	3.75	178.51	217.50	1.05	5.00	167.22	220.00	1.05	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9558E+01 EXCESS= .0000E+00 OUTFLOW= .9582E+01 BASIN STORAGE= .5960E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	3.00	117.10	219.00	.67	5.00	113.18	220.00	.67	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6066E+01 EXCESS= .0000E+00 OUTFLOW= .6080E+01 BASIN STORAGE= .5831E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	2.50	68.21	220.00	.39	5.00	68.21	220.00	.39	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3495E+01 EXCESS= .0000E+00 OUTFLOW= .3510E+01 BASIN STORAGE= .6046E-02 PERCENT ERROR= -.6										
FOR PLAN = 1	RATIO=	.00								
RC5FD	MANE	.75	20.08	229.50	.09	5.00	15.03	230.00	.10	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8362E+00 EXCESS= .0000E+00 OUTFLOW= .8529E+00 BASIN STORAGE= .6047E-02 PERCENT ERROR= -2.7										

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FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 3.00	1051.42	216.00	1.99	5.00	1021.36	215.00	1.98	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5349E+02 EXCESS= .0000E+00 OUTFLOW= .5369E+02 BASIN STORAGE= .1122E-01 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 3.25	873.95	214.50	1.76	5.00	870.05	215.00	1.75	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4736E+02 EXCESS= .0000E+00 OUTFLOW= .4754E+02 BASIN STORAGE= .1281E-01 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 3.75	824.79	217.50	1.63	5.00	811.52	215.00	1.63	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4398E+02 EXCESS= .0000E+00 OUTFLOW= .4413E+02 BASIN STORAGE= .1019E-01 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 4.00	756.64	216.00	1.53	5.00	746.59	215.00	1.53	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4132E+02 EXCESS= .0000E+00 OUTFLOW= .4150E+02 BASIN STORAGE= .9741E-02 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 4.00	704.23	216.00	1.42	5.00	693.66	215.00	1.42	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3824E+02 EXCESS= .0000E+00 OUTFLOW= .3843E+02 BASIN STORAGE= .1450E-01 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 4.25	644.56	216.75	1.30	5.00	633.64	215.00	1.30	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3509E+02 EXCESS= .0000E+00 OUTFLOW= .3527E+02 BASIN STORAGE= .1075E-01 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 3.75	471.25	217.50	.88	5.00	441.92	215.00	.88	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2377E+02 EXCESS= .0000E+00 OUTFLOW= .2389E+02 BASIN STORAGE= .1270E-01 PERCENT ERROR= -.6									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 3.75	290.43	217.50	.55	5.00	288.67	220.00	.55	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1480E+02 EXCESS= .0000E+00 OUTFLOW= .1487E+02 BASIN STORAGE= .1440E-01 PERCENT ERROR= -.6									
FOR PLAN = 1	RATIO= .00								
RC5FA	MANE 1.25	122.02	225.00	.17	5.00	122.02	225.00	.17	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4556E+01 EXCESS= .0000E+00 OUTFLOW= .4632E+01 BASIN STORAGE= .1288E-01 PERCENT ERROR= -2.0									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 3.11	1403.16	217.77	1.60	5.00	1314.84	215.00	1.60	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7997E+02 EXCESS= .0000E+00 OUTFLOW= .8004E+02 BASIN STORAGE= .3687E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 3.29	1194.52	217.26	1.40	5.00	1134.62	220.00	1.40	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7013E+02 EXCESS= .0000E+00 OUTFLOW= .7020E+02 BASIN STORAGE= .5218E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 3.39	1103.11	216.95	1.29	5.00	1063.76	220.00	1.29	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6439E+02 EXCESS= .0000E+00 OUTFLOW= .6445E+02 BASIN STORAGE= .5246E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 3.48	1019.30	219.49	1.21	5.00	1006.22	220.00	1.21	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6053E+02 EXCESS= .0000E+00 OUTFLOW= .6059E+02 BASIN STORAGE= .3595E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 3.60	945.78	219.33	1.11	5.00	931.65	220.00	1.11	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5556E+02 EXCESS= .0000E+00 OUTFLOW= .5561E+02 BASIN STORAGE= .4453E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 3.72	857.69	219.53	1.01	5.00	848.56	220.00	1.01	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5044E+02 EXCESS= .0000E+00 OUTFLOW= .5048E+02 BASIN STORAGE= .4601E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 4.00	574.69	220.00	.66	5.00	574.69	220.00	.66	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3283E+02 EXCESS= .0000E+00 OUTFLOW= .3289E+02 BASIN STORAGE= .5022E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 4.75	355.84	223.25	.39	5.00	334.09	225.00	.39	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1940E+02 EXCESS= .0000E+00 OUTFLOW= .1947E+02 BASIN STORAGE= .5564E-02 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO= .00								
RCP28	MANE 2.00	118.51	232.00	.11	5.00	85.31	235.00	.11	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5415E+01 EXCESS= .0000E+00 OUTFLOW= .5457E+01 BASIN STORAGE= .5115E-02 PERCENT ERROR= -.9									
FOR PLAN = 1	RATIO= .00								
RCP29	MANE 3.54	1502.56	219.50	1.49	5.00	1496.56	220.00	1.49	

SDN3.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9191E+02 EXCESS= .0000E+00 OUTFLOW= .9201E+02 BASIN STORAGE= .7348E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP29 MANE 3.76 1275.12 221.63 1.30 5.00 1265.89 220.00 1.30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8042E+02 EXCESS= .0000E+00 OUTFLOW= .8052E+02 BASIN STORAGE= .5594E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP29 MANE 3.86 1192.71 219.89 1.19 5.00 1192.21 220.00 1.19

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7354E+02 EXCESS= .0000E+00 OUTFLOW= .7365E+02 BASIN STORAGE= .7336E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP29 MANE 3.94 1101.06 220.78 1.11 5.00 1080.27 220.00 1.11

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6884E+02 EXCESS= .0000E+00 OUTFLOW= .6891E+02 BASIN STORAGE= .5421E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP29 MANE 4.06 1026.93 223.53 1.02 5.00 1006.78 220.00 1.03

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6315E+02 EXCESS= .0000E+00 OUTFLOW= .6324E+02 BASIN STORAGE= .5324E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP29 MANE 4.21 934.94 223.39 .93 5.00 902.98 220.00 .93

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5725E+02 EXCESS= .0000E+00 OUTFLOW= .5733E+02 BASIN STORAGE= .6303E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP29 MANE 4.50 624.52 225.00 .59 5.00 624.52 225.00 .60

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3669E+02 EXCESS= .0000E+00 OUTFLOW= .3675E+02 BASIN STORAGE= .5552E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP29 MANE 5.00 372.59 230.00 .34 5.00 372.59 230.00 .34

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2101E+02 EXCESS= .0000E+00 OUTFLOW= .2109E+02 BASIN STORAGE= .7294E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCP29 MANE 2.75 101.70 247.50 .09 5.00 64.76 245.00 .09

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5333E+01 EXCESS= .0000E+00 OUTFLOW= .5386E+01 BASIN STORAGE= .5404E-02 PERCENT ERROR= -1.1

FOR PLAN = 1 RATIO= .00
RCP30 MANE 2.72 2029.62 220.08 1.52 5.00 2026.82 220.00 1.52

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1333E+03 EXCESS= .0000E+00 OUTFLOW= .1333E+03 BASIN STORAGE= .5929E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP30 MANE 2.88 1721.73 221.69 1.33 5.00 1710.81 220.00 1.33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1168E+03 EXCESS= .0000E+00 OUTFLOW= .1168E+03 BASIN STORAGE= .5357E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP30 MANE 2.95 1600.01 221.49 1.21 5.00 1567.23 220.00 1.21

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1066E+03 EXCESS= .0000E+00 OUTFLOW= .1066E+03 BASIN STORAGE= .5307E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP30 MANE 3.05 1464.53 222.74 1.14 5.00 1443.99 220.00 1.14

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9976E+02 EXCESS= .0000E+00 OUTFLOW= .9978E+02 BASIN STORAGE= .5155E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP30 MANE 3.14 1356.89 222.71 1.04 5.00 1321.68 225.00 1.04

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9168E+02 EXCESS= .0000E+00 OUTFLOW= .9170E+02 BASIN STORAGE= .5863E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP30 MANE 3.26 1216.76 221.78 .95 5.00 1191.19 225.00 .95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8316E+02 EXCESS= .0000E+00 OUTFLOW= .8318E+02 BASIN STORAGE= .5655E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP30 MANE 3.85 781.98 227.30 .60 5.00 742.73 225.00 .60

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5306E+02 EXCESS= .0000E+00 OUTFLOW= .5309E+02 BASIN STORAGE= .6087E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP30 MANE 4.77 471.66 233.70 .34 5.00 435.30 235.00 .34

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3020E+02 EXCESS= .0000E+00 OUTFLOW= .3024E+02 BASIN STORAGE= .5718E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP30 MANE 2.25 80.67 254.25 .08 5.00 78.64 255.00 .08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7341E+01 EXCESS= .0000E+00 OUTFLOW= .7362E+01 BASIN STORAGE= .5717E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCSEB MANE 4.75 807.04 223.25 2.05 5.00 781.29 220.00 2.05

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5973E+02 EXCESS= .0000E+00 OUTFLOW= .5980E+02 BASIN STORAGE= .5530E-02 PERCENT ERROR= -.1

SDN3.OUT

FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	4.75	727.61	223.25	1.84	5.00	703.23	225.00	1.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5346E+02 EXCESS= .0000E+00 OUTFLOW= .5353E+02 BASIN STORAGE= .5274E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	4.75	673.13	223.25	1.69	5.00	651.61	225.00	1.69
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4922E+02 EXCESS= .0000E+00 OUTFLOW= .4927E+02 BASIN STORAGE= .5091E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	5.00	642.91	225.00	1.61	5.00	642.91	225.00	1.61
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4680E+02 EXCESS= .0000E+00 OUTFLOW= .4686E+02 BASIN STORAGE= .6495E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	5.00	600.00	225.00	1.49	5.00	600.00	225.00	1.49
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4341E+02 EXCESS= .0000E+00 OUTFLOW= .4346E+02 BASIN STORAGE= .6293E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	5.00	556.00	225.00	1.37	5.00	556.00	225.00	1.37
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3996E+02 EXCESS= .0000E+00 OUTFLOW= .4002E+02 BASIN STORAGE= .6080E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	5.00	387.14	225.00	.93	5.00	387.14	225.00	.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2710E+02 EXCESS= .0000E+00 OUTFLOW= .2714E+02 BASIN STORAGE= .6732E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	5.00	247.49	225.00	.59	5.00	247.49	225.00	.59
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1715E+02 EXCESS= .0000E+00 OUTFLOW= .1718E+02 BASIN STORAGE= .5661E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCSEB	MANE	2.00	77.25	232.00	.19	5.00	74.16	230.00	.19
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5638E+01 EXCESS= .0000E+00 OUTFLOW= .5656E+01 BASIN STORAGE= .5459E-02 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	2.79	2902.30	223.51	1.58	5.00	2865.38	225.00	1.58
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2040E+03 EXCESS= .0000E+00 OUTFLOW= .2040E+03 BASIN STORAGE= .4092E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	2.95	2492.69	223.84	1.39	5.00	2478.07	225.00	1.39
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1793E+03 EXCESS= .0000E+00 OUTFLOW= .1794E+03 BASIN STORAGE= .3702E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	3.04	2308.41	224.68	1.27	5.00	2301.23	225.00	1.27
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1636E+03 EXCESS= .0000E+00 OUTFLOW= .1637E+03 BASIN STORAGE= .4017E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	3.10	2184.12	226.49	1.20	5.00	2179.50	225.00	1.20
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1541E+03 EXCESS= .0000E+00 OUTFLOW= .1541E+03 BASIN STORAGE= .3630E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	3.20	2000.96	227.15	1.10	5.00	1997.66	225.00	1.10
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1417E+03 EXCESS= .0000E+00 OUTFLOW= .1417E+03 BASIN STORAGE= .4848E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	3.31	1797.37	224.90	1.00	5.00	1797.35	225.00	1.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1290E+03 EXCESS= .0000E+00 OUTFLOW= .1290E+03 BASIN STORAGE= .4560E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	3.85	1132.11	231.18	.65	5.00	1129.10	230.00	.65
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8311E+02 EXCESS= .0000E+00 OUTFLOW= .8315E+02 BASIN STORAGE= .4911E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	4.74	624.78	236.92	.38	5.00	597.50	235.00	.38
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4853E+02 EXCESS= .0000E+00 OUTFLOW= .4856E+02 BASIN STORAGE= .4141E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP31	MANE	3.25	117.51	237.25	.10	5.00	103.51	265.00	.10
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1294E+02 EXCESS= .0000E+00 OUTFLOW= .1298E+02 BASIN STORAGE= .4180E-02 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RCP32	MANE	1.11	2991.93	224.78	1.57	5.00	2989.98	225.00	1.57
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2153E+03 EXCESS= .0000E+00 OUTFLOW= .2153E+03 BASIN STORAGE= .1427E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP32	MANE	1.17	2580.51	225.71	1.38	5.00	2577.53	225.00	1.38

SDN3.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1893E+03 EXCESS= .0000E+00 OUTFLOW= .1893E+03 BASIN STORAGE= .1447E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP32 MANE 1.20 2386.33 225.62 1.26 5.00 2369.57 225.00 1.26

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1726E+03 EXCESS= .0000E+00 OUTFLOW= .1726E+03 BASIN STORAGE= .1485E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP32 MANE 1.22 2267.48 226.23 1.18 5.00 2245.76 225.00 1.19

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1625E+03 EXCESS= .0000E+00 OUTFLOW= .1625E+03 BASIN STORAGE= .1486E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP32 MANE 1.26 2066.75 226.83 1.09 5.00 2036.07 225.00 1.09

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1493E+03 EXCESS= .0000E+00 OUTFLOW= .1493E+03 BASIN STORAGE= .1518E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP32 MANE 1.31 1866.23 226.07 .99 5.00 1820.97 225.00 .99

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1359E+03 EXCESS= .0000E+00 OUTFLOW= .1359E+03 BASIN STORAGE= .1582E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP32 MANE 1.54 1156.00 230.77 .64 5.00 1141.85 230.00 .64

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8728E+02 EXCESS= .0000E+00 OUTFLOW= .8728E+02 BASIN STORAGE= .1544E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP32 MANE 1.92 614.08 238.09 .37 5.00 605.88 240.00 .37

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5068E+02 EXCESS= .0000E+00 OUTFLOW= .5068E+02 BASIN STORAGE= .1516E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP32 MANE 3.53 107.17 239.99 .10 5.00 107.10 240.00 .10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1322E+02 EXCESS= .0000E+00 OUTFLOW= .1324E+02 BASIN STORAGE= .1643E-02 PERCENT ERROR= -.1
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 1.68 4329.06 212.00 1.71 5.00 4193.31 220.00 1.71

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3794E+03 EXCESS= .0000E+00 OUTFLOW= .3795E+03 BASIN STORAGE= .3154E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 1.77 3770.59 211.90 1.51 5.00 3630.97 225.00 1.51

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3356E+03 EXCESS= .0000E+00 OUTFLOW= .3357E+03 BASIN STORAGE= .3385E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 1.83 3354.89 212.69 1.38 5.00 3315.38 225.00 1.38

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3069E+03 EXCESS= .0000E+00 OUTFLOW= .3069E+03 BASIN STORAGE= .2884E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 1.88 3165.12 212.08 1.30 5.00 3146.20 225.00 1.30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2900E+03 EXCESS= .0000E+00 OUTFLOW= .2900E+03 BASIN STORAGE= .3005E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 1.94 2868.71 226.58 1.20 5.00 2865.45 225.00 1.20

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2669E+03 EXCESS= .0000E+00 OUTFLOW= .2670E+03 BASIN STORAGE= .2850E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 2.01 2598.87 226.79 1.10 5.00 2575.97 225.00 1.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2439E+03 EXCESS= .0000E+00 OUTFLOW= .2439E+03 BASIN STORAGE= .3122E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 2.37 1601.46 213.01 .72 5.00 1491.44 230.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1593E+03 EXCESS= .0000E+00 OUTFLOW= .1593E+03 BASIN STORAGE= .3642E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 2.84 943.62 213.22 .43 5.00 856.71 215.00 .43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9524E+02 EXCESS= .0000E+00 OUTFLOW= .9526E+02 BASIN STORAGE= .3549E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP33 MANE 2.50 282.72 215.00 .12 5.00 282.72 215.00 .12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2691E+02 EXCESS= .0000E+00 OUTFLOW= .2693E+02 BASIN STORAGE= .3406E-02 PERCENT ERROR= -.1
 FOR PLAN = 1 RATIO= .00
 RCP24 MANE 1.45 5680.51 225.62 1.66 5.00 5646.38 225.00 1.66

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5180E+03 EXCESS= .0000E+00 OUTFLOW= .5181E+03 BASIN STORAGE= .2903E-02 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RCP24 MANE 1.55 4704.83 225.75 1.44 5.00 4680.58 225.00 1.44

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4493E+03 EXCESS= .0000E+00 OUTFLOW= .4494E+03 BASIN STORAGE= .2583E-02 PERCENT ERROR= .0

SDN3.OUT

FOR PLAN = 1	RATIO=	.00								
RCP24	MANE	1.61	4185.76	227.10	1.30	5.00	4158.45	225.00	1.30	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4071E+03 EXCESS= .0000E+00 OUTFLOW= .4071E+03 BASIN STORAGE= .2741E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP24	MANE	1.65	3911.68	226.04	1.23	5.00	3871.27	225.00	1.23	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3830E+03 EXCESS= .0000E+00 OUTFLOW= .3830E+03 BASIN STORAGE= .2853E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP24	MANE	1.71	3516.60	226.19	1.12	5.00	3475.85	225.00	1.12	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3503E+03 EXCESS= .0000E+00 OUTFLOW= .3503E+03 BASIN STORAGE= .3007E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP24	MANE	1.79	3124.56	227.06	1.02	5.00	3074.48	225.00	1.02	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3176E+03 EXCESS= .0000E+00 OUTFLOW= .3176E+03 BASIN STORAGE= .2796E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP24	MANE	2.19	1739.19	230.35	.64	5.00	1735.87	230.00	.64	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1995E+03 EXCESS= .0000E+00 OUTFLOW= .1996E+03 BASIN STORAGE= .2623E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP24	MANE	2.78	880.55	216.45	.36	5.00	869.79	215.00	.36	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1139E+03 EXCESS= .0000E+00 OUTFLOW= .1139E+03 BASIN STORAGE= .2802E-02 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO=	.00								
RCP24	MANE	2.75	260.53	220.00	.09	5.00	260.53	220.00	.09	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2934E+02 EXCESS= .0000E+00 OUTFLOW= .2936E+02 BASIN STORAGE= .2558E-02 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	4.00	515.13	220.00	1.58	5.00	515.13	220.00	1.59	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2719E+02 EXCESS= .0000E+00 OUTFLOW= .2749E+02 BASIN STORAGE= .2750E-01 PERCENT ERROR= -1.2										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	4.00	461.81	220.00	1.39	5.00	461.81	220.00	1.40	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2393E+02 EXCESS= .0000E+00 OUTFLOW= .2419E+02 BASIN STORAGE= .2380E-01 PERCENT ERROR= -1.2										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	3.75	440.89	221.25	1.28	5.00	405.48	225.00	1.27	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2199E+02 EXCESS= .0000E+00 OUTFLOW= .2221E+02 BASIN STORAGE= .2316E-01 PERCENT ERROR= -1.1										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	3.75	428.34	221.25	1.20	5.00	380.66	225.00	1.20	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2072E+02 EXCESS= .0000E+00 OUTFLOW= .2094E+02 BASIN STORAGE= .2134E-01 PERCENT ERROR= -1.2										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	3.50	387.43	220.50	1.10	5.00	355.05	225.00	1.11	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1894E+02 EXCESS= .0000E+00 OUTFLOW= .1917E+02 BASIN STORAGE= .2950E-01 PERCENT ERROR= -1.4										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	3.75	345.74	225.00	1.00	5.00	345.74	225.00	1.01	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1724E+02 EXCESS= .0000E+00 OUTFLOW= .1746E+02 BASIN STORAGE= .2993E-01 PERCENT ERROR= -1.5										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	2.75	254.21	228.25	.63	5.00	192.04	225.00	.63	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1076E+02 EXCESS= .0000E+00 OUTFLOW= .1095E+02 BASIN STORAGE= .2398E-01 PERCENT ERROR= -2.0										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	2.00	213.24	234.00	.37	5.00	142.42	235.00	.37	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6177E+01 EXCESS= .0000E+00 OUTFLOW= .6415E+01 BASIN STORAGE= .2793E-01 PERCENT ERROR= -4.3										
FOR PLAN = 1	RATIO=	.00								
RC5DC	MANE	.75	21.79	270.00	.09	5.00	21.79	270.00	.09	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1417E+01 EXCESS= .0000E+00 OUTFLOW= .1516E+01 BASIN STORAGE= .2620E-01 PERCENT ERROR= -8.8										
FOR PLAN = 1	RATIO=	.00								
RC48F	MANE	4.00	363.47	216.00	1.35	5.00	352.54	215.00	1.36	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1997E+02 EXCESS= .0000E+00 OUTFLOW= .2004E+02 BASIN STORAGE= .1211E-01 PERCENT ERROR= -.4										
FOR PLAN = 1	RATIO=	.00								
RC48F	MANE	3.75	337.00	217.50	1.19	5.00	314.01	215.00	1.19	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1759E+02 EXCESS= .0000E+00 OUTFLOW= .1766E+02 BASIN STORAGE= .1327E-01 PERCENT ERROR= -.5										
FOR PLAN = 1 RATIO= .00										

RC48F	MANE	3.50	305.01	217.00	1.07	5.00	SDN3.OUT 290.31	220.00	1.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1585E+02 EXCESS= .0000E+00 OUTFLOW= .1591E+02 BASIN STORAGE= .1242E-01 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RC48F	MANE	3.50	285.58	217.00	1.01	5.00	275.70	220.00	1.01
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1488E+02 EXCESS= .0000E+00 OUTFLOW= .1493E+02 BASIN STORAGE= .1223E-01 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RC48F	MANE	3.75	258.41	217.50	.92	5.00	249.91	220.00	.92
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1358E+02 EXCESS= .0000E+00 OUTFLOW= .1363E+02 BASIN STORAGE= .1077E-01 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO=	.00							
RC48F	MANE	3.50	233.74	220.50	.83	5.00	233.36	220.00	.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1222E+02 EXCESS= .0000E+00 OUTFLOW= .1227E+02 BASIN STORAGE= .1165E-01 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO=	.00							
RC48F	MANE	2.25	152.73	220.50	.50	5.00	148.55	220.00	.50
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7397E+01 EXCESS= .0000E+00 OUTFLOW= .7431E+01 BASIN STORAGE= .1079E-01 PERCENT ERROR= -.6									
FOR PLAN = 1	RATIO=	.00							
RC48F	MANE	1.25	96.41	221.25	.27	5.00	69.84	220.00	.28
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4005E+01 EXCESS= .0000E+00 OUTFLOW= .4053E+01 BASIN STORAGE= .1112E-01 PERCENT ERROR= -1.5									
FOR PLAN = 1	RATIO=	.00							
RC48F	MANE	1.25	14.22	248.75	.05	5.00	8.42	305.00	.05
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7294E+00 EXCESS= .0000E+00 OUTFLOW= .7626E+00 BASIN STORAGE= .9997E-02 PERCENT ERROR= -5.9									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	4.75	1822.41	303.86	1.37	5.00	1821.99	305.00	1.37
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5288E+03 EXCESS= .0000E+00 OUTFLOW= .5265E+03 BASIN STORAGE= .3549E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	1056.67	325.00	1.16	5.00	1056.67	325.00	1.16
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4484E+03 EXCESS= .0000E+00 OUTFLOW= .4460E+03 BASIN STORAGE= .3542E+01 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	662.77	225.00	1.05	5.00	662.77	225.00	1.05
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4064E+03 EXCESS= .0000E+00 OUTFLOW= .4036E+03 BASIN STORAGE= .3472E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	633.21	225.00	1.01	5.00	633.21	225.00	1.01
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3931E+03 EXCESS= .0000E+00 OUTFLOW= .3904E+03 BASIN STORAGE= .3347E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	592.53	225.00	.96	5.00	592.53	225.00	.96
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3739E+03 EXCESS= .0000E+00 OUTFLOW= .3714E+03 BASIN STORAGE= .3147E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	552.25	225.00	.91	5.00	552.25	225.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3528E+03 EXCESS= .0000E+00 OUTFLOW= .3505E+03 BASIN STORAGE= .2920E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	380.55	230.00	.62	5.00	380.55	230.00	.62
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2399E+03 EXCESS= .0000E+00 OUTFLOW= .2399E+03 BASIN STORAGE= .1746E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	234.50	235.00	.35	5.00	234.50	235.00	.35
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1367E+03 EXCESS= .0000E+00 OUTFLOW= .1367E+03 BASIN STORAGE= .1183E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP34	MANE	5.00	93.22	320.00	.09	5.00	93.22	320.00	.09
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3409E+02 EXCESS= .0000E+00 OUTFLOW= .3415E+02 BASIN STORAGE= .1066E-01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	583.82	230.00	-1.00	5.00	583.82	230.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	574.74	230.00	-1.00	5.00	574.74	230.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	492.40	235.00	-1.00	5.00	492.40	235.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	428.98	235.00	-1.00	5.00	428.98	235.00	-1.00

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FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	295.41	240.00	-1.00	5.00	295.41	240.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	196.68	240.00	-1.00	5.00	196.68	240.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	45.73	250.00	-1.00	5.00	45.73	250.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	5.00	18.99	275.00	-1.00	5.00	18.99	275.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RDIV5	MANE	2.25	3.85	303.75	-1.00	5.00	3.44	305.00	-1.00
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	4.70	2079.56	310.09	1.42	5.00	2077.79	310.00	1.42
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6147E+03 EXCESS= .0000E+00 OUTFLOW= .6125E+03 BASIN STORAGE= .3369E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	4.98	1698.15	234.12	1.20	5.00	1669.49	235.00	1.20
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5206E+03 EXCESS= .0000E+00 OUTFLOW= .5183E+03 BASIN STORAGE= .3367E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	5.00	1439.54	235.00	1.08	5.00	1439.54	235.00	1.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4684E+03 EXCESS= .0000E+00 OUTFLOW= .4661E+03 BASIN STORAGE= .3298E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	5.00	1281.77	240.00	1.04	5.00	1281.77	240.00	1.04
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4496E+03 EXCESS= .0000E+00 OUTFLOW= .4474E+03 BASIN STORAGE= .3176E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	5.00	1126.39	230.00	.97	5.00	1126.39	230.00	.97
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4229E+03 EXCESS= .0000E+00 OUTFLOW= .4209E+03 BASIN STORAGE= .2985E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	5.00	1018.42	230.00	.91	5.00	1018.42	230.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3950E+03 EXCESS= .0000E+00 OUTFLOW= .3932E+03 BASIN STORAGE= .2762E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	5.00	638.52	235.00	.62	5.00	638.52	235.00	.62
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2655E+03 EXCESS= .0000E+00 OUTFLOW= .2655E+03 BASIN STORAGE= .2096E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	5.00	340.93	240.00	.35	5.00	340.93	240.00	.35
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1503E+03 EXCESS= .0000E+00 OUTFLOW= .1504E+03 BASIN STORAGE= .8118E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP35	MANE	5.00	105.63	315.00	.08	5.00	105.63	315.00	.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3652E+02 EXCESS= .0000E+00 OUTFLOW= .3656E+02 BASIN STORAGE= .8690E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC4BE	MANE	5.00	240.64	230.00	1.60	5.00	240.64	230.00	1.60
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1880E+02 EXCESS= .0000E+00 OUTFLOW= .1884E+02 BASIN STORAGE= .1022E-01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RC4BE	MANE	5.00	214.71	230.00	1.42	5.00	214.71	230.00	1.42
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1663E+02 EXCESS= .0000E+00 OUTFLOW= .1666E+02 BASIN STORAGE= .9744E-02 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RC4BE	MANE	5.00	197.35	230.00	1.29	5.00	197.35	230.00	1.29
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1516E+02 EXCESS= .0000E+00 OUTFLOW= .1520E+02 BASIN STORAGE= .8589E-02 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RC4BE	MANE	5.00	187.03	230.00	1.22	5.00	187.03	230.00	1.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1432E+02 EXCESS= .0000E+00 OUTFLOW= .1435E+02 BASIN STORAGE= .8417E-02 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RC4BE	MANE	5.00	172.69	230.00	1.12	5.00	172.69	230.00	1.12
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1317E+02 EXCESS= .0000E+00 OUTFLOW= .1320E+02 BASIN STORAGE= .8170E-02 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RC4BE	MANE	5.00	158.02	230.00	1.02	5.00	158.02	230.00	1.02

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CONTINUITY SUMMARY (AC-FT) - INFLOW= .1200E+02 EXCESS= .0000E+00 OUTFLOW= .1203E+02 BASIN STORAGE= .1012E-01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RC4BE MANE 5.00 100.65 230.00 .66 5.00 100.65 230.00 .66

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7727E+01 EXCESS= .0000E+00 OUTFLOW= .7755E+01 BASIN STORAGE= .1033E-01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC4BE MANE 3.75 61.20 236.25 .39 5.00 58.43 235.00 .39

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4550E+01 EXCESS= .0000E+00 OUTFLOW= .4576E+01 BASIN STORAGE= .9482E-02 PERCENT ERROR= -.8

FOR PLAN = 1 RATIO= .00
RC4BE MANE 1.75 17.70 245.00 .10 5.00 17.70 245.00 .11

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1168E+01 EXCESS= .0000E+00 OUTFLOW= .1194E+01 BASIN STORAGE= .1009E-01 PERCENT ERROR= -3.0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 3.55 608.48 227.17 1.65 5.00 598.63 230.00 1.65

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5005E+02 EXCESS= .0000E+00 OUTFLOW= .5006E+02 BASIN STORAGE= .1213E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 3.66 535.72 230.34 1.47 5.00 535.48 230.00 1.47

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4441E+02 EXCESS= .0000E+00 OUTFLOW= .4442E+02 BASIN STORAGE= .1237E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 3.74 496.95 228.08 1.34 5.00 491.02 230.00 1.34

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4061E+02 EXCESS= .0000E+00 OUTFLOW= .4062E+02 BASIN STORAGE= .9618E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 3.79 466.22 227.50 1.27 5.00 462.58 230.00 1.27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3843E+02 EXCESS= .0000E+00 OUTFLOW= .3844E+02 BASIN STORAGE= .1021E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 3.87 433.70 228.41 1.17 5.00 429.87 230.00 1.17

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3541E+02 EXCESS= .0000E+00 OUTFLOW= .3542E+02 BASIN STORAGE= .1186E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 3.96 396.65 229.78 1.07 5.00 396.02 230.00 1.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3236E+02 EXCESS= .0000E+00 OUTFLOW= .3237E+02 BASIN STORAGE= .1025E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 4.42 257.20 229.87 .70 5.00 257.14 230.00 .70

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2120E+02 EXCESS= .0000E+00 OUTFLOW= .2120E+02 BASIN STORAGE= .9764E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 5.00 153.59 235.00 .42 5.00 153.59 235.00 .42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1274E+02 EXCESS= .0000E+00 OUTFLOW= .1274E+02 BASIN STORAGE= .8751E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP36 MANE 2.25 35.04 252.00 .12 5.00 32.40 255.00 .12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3641E+01 EXCESS= .0000E+00 OUTFLOW= .3643E+01 BASIN STORAGE= .1090E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP37 MANE 3.51 697.50 228.12 1.42 5.00 695.14 230.00 1.42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6179E+02 EXCESS= .0000E+00 OUTFLOW= .6180E+02 BASIN STORAGE= .1165E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP37 MANE 3.63 614.87 228.62 1.25 5.00 614.34 230.00 1.25

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5440E+02 EXCESS= .0000E+00 OUTFLOW= .5440E+02 BASIN STORAGE= .9295E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP37 MANE 3.72 561.81 230.37 1.13 5.00 558.95 230.00 1.13

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4943E+02 EXCESS= .0000E+00 OUTFLOW= .4944E+02 BASIN STORAGE= .9872E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP37 MANE 3.77 528.91 230.17 1.07 5.00 527.41 230.00 1.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4661E+02 EXCESS= .0000E+00 OUTFLOW= .4662E+02 BASIN STORAGE= .9695E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP37 MANE 3.85 486.31 231.13 .98 5.00 478.68 230.00 .98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4267E+02 EXCESS= .0000E+00 OUTFLOW= .4268E+02 BASIN STORAGE= .1131E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP37 MANE 3.94 443.33 232.18 .89 5.00 431.74 230.00 .89

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3876E+02 EXCESS= .0000E+00 OUTFLOW= .3877E+02 BASIN STORAGE= .1055E-02 PERCENT ERROR= .0

SDN3.OUT									
FOR PLAN = 1	RATIO=	.00							
RCP37	MANE	4.40	281.31	233.13	.57	5.00	278.26	235.00	.57
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2464E+02 EXCESS= .0000E+00 OUTFLOW= .2464E+02 BASIN STORAGE= .8932E-03 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP37	MANE	5.00	161.07	240.00	.33	5.00	161.07	240.00	.33
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1422E+02 EXCESS= .0000E+00 OUTFLOW= .1423E+02 BASIN STORAGE= .9275E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP37	MANE	3.00	32.06	261.00	.08	5.00	31.40	260.00	.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3701E+01 EXCESS= .0000E+00 OUTFLOW= .3704E+01 BASIN STORAGE= .8981E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	.88	5118.44	230.88	1.12	5.00	5089.31	230.00	1.12
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1509E+04 EXCESS= .0000E+00 OUTFLOW= .1508E+04 BASIN STORAGE= .1266E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	.92	4458.39	230.84	.99	5.00	4425.01	230.00	.99
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1337E+04 EXCESS= .0000E+00 OUTFLOW= .1336E+04 BASIN STORAGE= .1228E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	.95	3966.41	231.75	.91	5.00	3941.48	235.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1230E+04 EXCESS= .0000E+00 OUTFLOW= .1229E+04 BASIN STORAGE= .1184E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	.97	3711.62	231.57	.87	5.00	3680.62	230.00	.87
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1179E+04 EXCESS= .0000E+00 OUTFLOW= .1178E+04 BASIN STORAGE= .1145E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	1.00	3389.22	231.15	.82	5.00	3349.33	230.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1108E+04 EXCESS= .0000E+00 OUTFLOW= .1107E+04 BASIN STORAGE= .1087E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	1.03	3015.22	231.37	.76	5.00	2965.01	230.00	.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1033E+04 EXCESS= .0000E+00 OUTFLOW= .1032E+04 BASIN STORAGE= .1017E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	1.22	1733.33	236.18	.53	5.00	1706.62	235.00	.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7150E+03 EXCESS= .0000E+00 OUTFLOW= .7146E+03 BASIN STORAGE= .4554E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	1.52	849.13	242.26	.31	5.00	835.61	245.00	.31
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4118E+03 EXCESS= .0000E+00 OUTFLOW= .4118E+03 BASIN STORAGE= .2991E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP38	MANE	2.34	211.29	347.97	.07	5.00	209.68	350.00	.07
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9555E+02 EXCESS= .0000E+00 OUTFLOW= .9555E+02 BASIN STORAGE= .1334E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RDB5	MANE	5.00	89.79	365.00	.56	5.00	89.79	365.00	.56
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1627E+03 EXCESS= .0000E+00 OUTFLOW= .1609E+03 BASIN STORAGE= .1962E+01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RDB5	MANE	5.00	87.71	365.00	.54	5.00	87.71	365.00	.54
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1576E+03 EXCESS= .0000E+00 OUTFLOW= .1558E+03 BASIN STORAGE= .1924E+01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RDB5	MANE	5.00	86.11	365.00	.53	5.00	86.11	365.00	.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1538E+03 EXCESS= .0000E+00 OUTFLOW= .1521E+03 BASIN STORAGE= .1894E+01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RDB5	MANE	5.00	85.07	365.00	.52	5.00	85.07	365.00	.52
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1516E+03 EXCESS= .0000E+00 OUTFLOW= .1499E+03 BASIN STORAGE= .1876E+01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RDB5	MANE	5.00	83.64	365.00	.51	5.00	83.64	365.00	.51
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1484E+03 EXCESS= .0000E+00 OUTFLOW= .1467E+03 BASIN STORAGE= .1849E+01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RDB5	MANE	5.00	82.16	365.00	.50	5.00	82.16	365.00	.50
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1449E+03 EXCESS= .0000E+00 OUTFLOW= .1432E+03 BASIN STORAGE= .1815E+01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RDB5	MANE	5.00	75.19	340.00	.44	5.00	75.19	340.00	.44

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1275E+03 EXCESS= .0000E+00 OUTFLOW= .1259E+03 BASIN STORAGE= .1631E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RDB5 MANE 5.00 66.99 330.00 .36 5.00 66.99 330.00 .36

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1049E+03 EXCESS= .0000E+00 OUTFLOW= .1037E+03 BASIN STORAGE= .1339E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RDB5 MANE 5.00 46.64 245.00 .13 5.00 46.64 245.00 .13

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3661E+02 EXCESS= .0000E+00 OUTFLOW= .3662E+02 BASIN STORAGE= .7622E-01 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP39 MANE 3.65 670.36 219.18 .66 5.00 667.24 220.00 .66

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2060E+03 EXCESS= .0000E+00 OUTFLOW= .2052E+03 BASIN STORAGE= .1111E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 3.79 606.80 219.75 .63 5.00 605.79 220.00 .63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1961E+03 EXCESS= .0000E+00 OUTFLOW= .1952E+03 BASIN STORAGE= .1089E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 3.89 557.35 221.91 .60 5.00 556.01 220.00 .61

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1889E+03 EXCESS= .0000E+00 OUTFLOW= .1881E+03 BASIN STORAGE= .1072E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 3.96 532.64 221.78 .59 5.00 529.65 220.00 .59

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1851E+03 EXCESS= .0000E+00 OUTFLOW= .1842E+03 BASIN STORAGE= .1062E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 4.06 505.14 219.29 .57 5.00 503.55 220.00 .57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1795E+03 EXCESS= .0000E+00 OUTFLOW= .1786E+03 BASIN STORAGE= .1047E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 4.17 466.24 221.14 .55 5.00 459.27 220.00 .55

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1733E+03 EXCESS= .0000E+00 OUTFLOW= .1725E+03 BASIN STORAGE= .1028E+01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 4.74 329.37 222.91 .47 5.00 320.75 220.00 .47

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1463E+03 EXCESS= .0000E+00 OUTFLOW= .1456E+03 BASIN STORAGE= .9244E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 5.00 219.37 220.00 .37 5.00 219.37 220.00 .37

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1167E+03 EXCESS= .0000E+00 OUTFLOW= .1161E+03 BASIN STORAGE= .7602E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP39 MANE 5.00 83.43 240.00 .13 5.00 83.43 240.00 .13

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4093E+02 EXCESS= .0000E+00 OUTFLOW= .4092E+02 BASIN STORAGE= .4313E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP40 MANE 1.32 1058.76 217.37 .72 5.00 1043.29 220.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2341E+03 EXCESS= .0000E+00 OUTFLOW= .2338E+03 BASIN STORAGE= .4579E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP40 MANE 1.37 954.43 217.52 .68 5.00 943.40 220.00 .68

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2213E+03 EXCESS= .0000E+00 OUTFLOW= .2210E+03 BASIN STORAGE= .4488E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP40 MANE 1.41 883.66 216.44 .65 5.00 868.85 220.00 .65

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2124E+03 EXCESS= .0000E+00 OUTFLOW= .2120E+03 BASIN STORAGE= .4417E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP40 MANE 1.43 841.18 217.43 .64 5.00 829.45 220.00 .64

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2072E+03 EXCESS= .0000E+00 OUTFLOW= .2069E+03 BASIN STORAGE= .4375E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP40 MANE 1.47 786.78 216.95 .61 5.00 779.94 220.00 .62

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1998E+03 EXCESS= .0000E+00 OUTFLOW= .1995E+03 BASIN STORAGE= .4312E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP40 MANE 1.51 723.27 217.62 .59 5.00 716.90 220.00 .59

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1921E+03 EXCESS= .0000E+00 OUTFLOW= .1917E+03 BASIN STORAGE= .4231E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP40 MANE 1.72 501.73 221.57 .49 5.00 498.42 220.00 .49

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1589E+03 EXCESS= .0000E+00 OUTFLOW= .1586E+03 BASIN STORAGE= .3801E+00 PERCENT ERROR= .0

SDN3.OUT

FOR PLAN = 1	RATIO=	.00							
RCP40	MANE	1.97	334.99	223.13	.38	5.00	330.19	220.00	.38
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1246E+03 EXCESS= .0000E+00 OUTFLOW= .1244E+03 BASIN STORAGE= .3118E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP40	MANE	3.07	95.04	242.17	.14	5.00	94.39	245.00	.14
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4394E+02 EXCESS= .0000E+00 OUTFLOW= .4393E+02 BASIN STORAGE= .1688E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	2.66	2515.68	213.01	2.11	5.00	2331.08	210.00	2.11
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1394E+03 EXCESS= .0000E+00 OUTFLOW= .1396E+03 BASIN STORAGE= .5843E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	2.77	2274.47	213.06	1.89	5.00	2090.23	210.00	1.89
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1248E+03 EXCESS= .0000E+00 OUTFLOW= .1249E+03 BASIN STORAGE= .7247E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	2.85	2067.57	213.59	1.74	5.00	1917.86	215.00	1.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1149E+03 EXCESS= .0000E+00 OUTFLOW= .1150E+03 BASIN STORAGE= .7201E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	2.90	1950.31	211.63	1.66	5.00	1839.08	215.00	1.65
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1092E+03 EXCESS= .0000E+00 OUTFLOW= .1093E+03 BASIN STORAGE= .5852E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	2.98	1793.07	214.29	1.53	5.00	1719.86	215.00	1.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1011E+03 EXCESS= .0000E+00 OUTFLOW= .1012E+03 BASIN STORAGE= .7399E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	3.06	1656.64	214.45	1.41	5.00	1603.55	215.00	1.42
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9316E+02 EXCESS= .0000E+00 OUTFLOW= .9327E+02 BASIN STORAGE= .5318E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	3.51	1182.37	214.29	.96	5.00	1142.09	215.00	.96
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6351E+02 EXCESS= .0000E+00 OUTFLOW= .6359E+02 BASIN STORAGE= .7243E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	3.50	776.11	213.50	.61	5.00	752.56	215.00	.61
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4044E+02 EXCESS= .0000E+00 OUTFLOW= .4050E+02 BASIN STORAGE= .7313E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RC3B3C	MANE	1.50	262.06	216.00	.20	5.00	254.16	215.00	.20
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1341E+02 EXCESS= .0000E+00 OUTFLOW= .1343E+02 BASIN STORAGE= .5216E-02 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	4.00	2754.58	216.00	2.08	5.00	2678.06	220.00	2.09
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1731E+03 EXCESS= .0000E+00 OUTFLOW= .1734E+03 BASIN STORAGE= .1191E-01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	3.75	2571.81	217.50	1.86	5.00	2409.24	215.00	1.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1547E+03 EXCESS= .0000E+00 OUTFLOW= .1550E+03 BASIN STORAGE= .1576E-01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	4.00	2265.53	216.00	1.71	5.00	2250.04	220.00	1.72
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1423E+03 EXCESS= .0000E+00 OUTFLOW= .1426E+03 BASIN STORAGE= .1164E-01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	4.25	2168.78	216.75	1.63	5.00	2112.76	220.00	1.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1352E+03 EXCESS= .0000E+00 OUTFLOW= .1355E+03 BASIN STORAGE= .1193E-01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	4.50	2006.30	220.50	1.51	5.00	2003.72	220.00	1.51
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1254E+03 EXCESS= .0000E+00 OUTFLOW= .1257E+03 BASIN STORAGE= .1598E-01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	5.00	1912.64	220.00	1.40	5.00	1912.64	220.00	1.40
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1159E+03 EXCESS= .0000E+00 OUTFLOW= .1162E+03 BASIN STORAGE= .1584E-01 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	4.75	1304.72	218.50	.95	5.00	1286.80	220.00	.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7853E+02 EXCESS= .0000E+00 OUTFLOW= .7876E+02 BASIN STORAGE= .1178E-01 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RCP41	MANE	4.25	838.26	221.00	.60	5.00	810.72	220.00	.60

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4952E+02 EXCESS= .0000E+00 OUTFLOW= .4968E+02 BASIN STORAGE= .1469E-01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP41 MANE 1.50 359.83 225.00 .20 5.00 359.83 225.00 .21

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1623E+02 EXCESS= .0000E+00 OUTFLOW= .1641E+02 BASIN STORAGE= .1084E-01 PERCENT ERROR= -1.2

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 4538.36 220.00 1.05 5.00 4538.36 220.00 1.05

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4570E+03 EXCESS= .0000E+00 OUTFLOW= .4559E+03 BASIN STORAGE= .3690E+01 PERCENT ERROR= -.6

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 4096.76 220.00 .96 5.00 4096.76 220.00 .96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4202E+03 EXCESS= .0000E+00 OUTFLOW= .4191E+03 BASIN STORAGE= .3618E+01 PERCENT ERROR= -.6

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 3704.58 220.00 .91 5.00 3704.58 220.00 .91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3950E+03 EXCESS= .0000E+00 OUTFLOW= .3939E+03 BASIN STORAGE= .3563E+01 PERCENT ERROR= -.6

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 3480.60 220.00 .87 5.00 3480.60 220.00 .87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3801E+03 EXCESS= .0000E+00 OUTFLOW= .3784E+03 BASIN STORAGE= .3531E+01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 3226.21 225.00 .82 5.00 3226.21 225.00 .82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3605E+03 EXCESS= .0000E+00 OUTFLOW= .3588E+03 BASIN STORAGE= .3482E+01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 3059.85 225.00 .78 5.00 3059.85 225.00 .78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3400E+03 EXCESS= .0000E+00 OUTFLOW= .3384E+03 BASIN STORAGE= .3418E+01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 2113.90 225.00 .59 5.00 2113.90 225.00 .59

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2582E+03 EXCESS= .0000E+00 OUTFLOW= .2569E+03 BASIN STORAGE= .3083E+01 PERCENT ERROR= -.7

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 1345.59 230.00 .43 5.00 1345.59 230.00 .43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1867E+03 EXCESS= .0000E+00 OUTFLOW= .1854E+03 BASIN STORAGE= .2551E+01 PERCENT ERROR= -.7

FOR PLAN = 1 RATIO= .00
RCP42 MANE 5.00 467.03 240.00 .15 5.00 467.03 240.00 .15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6492E+02 EXCESS= .0000E+00 OUTFLOW= .6505E+02 BASIN STORAGE= .1495E+00 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 5325.73 235.00 1.04 5.00 5325.73 235.00 1.04

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4636E+03 EXCESS= .0000E+00 OUTFLOW= .4610E+03 BASIN STORAGE= .8587E+01 PERCENT ERROR= -1.3

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 4904.71 235.00 .96 5.00 4904.71 235.00 .96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4257E+03 EXCESS= .0000E+00 OUTFLOW= .4226E+03 BASIN STORAGE= .8413E+01 PERCENT ERROR= -1.2

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 4302.55 235.00 .90 5.00 4302.55 235.00 .90

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3997E+03 EXCESS= .0000E+00 OUTFLOW= .3966E+03 BASIN STORAGE= .8275E+01 PERCENT ERROR= -1.3

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 3894.44 240.00 .86 5.00 3894.44 240.00 .86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3839E+03 EXCESS= .0000E+00 OUTFLOW= .3809E+03 BASIN STORAGE= .8197E+01 PERCENT ERROR= -1.4

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 3839.75 240.00 .82 5.00 3839.75 240.00 .82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3637E+03 EXCESS= .0000E+00 OUTFLOW= .3608E+03 BASIN STORAGE= .8081E+01 PERCENT ERROR= -1.4

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 3870.61 240.00 .77 5.00 3870.61 240.00 .77

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3427E+03 EXCESS= .0000E+00 OUTFLOW= .3399E+03 BASIN STORAGE= .7925E+01 PERCENT ERROR= -1.5

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 2747.09 245.00 .58 5.00 2747.09 245.00 .58

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2592E+03 EXCESS= .0000E+00 OUTFLOW= .2565E+03 BASIN STORAGE= .7120E+01 PERCENT ERROR= -1.7

FOR PLAN = 1 RATIO= .00
RCP43 MANE 5.00 1798.55 255.00 .42 5.00 1798.55 255.00 .42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1865E+03 EXCESS= .0000E+00 OUTFLOW= .1844E+03 BASIN STORAGE= .5868E+01 PERCENT ERROR= -2.0

SDN3.OUT

FOR PLAN = 1	RATIO=	.00							
RCP43	MANE	5.00	660.47	280.00	.15	5.00	660.47	280.00	.15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6512E+02 EXCESS= .0000E+00 OUTFLOW= .6615E+02 BASIN STORAGE= .2841E+00 PERCENT ERROR= -2.0

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	5.00	298.87	240.00	1.32	5.00	298.87	240.00	1.32

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2857E+02 EXCESS= .0000E+00 OUTFLOW= .2861E+02 BASIN STORAGE= .1126E-01 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	5.00	259.71	240.00	1.14	5.00	259.71	240.00	1.14

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2478E+02 EXCESS= .0000E+00 OUTFLOW= .2482E+02 BASIN STORAGE= .1066E-01 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	5.00	233.25	240.00	1.03	5.00	233.25	240.00	1.03

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2226E+02 EXCESS= .0000E+00 OUTFLOW= .2230E+02 BASIN STORAGE= .1022E-01 PERCENT ERROR= -.2

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	5.00	218.03	240.00	.96	5.00	218.03	240.00	.96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2083E+02 EXCESS= .0000E+00 OUTFLOW= .2087E+02 BASIN STORAGE= .9962E-02 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	5.00	197.11	240.00	.87	5.00	197.11	240.00	.87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1887E+02 EXCESS= .0000E+00 OUTFLOW= .1891E+02 BASIN STORAGE= .9589E-02 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	5.00	176.03	240.00	.78	5.00	176.03	240.00	.78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1691E+02 EXCESS= .0000E+00 OUTFLOW= .1695E+02 BASIN STORAGE= .1209E-01 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	3.00	100.98	246.00	.46	5.00	99.82	245.00	.46

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9970E+01 EXCESS= .0000E+00 OUTFLOW= .1000E+02 BASIN STORAGE= .1168E-01 PERCENT ERROR= -.4

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	2.25	53.97	252.00	.24	5.00	45.10	255.00	.24

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5148E+01 EXCESS= .0000E+00 OUTFLOW= .5181E+01 BASIN STORAGE= .1016E-01 PERCENT ERROR= -.8

FOR PLAN = 1	RATIO=	.00							
RC4BA3	MANE	3.50	7.33	287.00	.03	5.00	5.82	335.00	.03

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7403E+00 EXCESS= .0000E+00 OUTFLOW= .7560E+00 BASIN STORAGE= .1016E-01 PERCENT ERROR= -3.5

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.02	5597.19	235.94	1.05	5.00	5371.98	235.00	1.05

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5033E+03 EXCESS= .0000E+00 OUTFLOW= .5030E+03 BASIN STORAGE= .5051E+00 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.05	5133.83	235.98	.96	5.00	4754.09	235.00	.96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4591E+03 EXCESS= .0000E+00 OUTFLOW= .4589E+03 BASIN STORAGE= .4945E+00 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.09	4546.36	236.86	.90	5.00	4231.71	240.00	.90

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4293E+03 EXCESS= .0000E+00 OUTFLOW= .4290E+03 BASIN STORAGE= .4861E+00 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.12	4177.41	237.10	.86	5.00	4134.45	240.00	.86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4114E+03 EXCESS= .0000E+00 OUTFLOW= .4111E+03 BASIN STORAGE= .4814E+00 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.13	3993.42	240.77	.81	5.00	3964.32	240.00	.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3883E+03 EXCESS= .0000E+00 OUTFLOW= .3880E+03 BASIN STORAGE= .4744E+00 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.13	3933.70	240.66	.76	5.00	3787.50	240.00	.76

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3645E+03 EXCESS= .0000E+00 OUTFLOW= .3642E+03 BASIN STORAGE= .4649E+00 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.26	2723.21	245.81	.57	5.00	2538.55	245.00	.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2706E+03 EXCESS= .0000E+00 OUTFLOW= .2704E+03 BASIN STORAGE= .4167E+00 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO=	.00							
RCP44	MANE	1.44	1788.49	256.47	.40	5.00	1708.31	255.00	.40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1915E+03 EXCESS= .0000E+00 OUTFLOW= .1913E+03 BASIN STORAGE= .3425E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00

RCP44	MANE	1.98	609.88	282.43	.14	5.00	SDN3.OUT 502.69	280.00	.14
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .6705E+02 EXCESS= .0000E+00 OUTFLOW= .6706E+02 BASIN STORAGE= .1443E-01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	.72	10261.79	236.02	1.10	5.00	10133.64	235.00	1.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2025E+04 EXCESS= .0000E+00 OUTFLOW= .2024E+04 BASIN STORAGE= .1657E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	.74	9188.54	235.91	.98	5.00	8908.21	235.00	.98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1807E+04 EXCESS= .0000E+00 OUTFLOW= .1806E+04 BASIN STORAGE= .1612E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	.78	8082.18	236.74	.91	5.00	8064.12	240.00	.91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1669E+04 EXCESS= .0000E+00 OUTFLOW= .1668E+04 BASIN STORAGE= .1562E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	.79	7678.38	240.26	.87	5.00	7661.46	240.00	.87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1600E+04 EXCESS= .0000E+00 OUTFLOW= .1599E+04 BASIN STORAGE= .1519E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	.81	7132.91	240.73	.82	5.00	7064.60	240.00	.82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1505E+04 EXCESS= .0000E+00 OUTFLOW= .1504E+04 BASIN STORAGE= .1456E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	.83	6554.15	241.30	.76	5.00	6430.73	240.00	.76

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1405E+04 EXCESS= .0000E+00 OUTFLOW= .1404E+04 BASIN STORAGE= .1379E+01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	.98	4095.82	246.34	.54	5.00	3922.66	245.00	.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9902E+03 EXCESS= .0000E+00 OUTFLOW= .9897E+03 BASIN STORAGE= .7815E+00 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	1.17	2394.32	256.34	.33	5.00	2303.46	255.00	.33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6059E+03 EXCESS= .0000E+00 OUTFLOW= .6057E+03 BASIN STORAGE= .3649E+00 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP45	MANE	1.82	653.43	282.75	.09	5.00	613.87	285.00	.09

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1627E+03 EXCESS= .0000E+00 OUTFLOW= .1627E+03 BASIN STORAGE= .2910E-01 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	5.00	763.53	220.00	1.73	5.00	763.53	220.00	1.73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4718E+02 EXCESS= .0000E+00 OUTFLOW= .4730E+02 BASIN STORAGE= .1272E-01 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	5.00	683.01	220.00	1.53	5.00	683.01	220.00	1.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4189E+02 EXCESS= .0000E+00 OUTFLOW= .4200E+02 BASIN STORAGE= .1227E-01 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	5.00	627.72	220.00	1.40	5.00	627.72	220.00	1.40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3832E+02 EXCESS= .0000E+00 OUTFLOW= .3842E+02 BASIN STORAGE= .1194E-01 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	5.00	595.47	220.00	1.33	5.00	595.47	220.00	1.33

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3626E+02 EXCESS= .0000E+00 OUTFLOW= .3635E+02 BASIN STORAGE= .1174E-01 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	5.00	550.49	220.00	1.22	5.00	550.49	220.00	1.22

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3343E+02 EXCESS= .0000E+00 OUTFLOW= .3353E+02 BASIN STORAGE= .1145E-01 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	4.75	482.10	218.50	1.12	5.00	481.45	220.00	1.12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3055E+02 EXCESS= .0000E+00 OUTFLOW= .3065E+02 BASIN STORAGE= .1192E-01 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	4.00	321.19	224.00	.73	5.00	320.40	220.00	.73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2000E+02 EXCESS= .0000E+00 OUTFLOW= .2006E+02 BASIN STORAGE= .1064E-01 PERCENT ERROR= -.4

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	3.50	200.24	224.00	.44	5.00	196.20	225.00	.44

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1208E+02 EXCESS= .0000E+00 OUTFLOW= .1214E+02 BASIN STORAGE= .1138E-01 PERCENT ERROR= -.5

FOR PLAN = 1	RATIO=	.00							
RC3A2B	MANE	1.25	69.39	230.00	.13	5.00	69.39	230.00	.13

SDN3.OUT
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3383E+01 EXCESS= .0000E+00 OUTFLOW= .3448E+01 BASIN STORAGE= .1055E-01 PERCENT ERROR= -2.2

FOR PLAN = 1 RATIO= .00
RCP46 MANE 4.01 1035.68 224.38 1.29 5.00 1018.17 225.00 1.29

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6786E+02 EXCESS= .0000E+00 OUTFLOW= .6793E+02 BASIN STORAGE= .5306E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP46 MANE 4.20 912.28 222.86 1.13 5.00 878.93 225.00 1.12

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5936E+02 EXCESS= .0000E+00 OUTFLOW= .5943E+02 BASIN STORAGE= .7146E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP46 MANE 4.36 813.88 222.44 1.02 5.00 797.24 225.00 1.01

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5353E+02 EXCESS= .0000E+00 OUTFLOW= .5361E+02 BASIN STORAGE= .7568E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP46 MANE 4.46 775.02 223.13 .96 5.00 755.01 225.00 .95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5039E+02 EXCESS= .0000E+00 OUTFLOW= .5048E+02 BASIN STORAGE= .6861E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP46 MANE 4.62 697.21 226.25 .87 5.00 691.84 225.00 .87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4601E+02 EXCESS= .0000E+00 OUTFLOW= .4607E+02 BASIN STORAGE= .6103E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP46 MANE 4.86 616.33 223.62 .79 5.00 608.23 225.00 .79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4152E+02 EXCESS= .0000E+00 OUTFLOW= .4159E+02 BASIN STORAGE= .5474E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP46 MANE 5.00 396.36 225.00 .49 5.00 396.36 225.00 .49

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2574E+02 EXCESS= .0000E+00 OUTFLOW= .2581E+02 BASIN STORAGE= .6766E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCP46 MANE 4.50 232.74 229.50 .28 5.00 229.27 230.00 .28

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1448E+02 EXCESS= .0000E+00 OUTFLOW= .1454E+02 BASIN STORAGE= .6835E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCP46 MANE 2.00 100.61 242.00 .07 5.00 43.85 250.00 .07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3730E+01 EXCESS= .0000E+00 OUTFLOW= .3796E+01 BASIN STORAGE= .5320E-02 PERCENT ERROR= -1.9

FOR PLAN = 1 RATIO= .00
RCP47 MANE 3.40 1099.48 224.58 1.18 5.00 1098.29 225.00 1.18

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7749E+02 EXCESS= .0000E+00 OUTFLOW= .7751E+02 BASIN STORAGE= .1044E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP47 MANE 3.53 949.63 225.95 1.02 5.00 934.78 225.00 1.02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6728E+02 EXCESS= .0000E+00 OUTFLOW= .6730E+02 BASIN STORAGE= .1126E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP47 MANE 3.62 857.13 227.98 .92 5.00 839.97 225.00 .92

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6037E+02 EXCESS= .0000E+00 OUTFLOW= .6039E+02 BASIN STORAGE= .1074E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP47 MANE 3.67 813.48 227.52 .86 5.00 789.49 225.00 .86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5674E+02 EXCESS= .0000E+00 OUTFLOW= .5676E+02 BASIN STORAGE= .1247E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP47 MANE 3.75 737.64 228.88 .79 5.00 717.37 230.00 .79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5179E+02 EXCESS= .0000E+00 OUTFLOW= .5181E+02 BASIN STORAGE= .1025E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP47 MANE 3.87 654.90 228.59 .71 5.00 634.39 230.00 .71

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4653E+02 EXCESS= .0000E+00 OUTFLOW= .4655E+02 BASIN STORAGE= .9875E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP47 MANE 4.33 441.45 229.28 .43 5.00 433.08 230.00 .43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2836E+02 EXCESS= .0000E+00 OUTFLOW= .2837E+02 BASIN STORAGE= .1335E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RCP47 MANE 4.75 222.46 232.75 .24 5.00 219.69 235.00 .24

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1549E+02 EXCESS= .0000E+00 OUTFLOW= .1552E+02 BASIN STORAGE= .1282E-02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RCP47 MANE 3.00 44.34 258.00 .06 5.00 41.92 255.00 .06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3671E+01 EXCESS= .0000E+00 OUTFLOW= .3681E+01 BASIN STORAGE= .1106E-02 PERCENT ERROR= -.3

		SDN3.OUT							
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	.70	10913.37	236.10	1.10	5.00	10796.40	235.00	1.10
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2119E+04 EXCESS= .0000E+00 OUTFLOW= .2118E+04 BASIN STORAGE= .1658E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	.73	9670.54	236.27	.98	5.00	9417.31	235.00	.98
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1889E+04 EXCESS= .0000E+00 OUTFLOW= .1887E+04 BASIN STORAGE= .1613E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	.76	8633.43	240.21	.91	5.00	8629.12	240.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1742E+04 EXCESS= .0000E+00 OUTFLOW= .1741E+04 BASIN STORAGE= .1563E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	.77	8186.75	240.53	.87	5.00	8154.30	240.00	.87
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1669E+04 EXCESS= .0000E+00 OUTFLOW= .1668E+04 BASIN STORAGE= .1520E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	.79	7564.87	240.83	.82	5.00	7483.36	240.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1568E+04 EXCESS= .0000E+00 OUTFLOW= .1567E+04 BASIN STORAGE= .1457E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	.82	6883.04	241.13	.76	5.00	6730.56	240.00	.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1461E+04 EXCESS= .0000E+00 OUTFLOW= .1460E+04 BASIN STORAGE= .1380E+01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	.97	4175.00	246.26	.53	5.00	4000.87	245.00	.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1025E+04 EXCESS= .0000E+00 OUTFLOW= .1024E+04 BASIN STORAGE= .7849E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	1.17	2371.81	256.86	.33	5.00	2281.39	255.00	.33
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6250E+03 EXCESS= .0000E+00 OUTFLOW= .6248E+03 BASIN STORAGE= .3656E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP48	MANE	1.85	621.87	286.92	.09	5.00	604.59	285.00	.09
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1672E+03 EXCESS= .0000E+00 OUTFLOW= .1672E+03 BASIN STORAGE= .2918E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	4.25	137.70	225.25	.87	5.00	137.38	225.00	.87
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9664E+01 EXCESS= .0000E+00 OUTFLOW= .9669E+01 BASIN STORAGE= .1103E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	4.00	118.35	224.00	.74	5.00	117.07	225.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8233E+01 EXCESS= .0000E+00 OUTFLOW= .8238E+01 BASIN STORAGE= .1064E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	3.25	103.05	224.25	.65	5.00	102.31	225.00	.65
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7282E+01 EXCESS= .0000E+00 OUTFLOW= .7285E+01 BASIN STORAGE= .1026E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	3.25	95.00	224.25	.60	5.00	94.44	225.00	.60
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6746E+01 EXCESS= .0000E+00 OUTFLOW= .6750E+01 BASIN STORAGE= .9884E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	2.50	85.06	225.00	.54	5.00	85.06	225.00	.54
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6023E+01 EXCESS= .0000E+00 OUTFLOW= .6026E+01 BASIN STORAGE= .1052E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	2.00	73.22	224.00	.48	5.00	72.98	225.00	.48
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5307E+01 EXCESS= .0000E+00 OUTFLOW= .5309E+01 BASIN STORAGE= .1178E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	1.50	36.73	228.00	.25	5.00	36.39	230.00	.25
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2843E+01 EXCESS= .0000E+00 OUTFLOW= .2844E+01 BASIN STORAGE= .9708E-03 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	1.50	13.72	234.00	.11	5.00	13.69	235.00	.11
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1250E+01 EXCESS= .0000E+00 OUTFLOW= .1252E+01 BASIN STORAGE= .9799E-03 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RC3B1B	MANE	3.50	.84	315.00	.00	5.00	.84	315.00	.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5537E-01 EXCESS= .0000E+00 OUTFLOW= .5543E-01 BASIN STORAGE= .1150E-02 PERCENT ERROR= -2.2									
FOR PLAN = 1	RATIO=	.00							
RCP49	MANE	1.05	10924.50	236.50	1.10	5.00	10681.43	235.00	1.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2140E+04 EXCESS= .0000E+00 OUTFLOW= .2138E+04 BASIN STORAGE= .2488E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 1.10 9604.29 236.78 .98 5.00 9463.34 240.00 .98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1907E+04 EXCESS= .0000E+00 OUTFLOW= .1905E+04 BASIN STORAGE= .2420E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 1.14 8689.84 240.86 .90 5.00 8676.68 240.00 .90

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1758E+04 EXCESS= .0000E+00 OUTFLOW= .1756E+04 BASIN STORAGE= .2347E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 1.16 8204.33 240.93 .86 5.00 8133.70 240.00 .87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1683E+04 EXCESS= .0000E+00 OUTFLOW= .1682E+04 BASIN STORAGE= .2281E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 1.19 7520.52 240.96 .81 5.00 7386.80 240.00 .81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1581E+04 EXCESS= .0000E+00 OUTFLOW= .1580E+04 BASIN STORAGE= .2187E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 1.24 6795.19 241.16 .76 5.00 6542.10 240.00 .76

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1473E+04 EXCESS= .0000E+00 OUTFLOW= .1471E+04 BASIN STORAGE= .2072E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 1.48 4048.59 246.83 .53 5.00 3958.97 250.00 .53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1031E+04 EXCESS= .0000E+00 OUTFLOW= .1030E+04 BASIN STORAGE= .1183E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 1.79 2264.36 258.15 .32 5.00 2151.44 260.00 .32

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6278E+03 EXCESS= .0000E+00 OUTFLOW= .6275E+03 BASIN STORAGE= .5500E+00 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCP49 MANE 2.82 591.74 287.95 .09 5.00 564.09 290.00 .09

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1675E+03 EXCESS= .0000E+00 OUTFLOW= .1675E+03 BASIN STORAGE= .4394E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 3.50 804.87 227.50 1.89 5.00 773.72 230.00 1.89

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4726E+02 EXCESS= .0000E+00 OUTFLOW= .4742E+02 BASIN STORAGE= .6566E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 3.50 722.08 227.50 1.69 5.00 701.84 230.00 1.69

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4222E+02 EXCESS= .0000E+00 OUTFLOW= .4236E+02 BASIN STORAGE= .6370E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 3.75 678.64 228.75 1.55 5.00 660.81 230.00 1.55

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3882E+02 EXCESS= .0000E+00 OUTFLOW= .3895E+02 BASIN STORAGE= .7137E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 4.25 627.72 229.50 1.47 5.00 621.68 230.00 1.47

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3670E+02 EXCESS= .0000E+00 OUTFLOW= .3684E+02 BASIN STORAGE= .7694E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 4.50 573.63 229.50 1.36 5.00 570.74 230.00 1.37

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3402E+02 EXCESS= .0000E+00 OUTFLOW= .3418E+02 BASIN STORAGE= .6059E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 4.50 524.49 229.50 1.25 5.00 523.41 230.00 1.26

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3128E+02 EXCESS= .0000E+00 OUTFLOW= .3142E+02 BASIN STORAGE= .5931E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 3.50 373.15 234.50 .84 5.00 364.59 235.00 .84

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2110E+02 EXCESS= .0000E+00 OUTFLOW= .2120E+02 BASIN STORAGE= .5443E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 4.00 239.20 236.00 .53 5.00 235.18 235.00 .53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1315E+02 EXCESS= .0000E+00 OUTFLOW= .1325E+02 BASIN STORAGE= .6046E-02 PERCENT ERROR= -.8

FOR PLAN = 1 RATIO= .00
RC3A2A MANE 1.50 119.69 244.50 .17 5.00 99.68 245.00 .19

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4184E+01 EXCESS= .0000E+00 OUTFLOW= .4282E+01 BASIN STORAGE= .6642E-02 PERCENT ERROR= -2.5

FOR PLAN = 1 RATIO= .00
RCP50 MANE 1.94 1418.95 213.12 1.53 5.00 1369.00 215.00 1.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1216E+03 EXCESS= .0000E+00 OUTFLOW= .1216E+03 BASIN STORAGE= .4174E-02 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	2.04	1251.03	212.32	1.35	5.00	1190.71	215.00	1.35
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1073E+03 EXCESS= .0000E+00 OUTFLOW= .1073E+03 BASIN STORAGE= .3932E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	2.12	1129.62	212.44	1.23	5.00	1070.95	215.00	1.23
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9754E+02 EXCESS= .0000E+00 OUTFLOW= .9755E+02 BASIN STORAGE= .3936E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	2.18	1052.46	213.18	1.16	5.00	1004.32	215.00	1.16
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9188E+02 EXCESS= .0000E+00 OUTFLOW= .9190E+02 BASIN STORAGE= .4255E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	2.26	972.80	212.21	1.06	5.00	912.93	215.00	1.06
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8443E+02 EXCESS= .0000E+00 OUTFLOW= .8445E+02 BASIN STORAGE= .4850E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	2.35	852.03	211.63	.97	5.00	818.02	215.00	.97
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7669E+02 EXCESS= .0000E+00 OUTFLOW= .7670E+02 BASIN STORAGE= .4331E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	2.87	522.32	212.48	.61	5.00	513.75	215.00	.61
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4865E+02 EXCESS= .0000E+00 OUTFLOW= .4866E+02 BASIN STORAGE= .4378E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	3.59	296.28	237.24	.35	5.00	292.15	240.00	.35
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2814E+02 EXCESS= .0000E+00 OUTFLOW= .2817E+02 BASIN STORAGE= .4680E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RCP50	MANE	1.75	129.02	250.25	.09	5.00	121.72	250.00	.10
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7453E+01 EXCESS= .0000E+00 OUTFLOW= .7474E+01 BASIN STORAGE= .4798E-02 PERCENT ERROR= -.3									

*** 2 ERROR(S) DETECTED BY HEC-1 ***

POST-PROJECT: HEC-1 OUTPUT
MISSIOND.OUT

```

1 *****
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUL 1997
* VERSION 4.1
* RUN DATE 02FEB06 TIME 16:45:31
*****

MISSIOND.OUT
*****
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*****

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X X XXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXX XXXX X XXXX X
X X X X X
X X X X X
X X XXXXXX XXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
*** FREE ***
1 ID MISSION LOMR FEMA HYDROLOGY
2 ID
3 ID POST-DEVELOPMENT CONDITIONS DRAINAGE SYSTEM SDN3
4 ID
5 ID INPUT FILE = MISSIOND.DAT
6 ID INPUT FILE DATE = 02/02/06
7 ID DESIGN STORM = 100-YEAR 6-HR STORM
8 ID STORM DISTRIBUTION = SDN #3
9 ID MODELED BY : VTN NEVADA
10 ID
11 ID
12 ID REFERENCED HYDROLOGIC MODELS:
13 ID C-1 WATERSHED FIS RESTUDY (CARTER BURGESS AND SOUTHWEST FLUVIAL SYSTEMS 2002)
14 ID PREDESIGN REPORT FOR THE BLACK MOUNTAIN AND MISSION HILLS DETENTION BASINS
15 ID AND OUTFALL STRUCTURES (VTN 1992)
16 ID SNWA RIVER MOUNTAINS WATER TREATMENT FACILITY DRAFT TECHNICAL DRAINAGE STUDY
17 ID (MONTGOMERY WATSON/CH2MHILL 1997)
18 ID EAST C-1 DETENTION BASIN FINAL DESIGN (VTN 1998)
19 ID DESIGN MEMORANDUM FOR THE EQUESTRIAN DETENTION BASIN (POGEMEYER 1994)
20 ID DESIGN CALCULATION NOTEBOOK FOR THE BLACK MOUNTAIN DETENTION BASIN
21 ID (VTN 1998)
22 ID CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2002 MASTER PLAN UPDATE (LBA)
23 ID 1-515 BOULDER HIGHWAY TO LAKE MEAD DRIVE DRAINAGE STUDY (SVERDRUP, 1991)
24 ID
25 ID JR CARDS CONTAINED DARFS BASED ON THE FOLLOWING VALUES:
26 ID
27 ID AREA DARF
28 ID SQ.MI.
29 ID
30 ID 0.0 - 0.2 0.992
31 ID 0.2 - 0.4 0.984
32 ID 0.4 - 0.6 0.978
33 ID 0.6 - 0.8 0.974
34 ID 0.8 - 1.0 0.970
35 ID 1.0 - 1.2 0.962
36 ID 1.2 - 1.4 0.954
37 ID 1.4 - 1.5 0.950
38 ID
39 ID
40 ID
41 ID
42 ID
43 ID
44 ID
45 IT 5 0 0 300
46 IN 5 0 0
47 IO 5
48 JR PREC 0.992 0.984 0.978 0.974 0.970 0.962 0.954 0.950

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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
49 KK C1G2B1
50 KM PART OF 2001 MPU C1-10
51 KM CN,TAKEN FROM C-1 WATERSHED FIS RESTUDY
52 KM BY (CARTER BURGESS AND SOUTHWEST FLUVIAL SYSTEMS 2002)
53 BA .3930
54 PB 3.17
55 PC .000 .020 .057 .070 .087 .108 .124 .130 .130 .130
56 PC .130 .130 .130 .133 .140 .142 .148 .158 .172 .181
57 PC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
58 PC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
59 PC .499 .590 .710 .744 .781 .812 .819 .835 .851 .856
60 PC .860 .868 .876 .888 .910 .926 .937 .950 .970 .976
61 PC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
62 PC .998 .999 1.00
63 LS 0 74
64 UD .376
*
65 KK RG2B1
66 KM ROUTE C1G2B1 TO C1G2B2
67 KM NO FACILITY - OVERLAND FLOW
68 RD 4400 .028 .030 0 TRAP 200
*
69 KK C1G2A
70 KM PART OF 2001 MPU C1-11
71 KM AREA,CN,LAG TIME TAKEN FROM C-1 WATERSHED FIS RESTUDY
72 KM BY (CARTER BURGESS AND SOUTHWEST FLUVIAL SYSTEMS 2002)
73 BA .3468
74 PB 3.17
75 LS 0 79
76 UD 0.22
*
77 KK RC1G2A

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MISSIOND.OUT

78	KM	ROUTE C1G2A TO CP7C							
79	KM	NDOT FACILITY @US95							
80	RD	3800 .018 .030	0	TRAP	100				
	*								
81	KK	CP7A							
82	KM	COMBINE C1G2A AND C1G2B1							
83	KM	GREENWAY AT US95							
84	HC	2							
	*								
85	KK	C1G2B2							
86	KM	PART OF 2001 MPU C1-12							
87	KM	SUBBASIN SPLIT INTO 4 SECTIONS TO MODEL TOPO							
88	BA	.1611							
89	PB	3.20							
90	LS	0 71.6							
91	UD	.270							
	*								

1 HEC-1 INPUT PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

92	KK	RG2B2							
93	KM	ROUTE C1G2B2 TO END							
94	KM	NO FACILITY - OVERLAND FLOW							
95	RD	4400 .028 .030	0	TRAP	200				
	*								
96	KK	CP7B							
97	KM	COMBINE C1G2B1 AND C1G2A							
98	KM	GREENWAY AT US95							
99	HC	2							
	*								
100	KK	C1G2B0							
101	KM	LOWER SECTION OF C1G2B1 TAKEN FROM C-1 WATERSHED FIS RESTUDY							
102	KM	BY (CARTER BURGESS AND SOUTHWEST FLUVIAL SYSTEMS 2002)							
103	KM	BEGINNING OF WASH							
104	BA	.1291							
105	PB	3.17							
106	LS	0 80							
107	UD	.133							
	*								
108	KK	RG2B0							
109	KM	ROUTE C1G2B0 TO C1G2B2							
110	KM	NO FACILITY - OVERLAND FLOW							
111	RD	4400 .028 .030	0	TRAP	200				
	*								
112	KK	C1G2B4							
113	KM	SPLIT SECTION OF C1G2B2							
114	KM	BEGINNING OF WASH							
115	BA	.031							
116	PB	3.17							
117	LS	0 77							
118	UD	.151							
	*								
119	KK	CP1							
120	KM	COMBINE C1G2B0 AND C1G2B4							
121	HC	2							
	*								
122	KK	RG2B4							
123	KM	ROUTE C1G2B4 TO C1G2B3							
124	KM	NO FACILITY - OVERLAND FLOW							
125	RD	4400 .028 .030	0	TRAP	200				
	*								
126	KK	C1G2B3							
127	KM	SPLIT SECTION OF C1G2B2							
128	KM	BEGINNING OF WASH							
129	BA	.0635							
130	PB	3.17							
131	LS	0 75.2							

1 HEC-1 INPUT PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

132	UD	.193							
	*								
133	KK	CP2							
134	KM	COMBINE C1G2B0,C1G2B4 & C1G2B3							
135	HC	2							
	*								
136	KK	RG2B3							
137	KM	ROUTE C1G2B3 TO C1G2B5							
138	KM	NO FACILITY - OVERLAND FLOW							
139	RD	4400 .028 .030	0	TRAP	200				
	*								
140	KK	C1G2B5							
141	KM	SPLIT SECTION OF C1G2B2							
142	KM	END OF WASH							
143	BA	.0209							
144	PB	3.17							
145	LS	0 77							
146	UD	.131							
	*								
147	KK	CP3							
148	KM	COMBINE C1G2B0,C1G2B4,C1G2B3 & C1G2B5							
149	HC	2							
	*								
150	KK	CP7C							
151	KM	COMBINE C1G2B0 AND C1G2B2							
152	KM	COLLEGE AT US95							
153	KM	END OF WASH							
154	HC	2							
	*								
155	ZZ								

1 SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

49 C1G2B1
V

65 RG2B1
V

MISSIOND.OUT

```

69      .      C1G2A
      .      V
77      .      RC1G2A
      .
81      CP7A.....
      .
85      .      C1G2B2
      .      V
92      .      RG2B2
      .
96      CP7B.....
      .
100     .      C1G2B0
      .      V
108     .      RG2B0
      .
112     .      C1G2B4
      .
119     .      CP1.....
      .      V
122     .      RG2B4
      .
126     .      C1G2B3
      .
133     .      CP2.....
      .      V
136     .      RG2B3
      .
140     .      C1G2B5
      .
147     .      CP3.....
      .
150     CP7C.....

```

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1 *****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUL 1997
* VERSION 4.1
* RUN DATE 02FEB06 TIME 16:45:31
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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MISSION LOMR FEMA HYDROLOGY

POST-DEVELOPMENT CONDITIONS DRAINAGE SYSTEM SDN3

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INPUT FILE = MISSIOND.DAT
INPUT FILE DATE = 02/02/06
DESIGN STORM = 100-YEAR 6-HR STORM
STORM DISTRIBUTION = SDN #3
MODELED BY : VTN NEVADA

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REFERENCED HYDROLOGIC MODELS:
C-1 WATERSHED FIS RESTUDY (CARTER BURGESS AND SOUTHWEST FLUVIAL SYSTEMS 2002
PREDESIGN REPORT FOR THE BLACK MOUNTAIN AND MISSION HILLS DETENTION BASINS
AND OUTFALL STRUCTURES (VTN 1992)
SNWA RIVER MOUNTAINS WATER TREATMENT FACILITY DRAFT TECHNICAL DRAINAGE STUDY
(MONTGOMERY WATSON/CH2MHILL 1997)
EAST C-1 DETENTION BASIN FINAL DESIGN (VTN 1998)
DESIGN MEMORANDUM FOR THE EQUESTRIAN DETENTION BASIN (POGGEMEYER 1994)
DESIGN CALCULATION NOTEBOOK FOR THE BLACK MOUNTAIN DETENTION BASIN
(VTN 1998)
CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2002 MASTER PLAN UPDATE (LBA)
1-515 BOULDER HIGHWAY TO LAKE MEAD DRIVE DRAINAGE STUDY (SVERDRUP, 1991)

```

JR CARDS CONTAINED DARFS BASED ON THE FOLLOWING VALUES:

AREA SQ.MI.	DARF
0.0 - 0.2	0.992
0.2 - 0.4	0.984
0.4 - 0.6	0.978
0.6 - 0.8	0.974
0.8 - 1.0	0.970
1.0 - 1.2	0.962
1.2 - 1.4	0.954
1.4 - 1.5	0.950

```

47 IO      OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

IT         HYDROGRAPH TIME DATA
      NMIN      5 MINUTES IN COMPUTATION INTERVAL
      IDATE      1 0 STARTING DATE
      ITIME      0000 STARTING TIME
      NQ         300 NUMBER OF HYDROGRAPH ORDINATES
      NDATE      0 ENDING DATE
      NDTIME      0055 ENDING TIME
      ICENT      19 CENTURY MARK

      COMPUTATION INTERVAL .08 HOURS
      TOTAL TIME BASE 24.92 HOURS

```


ENGLISH UNITS
 DRAINAGE AREA
 PRECIPITATION DEPTH
 LENGTH, ELEVATION
 FLOW
 STORAGE VOLUME
 SURFACE AREA
 TEMPERATURE

SQUARE MILES
 INCHES
 FEET
 CUBIC FEET PER SECOND
 ACRE-Feet
 ACRES
 DEGREES FAHRENHEIT

MISSIOND.OUT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION .99 .98 .97 .97 .96 .95 .95

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION							
				RATIO 1 .99	RATIO 2 .98	RATIO 3 .98	RATIO 4 .97	RATIO 5 .97	RATIO 6 .96	RATIO 7 .95	RATIO 8 .95
HYDROGRAPH AT +	C1G2B1	.39	1 FLOW TIME	228. 3.83	224. 3.83	221. 3.83	219. 3.83	217. 3.83	213. 3.83	210. 3.83	208. 3.83
ROUTED TO +	RG2B1	.39	1 FLOW TIME	231. 4.08	228. 4.08	225. 4.08	223. 4.08	222. 4.08	211. 4.08	207. 4.08	205. 4.08
HYDROGRAPH AT +	C1G2A	.35	1 FLOW TIME	334. 3.67	329. 3.67	325. 3.67	323. 3.67	320. 3.67	316. 3.67	311. 3.67	309. 3.67
ROUTED TO +	RC1G2A	.35	1 FLOW TIME	331. 3.83	327. 3.83	323. 3.83	311. 3.83	308. 3.83	304. 3.83	310. 3.83	308. 3.83
2 COMBINED AT +	CP7A	.74	1 FLOW TIME	501. 3.92	494. 3.92	488. 3.92	483. 3.92	480. 3.92	457. 3.92	451. 3.92	447. 3.92
HYDROGRAPH AT +	C1G2B2	.16	1 FLOW TIME	97. 3.75	95. 3.75	94. 3.75	93. 3.75	92. 3.75	90. 3.75	89. 3.75	88. 3.75
ROUTED TO +	RG2B2	.16	1 FLOW TIME	115. 4.00	111. 4.00	113. 4.00	114. 4.00	115. 4.00	99. 4.00	98. 4.00	98. 4.00
2 COMBINED AT +	CP7B	.90	1 FLOW TIME	575. 4.00	564. 4.00	560. 4.00	558. 4.00	556. 4.00	533. 4.00	526. 4.00	522. 4.00
HYDROGRAPH AT +	C1G2B0	.13	1 FLOW TIME	157. 3.58	155. 3.58	153. 3.58	152. 3.58	151. 3.58	149. 3.58	147. 3.58	145. 3.58
ROUTED TO +	RG2B0	.13	1 FLOW TIME	149. 3.83	147. 3.83	146. 3.83	145. 3.83	145. 3.83	143. 3.83	142. 3.83	141. 3.83
HYDROGRAPH AT +	C1G2B4	.03	1 FLOW TIME	31. 3.58	31. 3.58	31. 3.58	30. 3.58	30. 3.58	30. 3.58	29. 3.58	29. 3.58
2 COMBINED AT +	CP1	.16	1 FLOW TIME	166. 3.83	164. 3.83	163. 3.83	162. 3.83	161. 3.83	159. 3.83	158. 3.83	157. 3.83
ROUTED TO +	RG2B4	.16	1 FLOW TIME	192. 4.08	186. 4.08	181. 4.08	178. 4.08	175. 4.08	175. 4.17	176. 4.17	176. 4.17
HYDROGRAPH AT +	C1G2B3	.06	1 FLOW TIME	52. 3.67	51. 3.67	51. 3.67	50. 3.67	50. 3.67	49. 3.67	48. 3.67	48. 3.67
2 COMBINED AT +	CP2	.22	1 FLOW TIME	210. 4.08	204. 4.08	199. 4.08	195. 4.08	192. 4.08	189. 4.17	189. 4.17	189. 4.17
ROUTED TO +	RG2B3	.22	1 FLOW TIME	210. 4.42	213. 4.42	216. 4.42	217. 4.42	217. 4.42	216. 4.42	214. 4.42	212. 4.42
HYDROGRAPH AT +	C1G2B5	.02	1 FLOW TIME	22. 3.58	22. 3.58	22. 3.58	21. 3.58	21. 3.58	21. 3.58	21. 3.58	20. 3.58
2 COMBINED AT +	CP3	.24	1 FLOW TIME	213. 4.42	216. 4.42	219. 4.42	219. 4.42	219. 4.42	219. 4.42	216. 4.42	215. 4.42
2 COMBINED AT +	CP7C	1.15	1 FLOW TIME	643. 4.00	631. 4.00	633. 4.00	630. 4.00	627. 4.00	602. 4.00	593. 4.00	589. 4.00

*** NORMAL END OF HEC-1 ***

APPENDIX D

HYDRAULICS

**WSPG MODEL FOR MISSION DRIVE/GREENWAY RD
IMPROVEMENTS**

VTN3.OUT

(WSPG RUN FROM MISSION DRIVE/GREENWAY ROAD
IMPROVEMENTS FINAL DRAINAGE REPORT FEBRUARY 2004)

T1 MISSION DRIVE ROADWAY DESIGN
T2 MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN) 400CFS IN EX. CHANN.
T3 WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

SO	574.00	2303.54	16		.035					
R	674.00	2305.64	16		.035					
R	774.00	2307.74	16		.035					
JX	834.00	2309.00	14	1	.013	400.0		2309.00		10.00
R	868.47	2309.80	14		.013					
R	902.94	2310.61	14		.013					
R	979.63	2312.39	14		.013					
R	1056.31	2314.18	14		.013				100.00	
TS	1081.31	2314.76	15		.015					
R	1453.67	2318.49	15		.015					
TS	1478.67	2318.74	13		.015					
TS	1488.67	2318.84	12		.015					
JX	1498.67	2318.94	3	10	.015	24.0		2318.94		0.1
R	1656.18	2320.51	3		.013				100.00	
R	2116.18	2325.12	3		.013					
JX	2119.68	2325.15	3	7	.013	25.4		2326.38		45.00
R	2130.51	2325.26	3		.013					
R	2318.25	2331.23	3		.013				120.00	
R	2704.00	2343.53	3		.013					
R	2804.00	2347.74	3		.013					
R	2825.15	2348.12	3		.013					
JX	2830.15	2348.21	3	7	.013	85.8		2348.21		90.00
R	2890.01	2349.28	3		.013					
JX	2892.01	2349.32	3	6	.013	14.3		2352.92		45.00
R	3138.08	2353.72	3		.013					
JX	3144.08	2353.83	3	6	.013	22.3		2357.83		75.00
R	3467.42	2359.63	3		.013					
JX	3473.42	2359.93	4	8	.013	98.3		2367.92		90.00
R	3558.73	2363.44	4		.013					
JX	3563.73	2363.65	4	10	.013	29.7		2374.12		45.00
R	3785.46	2372.79	4		.013					
R	3809.00	2373.76	4		.013					
R	4122.26	2375.72	4		.013					
JX	4126.26	2375.82	9	7	.013	42.2		2375.82		45.00
R	4454.00	2383.78	9		.013					
R	4719.59	2388.89	9		.013					
R	4860.42	2393.31	9		.013				40.00	80.00
JX	4864.42	2394.31	8	8	.013	31.0	31.0	2394.31	2394.31	35.00
R	5267.87	2403.84	8		.013					
R	5667.87	2412.70	8		.013					
JX	5671.87	2414.20	10	10	.013	152.2		2414.20		45.00
R	5998.89	2422.58	10		.013					
JX	6002.89	2423.08	6	6	.013	50.5		2423.08		40.00
R	6329.90	2429.66	6		.013					
SH			6		.013			2434.66		
CD	1	1		5.0		18.0	2.0	2.0		
CD	2	3		6.0		7.0				
CD	3	3		6.0		6.0				
CD	4	4		5.5						
CD	5	4		3.0						
CD	6	4		2.0						
CD	7	4		3.5						
CD	8	4		4.0						
CD	9	4		5.0						

DATE: 2/ 5/2004
TIME: 14:53

F0515P
WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

PAGE 1

CARD CODE	SECT NO	CHN TYPE	NO OF PIERS	AVE PIER WIDTH	HEIGHT 1 DIAMETER	BASE WIDTH	ZL	ZR	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	1	0	0.00	5.00	18.00	2.00	2.00	0.00										
CD	2	3	0	0.00	6.00	7.00	0.00	0.00	0.00										
CD	3	3	0	0.00	6.00	6.00	0.00	0.00	0.00										
CD	4	4			5.50														
CD	5	4			3.00														
CD	6	4			2.00														
CD	7	4			3.50														
CD	8	4			4.00														
CD	9	4			5.00														
CD	10	4			2.50														
CD	11	3	0	0.00	6.00	10.00	0.00	0.00	0.00										
CD	12	2	0	0.00	11.00	10.00													
CD	13	2	0	0.00	11.00	8.00													
CD	14	3	0	0.00	6.00	8.00	0.00	0.00	0.00										
CD	15	2	0	0.00	6.00	8.00													
CD	16	1	0	0.00	5.00	37.00	2.00	2.00	0.00										
F 0 5 1 5 P																			

PAGE NO 3

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS -

MISSION DRIVE ROADWAY DESIGN

HEADING LINE NO 2 IS -

MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C

HEADING LINE NO 3 IS -

WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04
F 0 5 1 5 P

PAGE NO 2

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	1 IS	A	SYSTEM OUTLET	STATION	INVERT	SECT	W S ELEV												
			U/S DATA	574.00	2303.54	16	0.00												
ELEMENT NO	2 IS	A	REACH	STATION	INVERT	SECT		N											
			U/S DATA	674.00	2305.64	16		0.035											
ELEMENT NO	3 IS	A	REACH	STATION	INVERT	SECT		N											
			U/S DATA	774.00	2307.74	16		0.035											
ELEMENT NO	4 IS	A	JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4				
			U/S DATA	834.00	2309.00	14	1	0	0.013	400.0	0.0	2309.00	0.00	10.00	0.00				
ELEMENT NO	5 IS	A	REACH	STATION	INVERT	SECT			N										
			U/S DATA	868.47	2309.80	14			0.013										
ELEMENT NO	6 IS	A	REACH	STATION	INVERT	SECT			N										
			U/S DATA	902.94	2310.61	14			0.013										
ELEMENT NO	7 IS	A	REACH	STATION	INVERT	SECT			N										
			U/S DATA	979.63	2312.39	14			0.013										
ELEMENT NO	8 IS	A	REACH	STATION	INVERT	SECT			N										
			U/S DATA	1056.31	2314.18	14			0.013										
ELEMENT NO	9 IS	A	TRANSITION	STATION	INVERT	SECT			N										
			U/S DATA	1081.31	2314.76	15			0.015										
ELEMENT NO	10 IS	A	REACH	STATION	INVERT	SECT			N										
			U/S DATA	1453.67	2318.49	15			0.015										
ELEMENT NO	11 IS	A	TRANSITION	STATION	INVERT	SECT			N										
			U/S DATA	1478.67	2318.74	13			0.015										
ELEMENT NO	12 IS	A	TRANSITION	STATION	INVERT	SECT			N										
			U/S DATA	1488.67	2318.84	12			0.015										
ELEMENT NO	13 IS	A	JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4				
			U/S DATA	1498.67	2318.94	3	10	0	0.015	24.0	0.0	2318.94	0.00	0.10	0.000				
F 0 5 1 5 P																			

PAGE NO 3

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	14 IS	A	REACH	STATION	INVERT	SECT		N											
			U/S DATA	1656.18	2320.51	3		0.013											
ELEMENT NO	15 IS	A	REACH	STATION	INVERT	SECT		N											
			U/S DATA	2116.18	2325.12	3		0.013											

Page 1

VTN3.OUT

ELEMENT NO	16	IS	A	JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
				U/S DATA	2119.68	2325.15	3	7	0	0.013	25.4	0.0	2326.38	0.00	45.00	0.00
ELEMENT NO	17	IS	A	REACH	STATION	INVERT	SECT			N				RADIUS	ANGLE	ANG PT
				U/S DATA	2130.51	2325.26	3			0.013				0.00	0.00	0.00
ELEMENT NO	18	IS	A	REACH	STATION	INVERT	SECT			N				RADIUS	ANGLE	ANG PT
				U/S DATA	2318.25	2331.23	3			0.013				120.00	0.00	0.00
ELEMENT NO	19	IS	A	REACH	STATION	INVERT	SECT			N				RADIUS	ANGLE	ANG PT
				U/S DATA	2704.00	2343.53	3			0.013				0.00	0.00	0.00
ELEMENT NO	20	IS	A	REACH	STATION	INVERT	SECT			N				RADIUS	ANGLE	ANG PT
				U/S DATA	2804.00	2347.74	3			0.013				0.00	0.00	0.00
ELEMENT NO	21	IS	A	REACH	STATION	INVERT	SECT			N				RADIUS	ANGLE	ANG PT
				U/S DATA	2825.15	2348.12	3			0.013				0.00	0.00	0.00
ELEMENT NO	22	IS	A	JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
				U/S DATA	2830.15	2348.21	3	7	0	0.013	85.8	0.0	2348.21	0.00	90.00	0.00
ELEMENT NO	23	IS	A	REACH	STATION	INVERT	SECT			N				RADIUS	ANGLE	ANG PT
				U/S DATA	2890.01	2349.28	3			0.013				0.00	0.00	0.00
ELEMENT NO	24	IS	A	JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
				U/S DATA	2892.01	2349.32	3	6	0	0.013	14.3	0.0	2352.92	0.00	45.00	0.00

PAGE NO 4

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	25	IS	A REACH	STATION	INVERT	SECT						RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	3138.08	2353.72	3			N			0.00	0.00	0.00	1
ELEMENT NO	26	IS	A JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
			U/S DATA	3144.08	2353.83	3	6	0	0.013	22.3	0.0	2357.83	0.00	75.00	0.00
ELEMENT NO	27	IS	A REACH	STATION	INVERT	SECT						RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	3467.42	2359.63	3			N			0.00	0.00	0.00	1
ELEMENT NO	28	IS	A JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
			U/S DATA	3473.42	2359.93	4	8	0	0.013	98.3	0.0	2367.92	0.00	90.00	0.00
ELEMENT NO	29	IS	A REACH	STATION	INVERT	SECT						RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	3558.73	2363.44	4			N			0.00	0.00	0.00	1
ELEMENT NO	30	IS	A JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
			U/S DATA	3563.73	2363.65	4	10	0	0.013	29.7	0.0	2374.12	0.00	45.00	0.00
ELEMENT NO	31	IS	A REACH	STATION	INVERT	SECT						RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	3785.46	2372.79	4			N			0.00	0.00	0.00	0
ELEMENT NO	32	IS	A REACH	STATION	INVERT	SECT						RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	3809.00	2373.76	4			N			0.00	0.00	0.00	1
ELEMENT NO	33	IS	A REACH	STATION	INVERT	SECT						RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	4122.26	2375.72	4			N			0.00	0.00	0.00	1
ELEMENT NO	34	IS	A JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
			U/S DATA	4126.26	2375.82	9	7	0	0.013	42.2	0.0	2375.82	0.00	45.00	0.00

5

PAGE NO 5

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	35	IS	A REACH	STATION	INVERT	SECT							RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	4454.00	2383.78	9	N						0.00	0.00	0.00	0
							0.013									
ELEMENT NO	36	IS	A REACH	STATION	INVERT	SECT							RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	4719.59	2388.89	9	N						0.00	0.00	0.00	0
							0.013									
ELEMENT NO	37	IS	A REACH	STATION	INVERT	SECT							RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	4860.42	2393.31	9	N						40.00	80.00	0.00	1
							0.013									
ELEMENT NO	38	IS	A JUNCTION	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4	
			U/S DATA	4864.42	2394.31	8	8	8	0.013	31.0	31.0	2394.31	2394.31	35.00	35.00	
ELEMENT NO	39	IS	A REACH	STATION	INVERT	SECT							RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	5267.87	2403.84	8	N						0.00	0.00	0.00	0
							0.013									
ELEMENT NO	40	IS	A REACH	STATION	INVERT	SECT							RADIUS	ANGLE	ANG PT	MAN H
			U/S DATA	5667.87	2412.70	8	N						0.00	0.00	0.00	1
							0.013									

VTN3.OUT

ELEMENT NO 41 IS A JUNCTION
U/S DATA STATION 5671.87 INVERT 2414.20 SECT 10 LAT-1 10 LAT-2 0 N 0.013 Q3 152.2 Q4 0.0 INVERT-3 2414.20 INVERT-4 0.00 PHI 3 45.00 PHI 4 0.00

ELEMENT NO 42 IS A REACH
U/S DATA STATION 5998.89 INVERT 2422.58 SECT 10 N 0.013 RADIUS 0.00 ANGLE 0.00 ANG PT 0.00 MAN H 1

ELEMENT NO 43 IS A JUNCTION
U/S DATA STATION 6002.89 INVERT 2423.08 SECT 6 LAT-1 6 LAT-2 0 N 0.013 Q3 50.5 Q4 0.0 INVERT-3 2423.08 INVERT-4 0.00 PHI 3 40.00 PHI 4 0.00

ELEMENT NO 44 IS A REACH
U/S DATA STATION 6329.90 INVERT 2429.66 SECT 6 N 0.013 RADIUS 0.00 ANGLE 0.00 ANG PT 0.00 MAN H 0

ELEMENT NO 45 IS A SYSTEM HEADWORKS
U/S DATA STATION 6329.90 INVERT 2429.66 SECT 6 W S ELEV 2434.66

F 0 5 1 5 P

PAGE NO 6

WATER SURFACE PROFILE - ELEMENT CARD LISTING

NO EDIT ERRORS ENCOUNTERED-COMPUTATION IS NOW BEGINNING

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WATER SURFACE PROFILE LISTING

MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD.EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF			NORM DEPTH		ZR		
574.00	2303.54	2.424	2305.964	1030.1	10.15	1.601	2307.565	0.00	2.743	5.00	37.00	2.00	0	0.00
66.03	0.02100					.021000	1.39			2.424		2.00		
640.03	2304.93	2.424	2307.351	1030.1	10.15	1.601	2308.952	0.00	2.743	5.00	37.00	2.00	0	0.00
33.97	0.02100					.021881	0.74			2.424		2.00		
674.00	2305.64	2.367	2308.007	1030.1	10.43	1.688	2309.695	0.00	2.743	5.00	37.00	2.00	0	0.00
7.85	0.02100					.023254	0.18			2.424		2.00		
681.85	2305.80	2.338	2308.143	1030.1	10.57	1.735	2309.878	0.00	2.743	5.00	37.00	2.00	0	0.00
16.29	0.02100					.025618	0.42			2.424		2.00		
698.14	2306.15	2.240	2308.387	1030.1	11.09	1.908	2310.295	0.00	2.743	5.00	37.00	2.00	0	0.00
11.13	0.02100					.029664	0.33			2.424		2.00		
709.27	2306.38	2.146	2308.527	1030.1	11.63	2.099	2310.626	0.00	2.743	5.00	37.00	2.00	0	0.00
8.91	0.02100					.034362	0.31			2.424		2.00		
718.18	2306.57	2.055	2308.623	1030.1	12.19	2.309	2310.932	0.00	2.743	5.00	37.00	2.00	0	0.00
7.63	0.02100					.039818	0.30			2.424		2.00		
725.81	2306.73	1.968	2308.696	1030.1	12.79	2.540	2311.236	0.00	2.743	5.00	37.00	2.00	0	0.00
6.77	0.02100					.046157	0.31			2.424		2.00		
732.58	2306.87	1.884	2308.754	1030.1	13.41	2.794	2311.548	0.00	2.743	5.00	37.00	2.00	0	0.00
6.11	0.02100					.053523	0.33			2.424		2.00		
738.69	2307.00	1.803	2308.802	1030.1	14.07	3.073	2311.875	0.00	2.743	5.00	37.00	2.00	0	0.00
5.60	0.02100					.062087	0.35			2.424		2.00		
744.29	2307.12	1.726	2308.842	1030.1	14.76	3.381	2312.223	0.00	2.743	5.00	37.00	2.00	0	0.00
5.17	0.02100					.072045	0.37			2.424		2.00		

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WATER SURFACE PROFILE LISTING

MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD.EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF			NORM DEPTH		ZR		
749.46	2307.22	1.652	2308.877	1030.1	15.48	3.719	2312.596	0.00	2.743	5.00	37.00	2.00	0	0.00
4.80	0.02100					.083628	0.40			2.424		2.00		
754.26	2307.32	1.580	2308.905	1030.1	16.23	4.091	2312.996	0.00	2.743	5.00	37.00	2.00	0	0.00
4.47	0.02100					.097105	0.43			2.424		2.00		
758.73	2307.42	1.512	2308.931	1030.1	17.02	4.500	2313.431	0.00	2.743	5.00	37.00	2.00	0	0.00
4.19	0.02100					.112790	0.47			2.424		2.00		
762.92	2307.51	1.446	2308.953	1030.1	17.85	4.950	2313.903	0.00	2.743	5.00	37.00	2.00	0	0.00
3.93	0.02100					.131049	0.52			2.424		2.00		

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VTN3.OUT

766.85	2307.59	1.383	2308.973	1030.1	18.73	5.445	2314.418	0.00	2.743		5.00	37.00	2.00	0	0.00
3.68	0.02100					.152310	0.56			2.424			2.00		
770.53	2307.67	1.323	2308.990	1030.1	19.64	5.989	2314.979	0.00	2.743		5.00	37.00	2.00	0	0.00
3.47	0.02100					.177074	0.61			2.424			2.00		
774.00	2307.74	1.265	2309.005	1030.1	20.60	6.588	2315.593	0.00	2.743		5.00	37.00	2.00	0	0.00
JUNCT STR	0.02100					.021744	1.30						2.00		
834.00	2309.00	3.473	2312.473	630.1	22.68	7.986	2320.459	0.00	5.777		6.00	8.00	0.00	0	0.00
34.47	0.02321					.016811	0.58			3.113			0.00		
868.47	2309.80	3.536	2313.336	630.1	22.27	7.704	2321.040	0.00	5.777		6.00	8.00	0.00	0	0.00
34.47	0.02350					.015911	0.55			3.099			0.00		
902.94	2310.61	3.617	2314.227	630.1	21.77	7.361	2321.588	0.00	5.777		6.00	8.00	0.00	0	0.00
28.43	0.02321					.014984	0.43			3.113			0.00		
931.37	2311.27	3.697	2314.967	630.1	21.31	7.048	2322.015	0.00	5.777		6.00	8.00	0.00	0	0.00
48.26	0.02321					.013671	0.66			3.113			0.00		
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MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD. EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF		NORM DEPTH			ZR		
979.63	2312.39	3.877	2316.267	630.1	20.31	6.408	2322.675	0.00	5.777	6.00	8.00	0.00	0	0.00
28.37	0.02334					.012186	0.35		3.107			0.00		
1008.00	2313.05	4.026	2317.078	630.1	19.56	5.942	2323.020	0.00	5.777	6.00	8.00	0.00	0	0.00
27.58	0.02334					.010885	0.30		3.107			0.00		
1035.58	2313.70	4.223	2317.919	630.1	18.65	5.402	2323.321	0.00	5.777	6.00	8.00	0.00	0	0.00
20.73	0.02334					.009594	0.20		3.107			0.00		
1056.31	2314.18	4.429	2318.609	630.1	17.78	4.911	2323.520	0.00	5.777	6.00	8.00	0.00	0	0.00
TRANS STR	0.02320					.011200	0.28					0.00		
1081.31	2314.76	4.667	2319.427	630.1	16.87	4.422	2323.849	0.00	5.777	6.00	8.00	0.00	0	0.00
150.00	0.01002					.010802	1.62		4.740			0.00		
1231.31	2316.26	4.546	2320.809	630.1	17.33	4.661	2325.470	0.00	5.777	6.00	8.00	0.00	0	0.00
133.60	0.01002					.011922	1.59		4.740			0.00		
1364.91	2317.60	4.335	2321.936	630.1	18.17	5.127	2327.063	0.00	5.777	6.00	8.00	0.00	0	0.00
88.76	0.01002					.013521	1.20		4.740			0.00		
1453.67	2318.49	4.133	2322.623	630.1	19.06	5.640	2328.263	0.00	5.777	6.00	8.00	0.00	0	0.00
TRANS STR	0.01000					.014836	0.37					0.00		
1478.67	2318.74	4.037	2322.777	630.1	19.51	5.911	2328.688	0.00	5.777	11.00	8.00	0.00	0	0.00
TRANS STR	0.01000					.018660	0.19					0.00		
1488.67	2318.84	2.871	2321.711	630.1	21.94	7.478	2329.189	0.00	4.979	11.00	10.00	0.00	0	0.00
JUNCT STR	0.01000					.018299	0.18					0.00		
1498.67	2318.94	5.441	2324.381	606.1	18.57	5.352	2329.733	0.00	6.000	6.00	6.00	0.00	0	0.00
157.51	0.00997					.011567	1.82		5.652			0.00		
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MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD. EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF		NORM DEPTH			ZR		
1656.18	2320.51	5.212	2325.722	606.1	19.38	5.834	2331.556	0.00	6.000	6.00	6.00	0.00	0	0.00
111.94	0.01002					.012919	1.45		5.640			0.00		
1768.12	2321.63	4.979	2326.611	606.1	20.29	6.392	2333.003	0.00	6.000	6.00	6.00	0.00	0	0.00
90.56	0.01002					.014521	1.32		5.640			0.00		
1858.68	2322.54	4.747	2327.286	606.1	21.28	7.031	2334.317	0.00	6.000	6.00	6.00	0.00	0	0.00
75.94	0.01002					.016372	1.24		5.640			0.00		

1934.62	2323.30	4.526	2327.826	606.1	22.32	7.734	2335.560	0.00	6.000		6.00	6.00	0.00	0	0.00
66.60	0.01002					.018471	1.23			5.640			0.00		
2001.22	2323.97	4.316	2328.284	606.1	23.41	8.508	2336.792	0.00	6.000		6.00	6.00	0.00	0	0.00
60.00	0.01002					.020855	1.25			5.640			0.00		
2061.22	2324.57	4.115	2328.684	606.1	24.55	9.358	2338.042	0.00	6.000		6.00	6.00	0.00	0	0.00
54.96	0.01002					.023564	1.30			5.640			0.00		
2116.18	2325.12	3.923	2329.043	606.1	25.75	10.294	2339.337	0.00	6.000		6.00	6.00	0.00	0	0.00
JUNCT STR	0.00857					.027461	0.10						0.00		
2119.68	2325.15	3.542	2328.692	580.7	27.32	11.590	2340.282	0.00	6.000		6.00	6.00	0.00	0	0.00
10.83	0.01016					.030354	0.33			5.418			0.00		
2130.51	2325.26	3.504	2328.764	580.7	27.62	11.849	2340.613	0.00	6.000		6.00	6.00	0.00	0	0.00
187.74	0.03180					.030210	5.67			3.461			0.00		
2318.25	2331.23	3.556	2334.786	580.7	27.22	11.505	2346.291	0.00	6.000		6.00	6.00	0.00	0	0.00
195.94	0.03189					.028195	5.52			3.457			0.00		
2514.19	2337.48	3.697	2341.175	580.7	26.18	10.641	2351.816	0.00	6.000		6.00	6.00	0.00	0	0.00
117.88	0.03189					.025211	2.97			3.457			0.00		
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MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (w/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W. S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD. EL.	SUPER ELEV	CRITICAL DEPTH		HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF			NORM DEPTH			ZR		

2632.07	2341.24	3.878	2345.114	580.7	24.96	9.673	2354.787	0.00	6.000		6.00	6.00	0.00	0	0.00
71.93	0.03189					.022291	1.60			3.457			0.00		
2704.00	2343.53	4.067	2347.597	580.7	23.80	8.794	2356.391	0.00	6.000		6.00	6.00	0.00	0	0.00
19.95	0.04210					.020049	0.40			3.111			0.00		
2723.95	2344.37	4.208	2348.578	580.7	23.00	8.212	2356.790	0.00	6.000		6.00	6.00	0.00	0	0.00
22.53	0.04210					.018077	0.41			3.111			0.00		
2746.48	2345.32	4.414	2349.732	580.7	21.93	7.466	2357.198	0.00	6.000		6.00	6.00	0.00	0	0.00
17.76	0.04210					.016016	0.28			3.111			0.00		
2764.24	2346.07	4.629	2350.695	580.7	20.91	6.787	2357.482	0.00	6.000		6.00	6.00	0.00	0	0.00
14.01	0.04210					.014201	0.20			3.111			0.00		
2778.25	2346.66	4.855	2351.511	580.7	19.93	6.170	2357.681	0.00	6.000		6.00	6.00	0.00	0	0.00
10.99	0.04210					.012599	0.14			3.111			0.00		
2789.24	2347.12	5.092	2352.210	580.7	19.01	5.609	2357.819	0.00	6.000		6.00	6.00	0.00	0	0.00
8.45	0.04210					.011187	0.09			3.111			0.00		
2797.69	2347.47	5.341	2352.815	580.7	18.12	5.099	2357.914	0.00	6.000		6.00	6.00	0.00	0	0.00
6.31	0.04210					.009940	0.06			3.111			0.00		
2804.00	2347.74	5.601	2353.341	580.7	17.28	4.636	2357.977	0.00	6.000		6.00	6.00	0.00	0	0.00
8.09	0.01797					.009121	0.07			4.317			0.00		
2812.09	2347.89	5.720	2353.605	580.7	16.92	4.446	2358.051	0.00	6.000		6.00	6.00	0.00	0	0.00
13.06	0.01797					.010378	0.14			4.317			0.00		
2825.15	2348.12	6.000	2354.120	580.7	16.24	4.097	2358.217	0.00	6.000		6.00	6.00	0.00	0	0.00
JUNCT STR	0.01800					.010246	0.05						0.00		

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MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN) 400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD.E.L.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF							

2830.15	2348.21	8.204	2356.414	494.9	13.84	2.976	2359.390	0.00	5.958	6.00	6.00	0.00	0	0.00
59.86	0.01787					.008621	0.52		3.819			0.00		
2890.01	2349.28	7.650	2356.930	494.9	13.84	2.976	2359.906	0.00	5.958	6.00	6.00	0.00	0	0.00
JUNCT STR	0.02000					.008376	0.02					0.00		
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VTN3.OUT															
2892.01	2349.32	7.926	2357.246	480.6	13.44	2.806	2360.052	0.00	5.842		6.00	6.00	0.00	0	0.00
86.60	0.01788					.008130	0.70			3.733			0.00		
2978.61	2350.87	7.131	2358.000	480.6	13.44	2.806	2360.806	0.00	5.842		6.00	6.00	0.00	0	0.00
HYDRAULIC JUMP													0.00		
2978.61	2350.87	3.953	2354.822	480.6	20.26	6.375	2361.197	0.00	5.842		6.00	6.00	0.00	0	0.00
70.09	0.01788					.015051	1.05			3.733			0.00		
3048.70	2352.12	4.029	2356.151	480.6	19.88	6.137	2362.288	0.00	5.842		6.00	6.00	0.00	0	0.00
89.38	0.01788					.013839	1.24			3.733			0.00		
3138.08	2353.72	4.226	2357.946	480.6	18.96	5.579	2363.525	0.00	5.842		6.00	6.00	0.00	0	0.00
JUNCT STR 0.01833													0.00		
3144.08	2353.83	3.681	2357.511	458.3	20.75	6.686	2364.197	0.00	5.660		6.00	6.00	0.00	0	0.00
68.77	0.01794					.016663	1.15			3.595			0.00		
3212.85	2355.06	3.715	2358.779	458.3	20.56	6.564	2365.343	0.00	5.660		6.00	6.00	0.00	0	0.00
171.12	0.01794					.015510	2.65			3.595			0.00		
3383.97	2358.13	3.896	2362.029	458.3	19.60	5.968	2367.997	0.00	5.660		6.00	6.00	0.00	0	0.00
83.45	0.01794					.013716	1.14			3.595			0.00		
3467.42	2359.63	4.086	2363.716	458.3	18.69	5.425	2369.141	0.00	5.660		6.00	6.00	0.00	0	0.00
JUNCT STR 0.05000													0.00		
LICENSEE: VTN - NEVADA															

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MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD.EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF			NORM DEPTH		ZR		

3473.42	2359.93	3.209	2363.139	360.0	25.01	9.713	2372.852	0.00	5.064	5.50	0.00	0.00	0	0.00
47.80	0.04114					.026237	1.25			2.842		0.00		
3521.22	2361.90	3.331	2365.228	360.0	23.91	8.879	2374.107	0.00	5.064	5.50	0.00	0.00	0	0.00
37.51	0.04114					.023315	0.87			2.842		0.00		
3558.73	2363.44	3.469	2366.909	360.0	22.80	8.072	2374.981	0.00	5.064	5.50	0.00	0.00	0	0.00
JUNCT STR 0.04200													0.00	
3563.73	2363.65	2.948	2366.598	330.3	25.47	10.072	2376.670	0.00	4.933	5.50	0.00	0.00	0	0.00
20.47	0.04122					.030141	0.62			2.700		0.00		
3584.20	2364.49	2.979	2367.473	330.3	25.14	9.812	2377.285	0.00	4.933	5.50	0.00	0.00	0	0.00
58.09	0.04122					.027881	1.62			2.700		0.00		
3642.29	2366.89	3.096	2369.984	330.3	23.97	8.919	2378.903	0.00	4.933	5.50	0.00	0.00	0	0.00
41.39	0.04122					.024625	1.02			2.700		0.00		
3683.68	2368.59	3.220	2371.814	330.3	22.85	8.109	2379.923	0.00	4.933	5.50	0.00	0.00	0	0.00
31.17	0.04122					.021777	0.68			2.700		0.00		
3714.85	2369.88	3.351	2373.230	330.3	21.79	7.371	2380.601	0.00	4.933	5.50	0.00	0.00	0	0.00
24.21	0.04122					.019287	0.47			2.700		0.00		
3739.06	2370.88	3.490	2374.368	330.3	20.77	6.701	2381.069	0.00	4.933	5.50	0.00	0.00	0	0.00
19.17	0.04122					.017108	0.33			2.700		0.00		
3758.23	2371.67	3.637	2375.305	330.3	19.81	6.092	2381.397	0.00	4.933	5.50	0.00	0.00	0	0.00
15.22	0.04122					.015208	0.23			2.700		0.00		
3773.45	2372.30	3.795	2376.090	330.3	18.89	5.538	2381.628	0.00	4.933	5.50	0.00	0.00	0	0.00
12.01	0.04122					.013558	0.16			2.700		0.00		
LICENSEE: VTN - NEVADA														

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MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD.EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF			NORM DEPTH		ZR		

3785.46	2372.79	3.966	2376.756	330.3	18.01	5.034	2381.790	0.00	4.933	5.50	0.00	0.00	0	0.00
2.59	0.04121					.012615	0.03			2.700		0.00		

VTN3.OUT														
3788.05	2372.90	4.011	2376.908	330.3	17.79	4.916	2381.824	0.00	4.933		5.50	0.00	0.00	0 0.00
8.77	0.04121					.011801	0.10			2.700			0.00	
3796.82	2373.26	4.200	2377.458	330.3	16.96	4.469	2381.927	0.00	4.933		5.50	0.00	0.00	0 0.00
6.42	0.04121					.010621	0.07			2.700			0.00	
3803.24	2373.52	4.410	2377.932	330.3	16.18	4.063	2381.995	0.00	4.933		5.50	0.00	0.00	0 0.00
4.19	0.04121					.009635	0.04			2.700			0.00	
3807.43	2373.70	4.647	2378.342	330.3	15.42	3.693	2382.035	0.00	4.933		5.50	0.00	0.00	0 0.00
1.57	0.04121					.008866	0.01			2.700			0.00	
3809.00	2373.76	4.933	2378.693	330.3	14.70	3.357	2382.050	0.00	4.933		5.50	0.00	0.00	0 0.00
45.17	0.00626					.008536	0.39			5.500			0.00	
3854.17	2374.04	5.341	2379.384	330.3	14.02	3.051	2382.435	0.00	4.933		5.50	0.00	0.00	0 0.00
38.93	0.00626					.009047	0.35			5.500			0.00	
3893.10	2374.29	5.500	2379.786	330.3	13.90	3.001	2382.787	0.00	4.933		5.50	0.00	0.00	0 0.00
229.16	0.00626					.009619	2.20			5.500			0.00	
4122.26	2375.72	6.393	2382.113	330.3	13.90	3.001	2385.114	0.00	4.933		5.50	0.00	0.00	0 0.00
JUNCT STR	0.02500												0.00	
4126.26	2375.82	3.151	2378.971	288.1	22.10	7.585	2386.556	0.00	4.623		5.00	0.00	0.00	0 0.00
168.67	0.02429					.022810	3.85			3.111			0.00	
4294.93	2379.92	3.206	2383.123	288.1	21.66	7.283	2390.406	0.00	4.623		5.00	0.00	0.00	0 0.00
159.07	0.02429					.020988	3.34			3.111			0.00	
LICENSEE: VTN - NEVADA						F0515P								PAGE 9

MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD.EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF			NORM DEPTH		ZR		
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
4454.00	2383.78	3.343	2387.123	288.1	20.65	6.621	2393.744	0.00	4.623	5.00	0.00	0.00	0 0.00	
265.59	0.01924					.020608	5.47			3.375		0.00		
4719.59	2388.89	3.246	2392.136	288.1	21.35	7.081	2399.217	0.00	4.623	5.00	0.00	0.00	0 0.00	
36.16	0.03139					.020539	0.74			2.862		0.00		
4755.75	2390.03	3.351	2393.376	288.1	20.59	6.584	2399.960	0.00	4.623	5.00	0.00	0.00	0 0.00	
35.16	0.03139					.018543	0.65			2.862		0.00		
4790.91	2391.13	3.498	2394.626	288.1	19.63	5.986	2400.612	0.00	4.623	5.00	0.00	0.00	0 0.00	
25.95	0.03139					.016545	0.43			2.862		0.00		
4816.86	2391.94	3.657	2395.600	288.1	18.72	5.442	2401.042	0.00	4.623	5.00	0.00	0.00	0 0.00	
19.42	0.03139					.014819	0.29			2.862		0.00		
4836.28	2392.55	3.830	2396.382	288.1	17.85	4.946	2401.328	0.00	4.623	5.00	0.00	0.00	0 0.00	
14.28	0.03139					.013343	0.19			2.862		0.00		
4850.56	2393.00	4.022	2397.023	288.1	17.02	4.497	2401.520	0.00	4.623	5.00	0.00	0.00	0 0.00	
9.86	0.03139					.012113	0.12			2.862		0.00		
4860.42	2393.31	4.241	2397.551	288.1	16.23	4.088	2401.639	0.00	4.623	5.00	0.00	0.00	0 0.00	
JUNCT STR	0.25000					.017455	0.07					0.00		
4864.42	2394.31	3.399	2397.709	226.1	19.87	6.130	2403.839	0.00	3.904	4.00	0.00	0.00	0 0.00	
153.95	0.02362					.023185	3.57			3.372		0.00		
5018.37	2397.95	3.431	2401.378	226.1	19.71	6.031	2407.409	0.00	3.904	4.00	0.00	0.00	0 0.00	
249.50	0.02362					.022308	5.57			3.372		0.00		
5267.87	2403.84	3.652	2407.492	226.1	18.79	5.482	2412.974	0.00	3.904	4.00	0.00	0.00	0 0.00	
400.00	0.02215					.021805	8.72			3.540		0.00		
LICENSEE: VTN - NEVADA						F0515P								PAGE 10

MISSION DRIVE ROADWAY DESIGN
MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

STATION	INVERT ELEV	DEPTH OF FLOW	W.S. ELEV	Q	VEL	VEL HEAD	ENERGY GRD.EL.	SUPER ELEV	CRITICAL DEPTH	HGT/ DIA	BASE/ ID NO.	ZL	NO PIER	AVBPR
L/ELEM	SO					SF AVE	HF			NORM DEPTH		ZR		
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****

VTN3.OUT

5667.87	2412.70	3.904	2416.604	226.1	18.11	5.090	2421.694	0.00	3.904	4.00	0.00	0.00	0	0.00
JUNCT STR	0.37500											0.00		
5671.87	2414.20	2.452	2416.652	73.9	15.12	3.551	2420.203	0.00	2.452	2.50	0.00	0.00	0	0.00
3.31	0.02562					.030517	0.10			2.500		0.00		
5675.18	2414.28	2.500	2416.785	73.9	15.05	3.519	2420.304	0.00	2.452	2.50	0.00	0.00	0	0.00
323.71	0.02562					.032186	10.42			2.500		0.00		
5998.89	2422.58	4.887	2427.467	73.9	15.05	3.519	2430.986	0.00	2.452	2.50	0.00	0.00	0	0.00
JUNCT STR	0.12500					.021580	0.09					0.00		
6002.89	2423.08	7.131	2430.211	23.4	7.45	0.861	2431.072	0.00	1.718	2.00	0.00	0.00	0	0.00
327.01	0.02012					.010699	3.50					0.00		
6329.90	2429.66	4.050	2433.710	23.4	7.45	0.861	2434.571	0.00	1.718	2.00	0.00	0.00	0	0.00

MISSION DRIVE ROADWAY DESIGN
 MAINLINE DESIGN FOR 100 YEAR STORM EVENT (W/ REVISED BASIN)400CFS IN EX. C
 WSPG FILE: VTN3.DAT, BY: W.T., VTN, 02/05/04

574.00	.IWCX													R
601.54	.													.
629.08	.													.
656.62	. IWCX													R
684.16	. I XEH													R
711.70	. I XEH													R
739.24	. I WCX													R
766.78	. IWCX													R
794.32	. IWCEH													R
821.86	. IWCEH													R
849.40	. IWC X													R
876.94	. I X X													R
904.48	. I X X													R
932.02	. I X X													R
959.56	. I X HE													R
987.10	. I WCHE													R
1014.64	. IWCH E													R
1042.18	. IWCH E													R
1069.72	. IWCH E													R
1097.26	. IWCH E													JX
1124.80	. I W X E													R
1152.34	. I W X E													R
1179.88	. I W X E													R
1207.42	. I W X E													R
1234.96	. I W X E													R
1262.50	. I W X E													R
1290.04	. I W X E													R
1317.59	. I W X E													TX
1345.13	. I XH E													R
1372.67	. I W X E													R
1400.21	. I W X E													R
1427.75	.													.
1455.29	. I W X E													TX
1482.83	. I W C X													TX
1510.37	. I W C EH													JX
1537.91	. I W X E													R
1565.45	.													.
1592.99	.													.
1620.53	.													.
1648.07	.													.
1675.61	. I W X E													R
1703.15	.													.
1730.69	.													.
1758.23	.													.
1785.77	. I W X E													R
1813.31	.													.
1840.85	.													.
1868.39	. I W X E													R
1895.93	.													.
1923.47	.													.
1951.01	. I W X E													R
1978.55	.													.
2006.09	. I W X E													R
2033.63	.													.
2061.17	.													.
2088.71	. I W X E													R
2116.25	. I W X E													JX
2143.79	. I W X E													R
2171.33	. I W X E													R
2198.87	.													.
2226.41	.													.
2253.95	.													.
2281.49	.													.
2309.03	.													.
2336.57	. I W X E													R
2364.11	.													.
2391.65	.													.
2419.19	.													.
2446.73	.													.
2474.27	.													.
2501.81	.													.
2529.35	. I W X E													R
2556.89	.													.
2584.43	.													.
2611.97	.													.
2639.51	. I W X E													R
2667.05	.													.

VTN3.OUT

2694.59	I	W	X	E		R
2722.13	I	WX	E		R	
2749.68	I	WX	E		R	
2777.22	I	W	X	E	R	
2804.76	I	WX	E		R	
2832.30	I	X	E		R	
2859.84	I	WX	E		R	
2887.38	I	X	E		R	
2914.92	I	X	E		R	
2942.46	I	X	E		R	
2970.00	I	X	E		JX	
2997.54	I	X	W	E	R	
3025.08	I	XW	E		JX	
3052.62	I	XW	E		R	
3080.16	I	XW	E		R	
3107.70	I	WX	E		R	
3135.24	I	WX	E		R	
3162.78	I	WX	E		JX	
3190.32	I	WX	E		R	
3217.86	I	WX	E		R	
3245.40						
3272.94						
3300.48						
3328.02						
3355.56						
3383.10	I	WCH	E		R	
3410.64						
3438.18	I	W	X	E	JX	
3465.72	I	WCH	E		R	
3493.26	I	WX	E		R	
3520.80	I	WCH	E		JX	
3548.34	I	WX	E		R	
3575.88	I	WCH	E		R	
3603.42	I	W	X	E	R	
3630.96	I	W	X	E	R	
3658.50	I	WX	E		R	
3686.04	I	WX	E		R	
3713.58						
3741.12	I	WX	E		R	
3768.66	I	WX	E		R	
3796.20	I	WCH	E		R	
3823.74	I	WX	E		R	
3851.28	I	WCH	E		R	
3878.82	I	WCH	E		R	
3906.36	I	XH	E		R	
3933.90	I	WX	E		R	
3961.44	I	X	E		R	
3988.98	I	X	E		R	
4016.52	I	XH	E		R	
4044.06	I	CX	E		R	
4071.60						
4099.14	I	CX	E		JX	
4126.68	I	WX	E		R	
4154.22						
4181.77						
4209.31						
4236.85						
4264.39						
4291.93						
4319.47	I	WCH	E		R	
4347.01						
4374.55						
4402.09						
4429.63						
4457.17	I	WCH	E		R	
4484.71						
4512.25						
4539.79						
4567.33						
4594.87						
4622.41						
4649.95						
4677.49						
4705.03						
4732.57	I	WX	E		R	
4760.11	I	WX	E		R	
4787.65						
4815.19	I	WX	E		R	
4842.73	I	XH	E		R	
4870.27	I	WX	E		R	
4897.81	I	XH	E		R	
4925.35	I	WX	E		JX	
4952.89	I	WX	E		R	
4980.43						
5007.97						
5035.51	I	WX	E		R	
5063.05						
5090.59						
5118.13						
5145.67						
5173.21						
5200.75						
5228.29						
5255.83						
5283.37						
5310.91	I	X	E		R	
5338.45						
5365.99						
5393.53						
5421.07						
5448.61						
5476.15						
5503.69						
5531.23						
5558.77						
5586.31						

NOTES

1. GLOSSARY
I = INVERT ELEVATION
C = CRITICAL DEPTH
W = WATER SURFACE ELEVATION
H = HEIGHT OF CHANNEL
E = ENERGY GRADE LINE
X = CURVES CROSSING OVER
B = BRIDGE ENTRANCE OR EXIT
Y = WALL ENTRANCE OR EXIT
2. STATIONS FOR POINTS AT A JUMP MAY NOT BE PLOTTED EXACTLY

MISSION DRIVE/GREENWAY ROADWAY IMPROVEMENT

WSPG HYDRAULIC SUMMARY WITH 100YR FLOW CONDITION

WSPG STATION	SD PROFILE STATION	LENGTH IN WSPG (ft)	DESIGN FLOW (cfs)	INVERT ELEV (ft)	SLOPE (ft/ft)	DEPTH OF FLOW ⁽¹⁾ y*(ft)	DEPTH OF FLOW y(ft)	VELOCITY V(fps)	H.G.L. H(ft)	E.G.L. E(ft)	CHANNEL TYPE	BASE WIDTH b(ft)	Z	FROUDE NUMBER Fr	DESIGN WALL H.T. (ft)	FREEBOARD (ft)	COMMENTS
574.00			819.1	2303.54		2.119	2.119	9.37	2305.659	2307.02	EX. TRAP.	37	2	1.13	5	2.88	TEMP. RIPRAP
674.00	41+70.00	100.00	819.1	2305.64	0.021	2.101	2.101	9.46	2307.741	2309.13	EX. TRAP.	37	2	1.15	5	2.90	TEMP. RIPRAP
774.00	40+70.00	100.00	819.1	2307.74	0.021	1.124	0.982	21.40	2308.722	2315.83	EX. TRAP.	37	2	3.81	5	4.02	TEMP. RIPRAP
834.00	39+70.00	60.00	630.1	2309.00	0.021	3.590	3.473	22.68	2312.473	2320.46	RCB	8	0	2.14	6	2.53	OK
868.47	39+35.53	34.47	630.1	2309.80	0.023	3.642	3.536	22.27	2313.336	2321.04	RCB	8	0	2.09	6	2.46	OK
902.94	39+01.06	34.47	630.1	2310.61	0.023	3.710	3.617	21.77	2314.227	2321.59	RCB	8	0	2.02	6	2.38	OK
979.63	38+24.37	76.69	630.1	2312.39	0.023	3.928	3.877	20.31	2316.267	2322.67	RCB	8	0	1.82	6	2.12	OK
1056.31	37+47.69	76.68	630.1	2314.18	0.023	4.429	4.429	17.78	2318.609	2323.52	RCB	8	0	1.49	6	1.57	OK
1081.31	37+22.69	25.00	630.1	2314.76	0.023	4.667	4.667	16.87	2319.427	2323.85	RECT	8	0	1.38	6.5	1.83	REQ. FREEBOARD=1.70', OK
1453.67	33+50.33	372.36	630.1	2318.49	0.010	4.145	4.133	19.06	2322.623	2328.26	RECT	8	0	1.65	6.5	2.37	REQ. FREEBOARD=1.76', OK
1478.67	33+25.33	25.00	630.1	2318.74	0.010	4.063	4.037	19.51	2322.777	2328.69	RECT	8	0	1.71	11	6.96	OK
1488.67	33+15.33	10.00	630.1	2318.84	0.010	2.993	2.871	21.94	2321.711	2329.19	RECT	10	0	2.28	11	8.13	OK
1498.67	33+05.33	10.00	606.1	2318.94	0.010	5.441	5.441	18.57	2324.381	2329.74	RCB	6	0	1.40	6	0.56	OK
1656.18	31+47.82	157.51	606.1	2320.51	0.010	5.212	5.212	19.38	2325.722	2331.55	RCB	6	0	1.50	6	0.79	OK
2116.18	26+87.82	460.00	606.1	2325.12	0.010	4.092	3.923	25.75	2329.043	2339.34	RCB	6	0	2.29	6	2.08	OK
2119.68	26+84.32	3.50	580.7	2325.15	0.009	3.756	3.542	27.32	2328.692	2340.28	RCB	6	0	2.56	6	2.46	OK
2130.51	26+73.49	10.83	580.7	2325.26	0.010	3.725	3.504	27.62	2328.764	2340.61	RCB	6	0	2.60	6	2.50	OK
2318.25	24+85.75	187.74	580.7	2331.23	0.032	3.767	3.556	27.22	2334.786	2346.29	RCB	6	0	2.54	6	2.44	OK
2704.00	21+00.00	385.75	580.7	2343.53	0.032	4.187	4.067	23.80	2347.597	2356.39	RCB	6	0	2.08	6	1.93	OK
2804.00	20+00.00	100.00	580.7	2347.74	0.042	5.601	5.601	17.28	2353.341	2357.98	RCB	6	0	1.29	6	0.40	OK
2825.15	19+78.85	21.15	580.7	2348.12	0.018	6.000	6.000	16.24	2354.120	2358.22	RCB	6	0	1.17	6	0.00	OK
2830.15	19+73.85	5.00	494.9	2348.21	0.018	8.204	8.204	13.84	2356.414	2359.39	RCB	6	0	0.85	6	0.00	OK
2890.01	19+07.99	59.86	494.9	2349.28	0.018	7.650	7.650	13.84	2356.930	2359.90	RCB	6	0	0.88	6	0.00	OK
2892.01	19+05.99	2.00	480.6	2349.32	0.020	7.926	7.926	13.44	2357.246	2360.05	RCB	6	0	0.84	6	0.00	OK
2978.61	18+19.39	86.60	480.6	2350.87	0.018	7.131	7.131	13.44	2358.001	2360.81	RCB	6	0	0.89	6	0.00	OK
2978.61	18+19.39	0.00	480.6	2350.87	N/A	4.000	3.953	20.26	2354.823	2361.20	RCB	6	0	1.80	6	2.05	OK
3138.08	16+65.91	159.47	480.6	2353.72	0.018	4.231	4.226	18.96	2357.946	2363.53	RCB	6	0	1.63	6	1.77	OK
3144.08	16+59.91	6.00	458.3	2353.83	0.018	3.750	3.681	20.75	2357.511	2364.20	RCB	6	0	1.91	6	2.32	OK
3467.42	13+36.58	323.34	458.3	2359.63	0.018	4.092	4.086	18.69	2363.716	2369.14	RCB	6	0	1.63	6	1.91	OK
3473.42	13+30.58	6.00	360.0	2359.93	0.050	3.382	3.209	25.01	2363.139	2372.85	RCP	0	0	2.46	5.5	2.29	OK
3558.73	12+45.27	85.31	360.0	2363.44	0.041	3.589	3.469	22.80	2366.909	2374.98	RCP	0	0	2.16	5.5	2.03	OK
3563.73	12+40.27	5.00	330.3	2363.65	0.042	3.137	2.948	25.47	2366.598	2376.67	RCP	0	0	2.61	5.5	2.55	OK
3785.46	10+00.00	221.73	330.3	2372.79	0.041	3.966	3.966	18.01	2376.756	2381.79	RCP	0	0	1.59	5.5	1.53	OK
3809.00	EXISTING FACILITY	23.54	330.3	2373.76	0.041	4.933	4.933	14.70	2378.693	2382.05	RCP	0	0	1.17	5.5	0.57	OK
4122.26		313.26	330.3	2375.72	0.006	6.393	6.393	13.90	2382.113	2385.11	RCP	0	0	0.97	5.5	0.00	OK
4126.26		4.00	288.1	2375.82	0.025	3.267	3.151	22.10	2378.971	2386.56	RCP	0	0	2.19	5	1.85	OK
4454.00		327.74	288.1	2383.78	0.024	3.423	3.343	20.65	2387.123	2393.74	RCP	0	0	1.99	5	1.66	OK
4719.59		265.59	288.1	2388.89	0.019	3.344	3.246	21.35	2392.136	2399.21	RCP	0	0	2.09	5	1.75	OK
4860.42		140.83	288.1	2393.31	0.031	4.241	4.241	16.23	2397.551	2401.64	RCP	0	0	1.39	5	0.76	OK
4864.42		4.00	226.1	2394.31	0.250	3.461	3.399	19.87	2397.709	2403.84	RCP	0	0	1.90	4	0.60	OK
5267.87		403.45	226.1	2403.84	0.024	3.681	3.652	18.79	2407.492	2412.97	RCP	0	0	1.73	4	0.35	OK
5667.87		400.00	226.1	2412.70	0.022	3.906	3.904	18.11	2416.604	2421.70	RCP	0	0	1.62	4	0.10	OK

WSPG STATION	SD PROFILE STATION	LENGTH IN WSPG	DESIGN FLOW	INVERT ELEV	SLOPE	DEPTH OF FLOW ⁽¹⁾	DEPTH OF FLOW	VELOCITY	H.G.L.	E.G.L.	CHANNEL TYPE	BASE WIDTH	Z	FROUDE NUMBER	DESIGN WALL H.T.	FREEBOARD	COMMENTS
		(ft)	(cfs)	(ft)	(ft/ft)	y*(ft)	y(ft)	V(fps)	H(ft)	E(ft)		b(ft)		Fr	(ft)	(ft)	
5671.87	EXISTING FACILITY	4.00	73.9	2414.20	0.375	2.467	2.452	15.12	2416.652	2420.20	RCP	0	0	1.70	2.5	0.05	OK
5998.89		327.02	7.4	2422.58	0.026	4.887	4.887	15.05	2427.467	2430.98	RCP	0	0	1.20	2.5	0.00	OK
6002.89		4.00	23.4	2423.08	0.125	7.131	7.131	7.45	2430.211	2431.07	RCP	0	0	0.49	2	0.00	OK
6329.90		327.01	23.4	2429.66	0.020	4.050	4.050	7.45	2433.710	2434.57	RCP	0	0	0.65	2	0.00	OK

(1) DEPTH WITH AIR ENTRAINMENT

**INLET CALCS FOR MISSION DRIVE/GREENWAY RD
IMPROVEMENTS**

(WSPG RUN FROM MISSION DRIVE/GREENWAY ROAD
IMPROVEMENTS FINAL DRAINAGE REPORT FEBRUARY 2004)

MISSION DRIVE/GREENWAY DRAINAGE DESIGN
Determination of Flow Interception Capacity of Drop Inlets
100-YR FLOW

All calculations are based on FHWA HEC-22 method

INPUT DATA:
n = 0.016

LOCATION	TYPE OF DROP INLET	DESIGN POINT	Q cfs	Q _{w/bypass} cfs	L _{grate} ¹ ft	L _{curb opening} ft	S ft/ft	S _x ft/ft	L _T ² ft	L _{eff} ³ ft	E ⁴	T ⁵ ft	Q _s ⁶ cfs	Q _x ⁷ cfs	E _o ⁸	V ft/s	R _f ⁹	R _s ¹⁰	Q _{grate} cfs	Q _{curb opening} cfs	CAPACITY FACTOR ¹¹		D.I. INTERCEPTION (cfs)	MAX. SYS. CAPACITY (cfs)	BYPASS (cfs)
																					GRATE	CURB OPENING			
Paradise Hills	Existing Type "C" w/ 1 Grate	G1	351.2	351.2	3.0	3.0	0.024	0.020	287.25	0.00	0.00	50.00	271.11	243.11	0.10	10.84	1	0.02	33.43	0.00	70%	80%	23.4	23.4	327.8
	Existing Modi. Type "C" w/ 3 Grates			327.8	9.0	9.0	0.024	0.020	279.05	0.00	0.00	50.00	271.11	243.11	0.10	10.84	1	0.22	82.06	0.00	70%	80%	57.4	50.5	277.3
	Propose 25' Type "CM2" DI			277.3	25.0	25.0	0.024	0.020	260.11	0.00	0.00	50.00	271.11	243.11	0.10	10.84	1	0.75	210.30	0.00	70%	80%	147.2	147.2	130.1
	Existing Modi. Type "C" w/ 4 Grates			130.1	12.0	12.0	0.024	0.020	189.29	0.00	0.00	37.98	130.10	112.60	0.13	9.02	1	0.44	66.56	0.00	70%	80%	46.6	5.0	125.1
	Existing 20' Type "CM2" DI (Middle School)			125.1	12.0	20.0	0.018	0.020	170.80	8.00	0.06	38.62	117.81	102.22	0.13	7.90	1	0.50	66.20	7.29	70%	80%	52.2	31.0	94.1
	Existing 20' Type "CM2" DI (Middle School)			94.1	12.0	20.0	0.027	0.020	171.15	8.00	0.06	32.18	88.63	74.67	0.16	8.56	1	0.46	48.23	5.47	70%	80%	38.1	31.0	63.1
	FLOW USED IN WSPG	288.1																							
Greenway Rd./Du Fort Ave.	Existing 18' Modi. Type "C" w/ 5 Grates	G2	54	54.0	15.0	18.0	0.027	0.020	135.24	3.00	0.03	26.48	52.50	42.57	0.19	7.49	1	0.64	37.32	1.50	70%	80%	27.3	27.3	26.7
	Existing 18' Modi. Type "C" w/ 5 Grates			26.7	15.0	18.0	0.027	0.020	100.57	3.00	0.04	20.26	25.68	19.46	0.24	6.26	1	0.71	20.11	0.99	70%	80%	14.9	14.9	11.8
	FLOW USED IN WSPG	42.2																							
Greenway Rd./Patti Ann Woods Dr.	Existing Modi. Type "C" w/ 4 Grates	G4	105	105.0	12.0	12.0	0.020	0.020	163.78	0.00	0.00	36.27	105.00	90.24	0.14	7.98	1	0.49	59.00	0.00	70%	80%	41.3	41.3	63.7
	Existing Modi. Type "C" w/ 3 Grates			63.7	9.0	12.0	0.020	0.020	132.77	3.00	0.03	29.75	61.90	51.40	0.17	6.99	1	0.39	30.36	1.80	70%	80%	22.7	22.7	41.0
	Propose 20' Type "CM2" DI			41.0	20.0	20.0	0.020	0.020	110.34	0.00	0.00	25.50	41.00	32.97	0.20	6.31	1	0.83	35.28	0.00	70%	80%	24.7	24.7	16.3
	Propose 15' Type "CM2" DI			16.3	15.0	15.0	0.020	0.020	74.91	0.00	0.00	18.05	16.30	11.92	0.27	5.00	1	0.79	13.78	0.00	70%	80%	9.6	9.6	6.7
	FLOW USED IN WSPG	98.3																							
Greenway Rd./Trenier Dr.	Propose 20' Type "CM2" DI	G6	90	90.0	20.0	20.0	0.026	0.020	166.09	0.00	0.00	32.59	90.00	76.00	0.16	8.47	1	0.74	69.99	0.00	70%	80%	49.0	49.0	41.0
	Propose 20' Type "CM2" DI			41.0	20.0	20.0	0.026	0.020	119.39	0.00	0.00	24.28	41.01	32.60	0.21	6.96	1	0.80	34.48	0.00	70%	80%	24.1	24.1	16.9
	Propose 10' Type "CM2" DI			16.9	10.0	10.0	0.026	0.020	82.22	0.00	0.00	17.41	16.87	12.18	0.28	5.57	1	0.55	11.36	0.00	70%	80%	8.0	8.0	8.9
	Propose 10' Type "CM2" DI			8.9	10.0	10.0	0.026	0.020	62.91	0.00	0.00	13.71	8.92	5.86	0.34	4.74	1	0.62	6.68	0.00	70%	80%	4.7	4.7	4.2
	FLOW USED IN WSPG	85.8																							
Greenway Rd./Mission Dr.	Existing 42" Wide Modi. Type "C"	G8	84.0	84.0	21.0	42.0	0.013	0.020	131.05	21.00	0.19	33.37	67.81	57.49	0.15	6.09	1	0.85	59.19	16.19	70%	80%	54.4	54.4	29.6
	Propose 20' Type "CM2" DI			29.6	20.0	20.0	0.025	0.020	102.91	0.00	0.00	21.65	29.61	22.86	0.23	6.32	1	0.83	25.63	0.00	70%	80%	17.9	17.9	11.7
	Propose 20' Type "CM2" DI			11.7	20.0	20.0	0.025	0.020	69.59	0.00	0.00	15.27	11.67	8.02	0.31	5.00	1	0.88	10.69	0.00	70%	80%	7.5	7.5	4.2
	FLOW USED IN WSPG	25.4																							
On Greenway Just Before Patti Ann Wood	Propose 10' Type "CM2" DI		74.9	74.9	10.0	10.0	0.023	0.030	116.66	0.00	0.00	24.10	74.90	59.44	0.21	8.60	1	0.45	42.43	0.00	70%	80%	29.7	29.7	45.2
On Greenway Between Patti Ann Wood & Trenier	Propose 10' Type "CM2" DI			51.9	10.0	10.0	0.023	0.030	99.96	0.00	0.00	21.00	51.86	39.70	0.23	7.84	1	0.49	31.81	0.00	70%	80%	22.3	22.3	29.6
On Greenway Just Before Trenier	Propose 10' Type "CM2" DI			29.6	10.0	10.0	0.022	0.030	77.74	0.00	0.00	17.19	29.59	21.27	0.28	6.68	1	0.57	20.38	0.00	70%	80%	14.3	14.3	15.3

L_{grate}¹ = Length of grate in total parallel with curb/sidewalk

L_T² = Curb opening length required to intercept 100% of the gutter flow
 $L_T = KQ^{0.42}S^{0.3}(1/nS_x)^{0.6}$ K = 0.6

L_{curb opening}³ = Curb opening length upstream of the grate

E⁴ = Curb opening inlet interception efficiency
 $E = 1 - (1 - L/L_T)^{1.8}$

T⁵ = Width of flow
 $T = (Q / ((0.56/n)S_x^{1.67}S^{0.5}))^{1/2.67}$

FLOW USED IN WSPG = DESIGN FLOW (Q) - FLOW BYPASS FROM LAST DI

Q_s⁶ = Gutter flow
 $Q_s = (0.56/n)S_x^{1.67}T^{2.67}S^{0.5}$

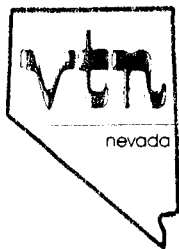
Q_x⁷ = Side flow
 $Q_x = (0.56/n)S_x^{1.67}T_x^{2.67}S^{0.5}$

E_o⁸ = Ratio of frontal flow to total gutter flow
 $E_o = Q_s - Q_x / Q_s$

R_f⁹ = Frontal flow interception efficiency

R_s¹⁰ = Side flow interception efficiency
 $R_s = 1 / (1 + 0.15V^{1.8}/S_xL^{2.3})$

STORM DRAIN PLAN & PROFILE
FOR MISSION DRIVE/GREENWAY RD IMPROVEMENTS
(WSPG RUN FROM MISSION DRIVE/GREENWAY ROAD
IMPROVEMENTS FINAL DRAINAGE REPORT FEBRUARY 2004)



CONSULTING ENGINEERS • PLANNERS • SURVEYORS
PROVIDING QUALITY PROFESSIONAL
SERVICES SINCE 1960

March 15, 2006
W.O.# 6139

City of Henderson
Public Works Department
240 Water Street
P.O. Box 95050
Henderson, Nevada 80990-5050

Attention: Ms. Jonna Sansom, P.E. Project Engineer III

**Subject: SUBSTANTIAL COMPLETION OF MISSION DRIVE / GREENWAY ROAD
IMPROVEMENTS: PARADISE HILLS TO GREENWAY ROAD TO COLLEGE
DRIVE.**

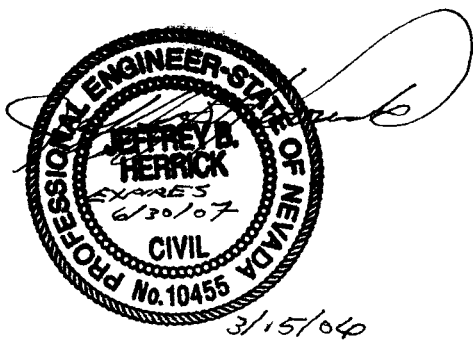
CONTRACT NO. 02-03-11 PWP-CL-2004-4

VTN-Nevada has reviewed the "As-Built" drawings for the subject project. In addition, VTN-Nevada conducted a field survey of the subject project alignment on March 8, 2006. Based on the review of the "As-Built" Drawings and project tour observations, Frehner Construction Company has substantially completed construction of all roadway and storm drain improvements indicated on the project improvement plans and technical documents.

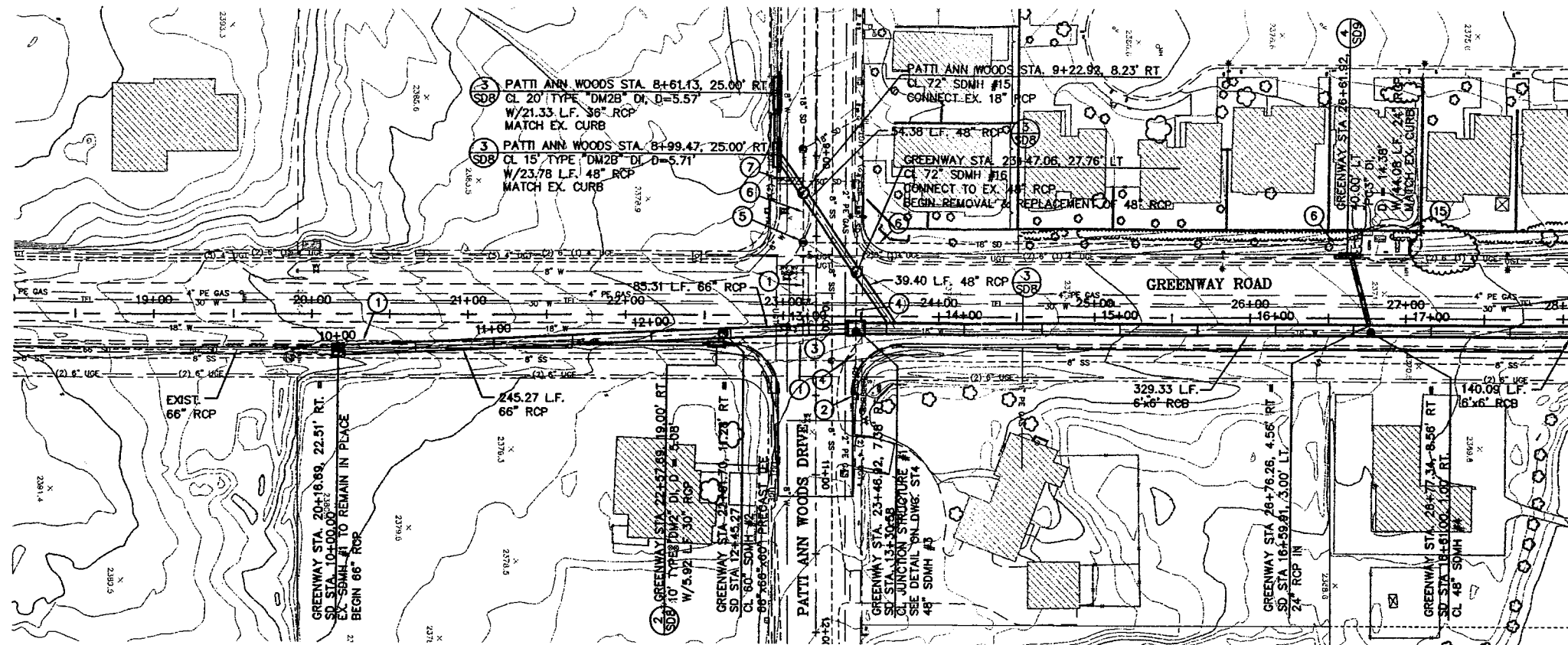
If you have any question regarding substantial Completion of the project, please contact me at (702) 253-2343.

Respectfully,

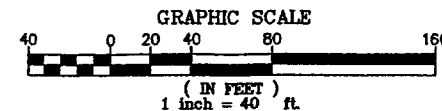
VTN Nevada



Jeffrey B. Herrick, P.E.



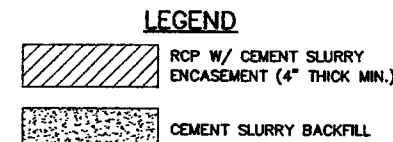
MATCHLINE
SD STA. 18+00.00
SEE SHEET SD2



NOTES

- SEE DRAWING I2 FOR GENERAL NOTES.
- CONTRACTOR SHALL VERIFY ALL HORIZONTAL AND VERTICAL LOCATIONS OF EXISTING UTILITIES PRIOR TO COMMENCEMENT OF CONSTRUCTION.
- CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF EXISTING UTILITY RELOCATION'S WITHIN PROPOSED AND EXISTING SIDEWALK, CURB AND GUTTER AREAS WITH THE APPROPRIATE UTILITY COMPANY.
- CONTRACTOR SHALL INSTALL NEW CURB, GUTTER AND SIDEWALK AS NECESSARY IN AREAS WHERE NEW DROP INLETS ARE INSTALLED IN EXISTING CURB, GUTTER AND SIDEWALK. MATCH EXISTING GRADES.
- SEE DRAWINGS D1 - D8 AND ST1 - ST6 FOR STORM DRAIN DETAILS.

MATCHLINE
SD STA. 18+00.00
SEE SHEET SD2



CONSTRUCTION NOTES

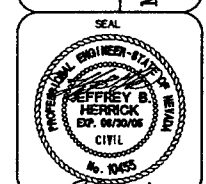
- REMOVE EXISTING 6" STORM DRAIN BLEEDER LINE
- REMOVE EXISTING STORM DRAIN BUBBLER
- CEMENT SLURRY BACKFILL TO SPRING LINE OF EXISTING 6" SS. 6" SS TO REMAIN IN SERVICE DURING CONSTRUCTION
- ABANDON AND/OR REMOVE EXISTING 48" STORM DRAIN RCP
- ABANDON AND/OR REMOVE EXISTING STORM DRAIN MANHOLE
- ABANDON AND/OR REMOVE EXISTING 18" STORM DRAIN RCP
- CEMENT SLURRY ENCASE EXISTING STORM DRAIN RCP (4" THICK MIN.) 10' EACH SIDE OF WATER PIPELINE
- PROTECT IN PLACE, EXISTING BLOCKWALL & UTILITY VAULTS

2 working days
Call before you Overhead
1-702-593-6111
Nevada Power Enhancement and Safety Services Department

2 working days
Call before you Dig
1-800-227-2600
Underground Service Alert (U.S.A.) (86475)

STORM DRAIN PLAN AND PROFILE
SD STA. 10+00.00 TO SD STA. 18+00.00
GREENWAY ROAD

PROJECT
MISSION DRIVE/GREENWAY ROAD IMPROVEMENTS
PARADISE HILLS TO GREENWAY ROAD TO COLLEGE DRIVE



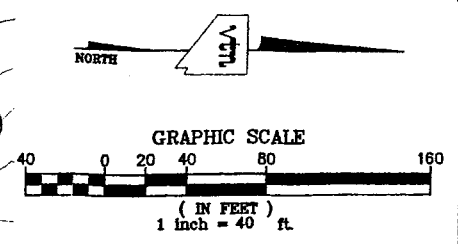
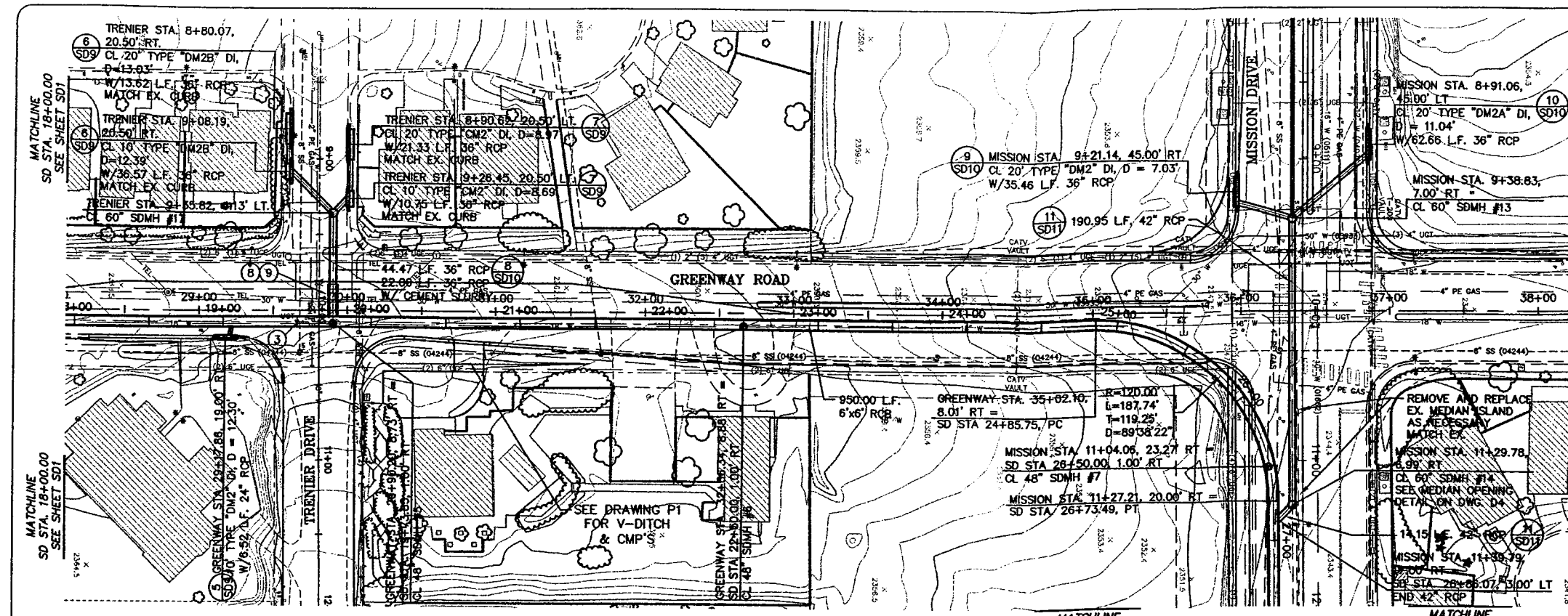
NO. NO. 6139
BY LMW
DATE 09/03/04
SCALE: HORIZ. 1"=40' VERT. 1"=4'
DRAWING SHEET
SD1 OF SHEETS

(06475)

DEPARTMENT OF PUBLIC WORKS
CITY OF HENDERSON

vtm nevada
CONSULTING ENGINEERS • PLANNERS • LAND SURVEYORS
2727 SOUTH RAINBOW BOULEVARD
LAS VEGAS, NEVADA 89146-5148 PHONE (702) 873-7550 FAX (702) 362-2597

I:\1130\DWG\1130-SD-MAIN.DWG



NOTES

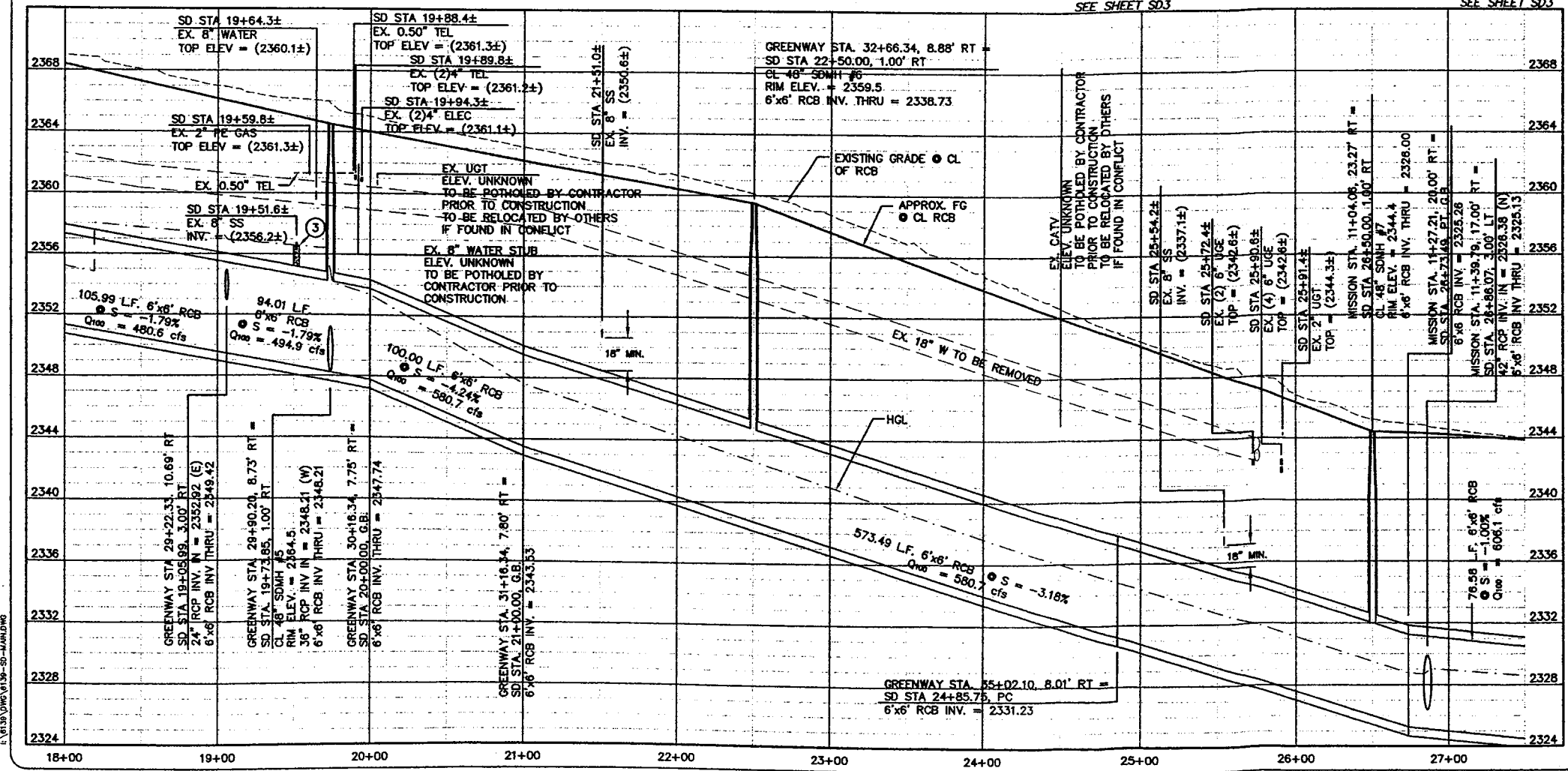
1. SEE DRAWING 12 FOR GENERAL NOTES.
2. CONTRACTOR SHALL VERIFY ALL HORIZONTAL AND VERTICAL LOCATIONS OF EXISTING UTILITIES PRIOR TO COMMENCEMENT OF CONSTRUCTION.
3. CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF EXISTING UTILITY RELOCATION'S WITHIN PROPOSED AND EXISTING SIDEWALK, CURB AND GUTTER AREAS WITH THE APPROPRIATE UTILITY COMPANY.
4. CONTRACTOR SHALL INSTALL NEW CURB, GUTTER AND SIDEWALK AS NECESSARY IN AREAS WHERE NEW DROP INLETS ARE INSTALLED IN EXISTING CURB, GUTTER AND SIDEWALK. MATCH EXISTING GRADES.
5. SEE DRAWINGS D1 - D8 AND S1 - S6 FOR STORM DRAIN DETAILS.

LEGEND

- RCP W/ CEMENT SLURRY ENCASEMENT (4" THICK MIN.)
- CEMENT SLURRY BACKFILL

CONSTRUCTION NOTES

- ③ CEMENT SLURRY BACKFILL TO SPRING LINE OF EXISTING 8" SS TO REMAIN IN SERVICE DURING CONSTRUCTION
- ⑧ CEMENT SLURRY ENCASE SD RCP (4" THICK MIN.) 10' MIN. EACH SIDE OF EXISTING WATER PIPELINE
- ⑨ CEMENT SLURRY BACKFILL TO SPRING LINE OF EX. WATER PIPELINE



Avoid overhead power line contact.
2 working days
Call before you Overhead
1-702-593-6111
Nevada Power Environment and Safety Services Department

Avoid cutting underground utility lines. It's costly.
2 working days
Call before you Dig
1-800-227-2600
Underground Service Alert (USA)

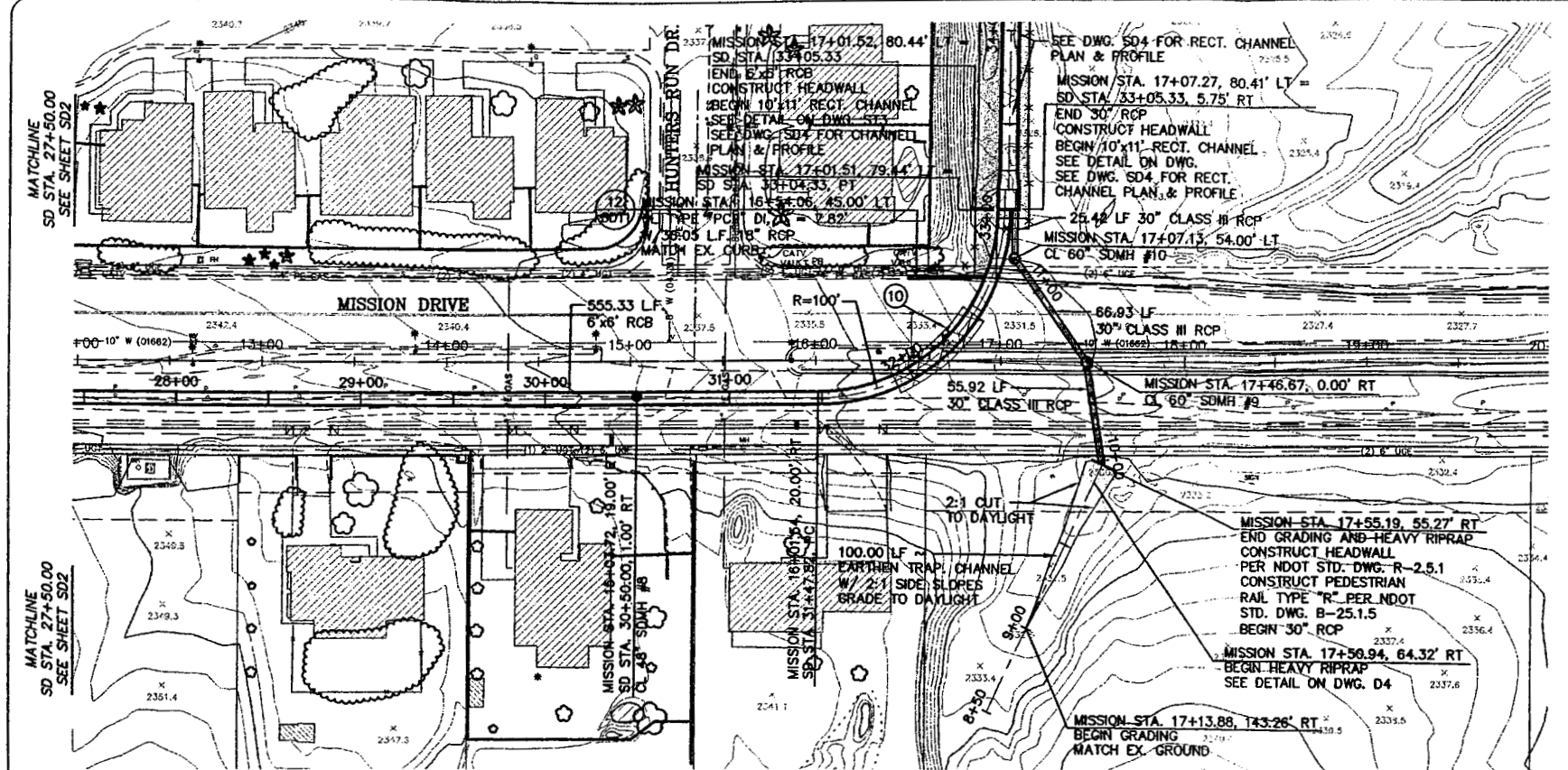
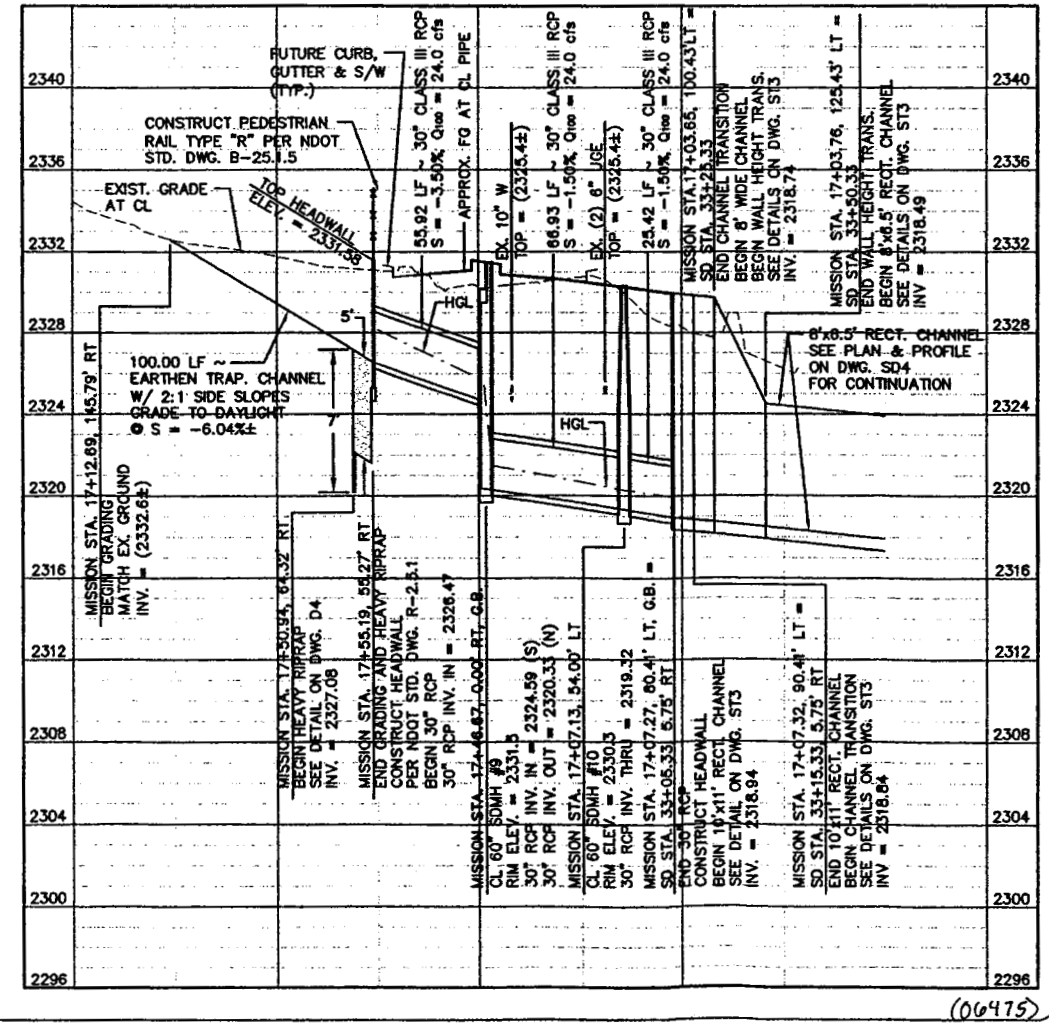
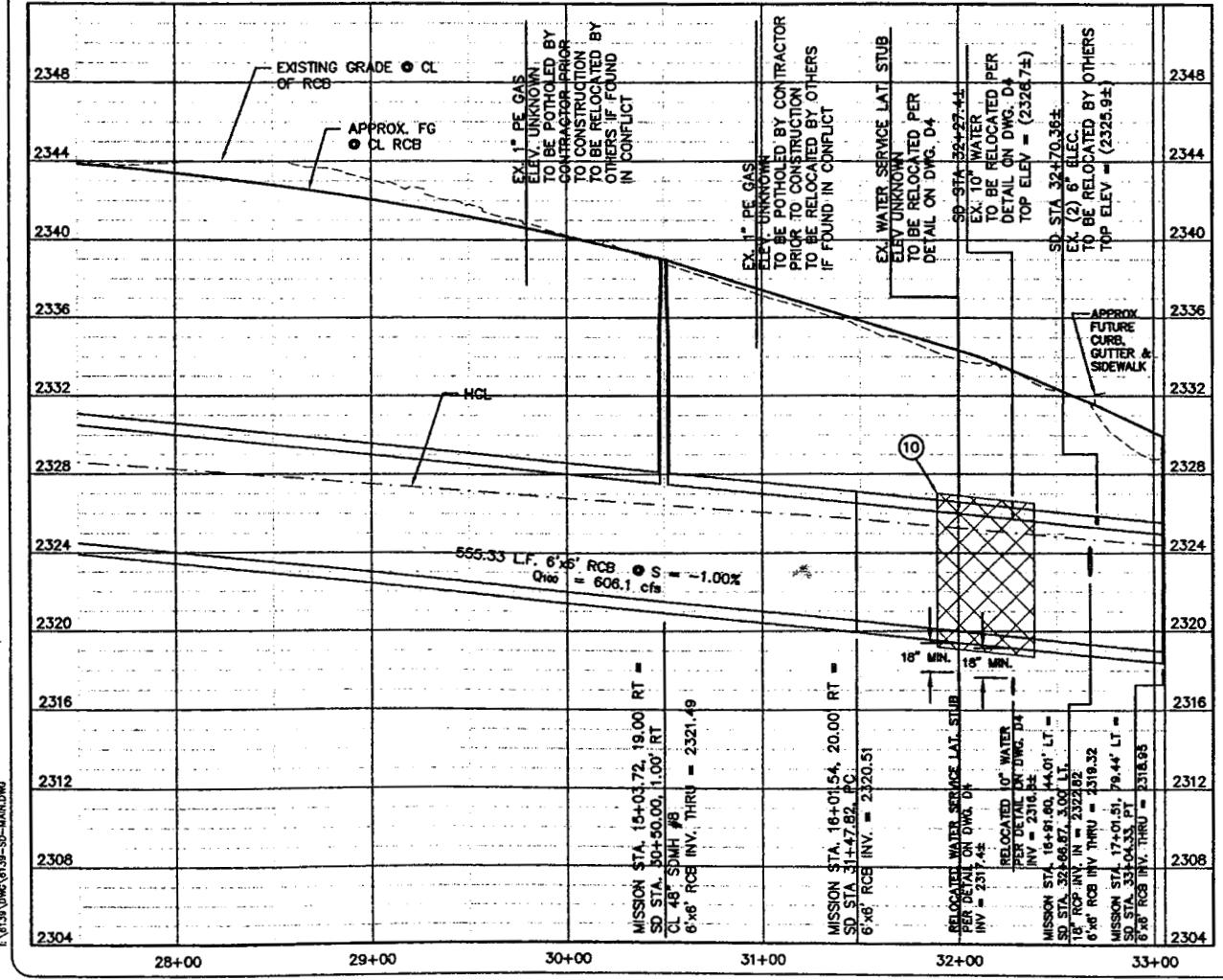
STORM DRAIN PLAN AND PROFILE
SD STA. 18+00.00 TO SD STA. 27+50.00
GREENWAY ROAD
MISSION DRIVE/GREENWAY ROAD IMPROVEMENTS
PARADISE HILLS TO GREENWAY ROAD TO COLLEGE DRIVE

NO. NO.	6139
BY	LMW
DATE	09/03/04
SCALE	HORIZ. 1"=40'
	VERT. 1"=4'
DRAWING	SHEET
SD2	OF 2 SHEETS

DEPARTMENT OF PUBLIC WORKS
 CITY OF HENDERSON
 CONSULTING ENGINEERS • PLANNERS • LAND SURVEYORS
 2727 SOUTH RAINBOW BOULEVARD
 LAS VEGAS, NEVADA 89146-5148 PHONE (702) 873-7550 FAX (702) 362-2597

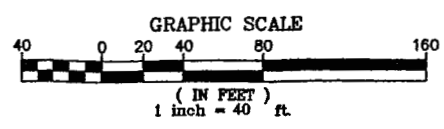
1:10/30/04/0139-SD-MAN/DWG

(06475)



Call before you Overhead
1-702-593-6111
Nevada Power and Safety Services Department

Call before you Dig
1-800-227-2600
Underground Service Alert (USA)



- NOTES**
- SEE DRAWING 12 FOR GENERAL NOTES.
 - CONTRACTOR SHALL VERIFY ALL HORIZONTAL AND VERTICAL LOCATIONS OF EXISTING UTILITIES PRIOR TO COMMENCEMENT OF CONSTRUCTION.
 - CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF EXISTING UTILITY RELOCATION'S WITHIN PROPOSED AND EXISTING SIDEWALK, CURB AND GUTTER AREAS WITH THE APPROPRIATE UTILITY COMPANY.
 - CONTRACTOR SHALL INSTALL NEW CURB, GUTTER AND SIDEWALK AS NECESSARY IN AREAS WHERE NEW DROP INLETS ARE INSTALLED IN EXISTING CURB, GUTTER AND SIDEWALK. MATCH EXISTING GRADES.
 - SEE DRAWINGS D1 - D8 AND ST1 - ST6 FOR STORM DRAIN DETAILS.

- LEGEND**
- RCB W/ POLYURETHANE ELASTOMERIC SEALANT
 - CHANNEL MAINTENANCE ROAD AND MANWAY ACCESS
- CONSTRUCTION NOTES**
- SEAL RCB JOINTS WITH POLYURETHANE ELASTOMERIC SEALANT 10' MINIMUM EACH SIDE OF WATER PIPELINE.

DEPARTMENT OF PUBLIC WORKS
CITY OF HENDERSON

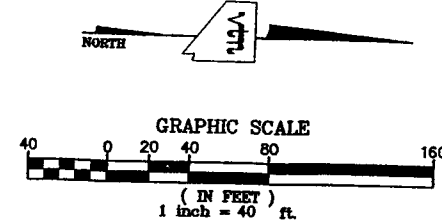
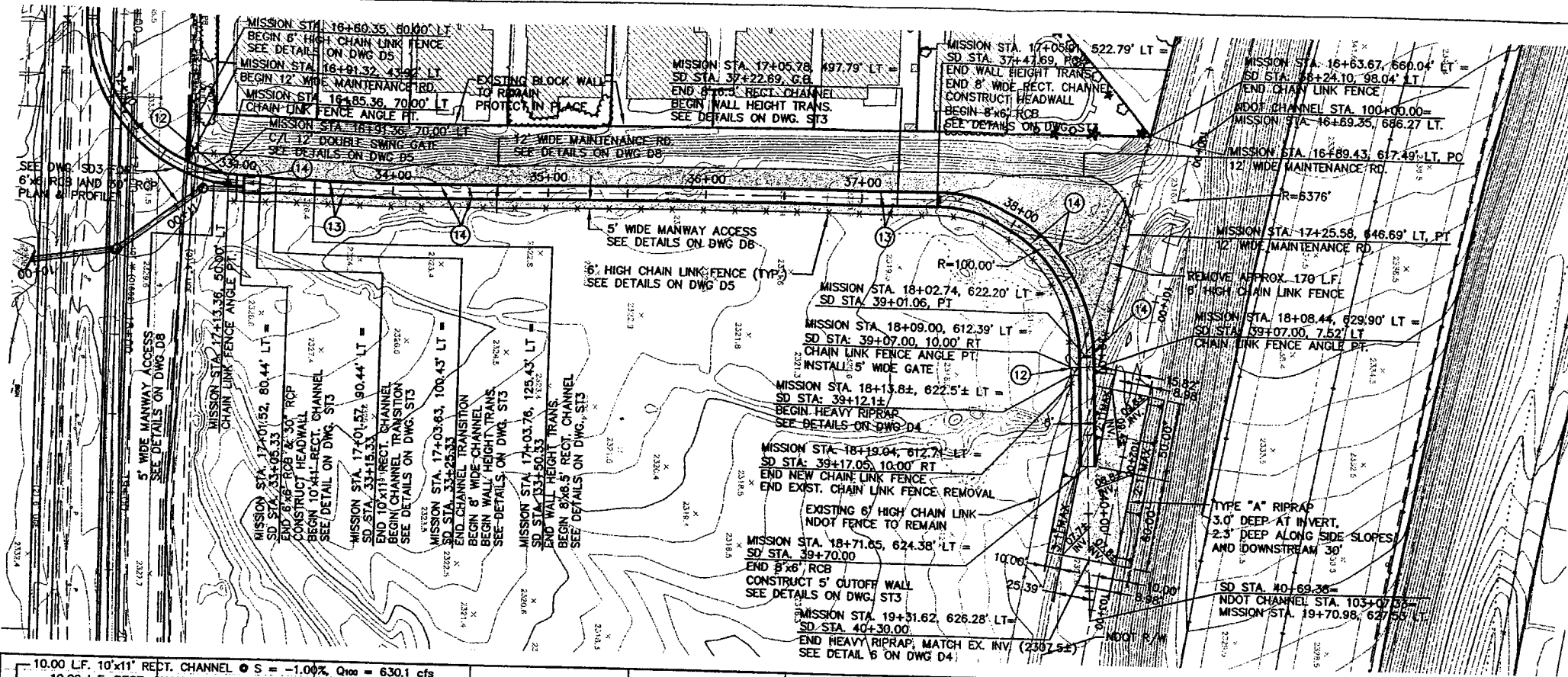
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LAS VEGAS, NEVADA 89146-5146 PHONE (702) 873-7550 FAX (702) 382-2597

vtm nevada

STORM DRAIN PLAN AND PROFILE
SD STA. 27+50.00 TO SD STA. 33+05.33
MISSION DRIVE

MISSION DRIVE/GREENWAY ROAD IMPROVEMENTS
PARADISE HILLS TO GREENWAY ROAD TO COLLEGE DRIVE

NO. 6139
BY TMM
DATE 09/03/04
SCALE HORIZ. 1"=40'
VERT. 1"=4'
DRAWING SHEET
SD3 OF 3 SHEETS



- NOTES**
1. SEE DRAWING 12 FOR GENERAL NOTES.
 2. CONTRACTOR SHALL VERIFY ALL HORIZONTAL AND VERTICAL LOCATIONS OF EXISTING UTILITIES PRIOR TO COMMENCEMENT OF CONSTRUCTION.
 3. CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF EXISTING UTILITY RELOCATION'S WITHIN PROPOSED AND EXISTING SIDEWALK, CURB AND GUTTER AREAS WITH THE APPROPRIATE UTILITY COMPANY.
 4. CONTRACTOR SHALL INSTALL NEW CURB, GUTTER AND SIDEWALK AS NECESSARY IN AREAS WHERE NEW DROP INLETS ARE INSTALLED IN EXISTING CURB, GUTTER AND SIDEWALK. MATCH EXISTING GRADES.
 5. SEE DRAWINGS D1 - D8 AND ST1 - ST6 FOR STORM DRAIN DETAILS.

LEGEND

CHANNEL MAINTENANCE ROAD AND MANWAY ACCESS

- CONSTRUCTION NOTES**
12. INSTALL FLOOD WARNING SIGN ON CHAIN LINK FENCE ADJACENT TO GATE, SEE DETAIL ON DWG. D5
 13. INSTALL CHANNEL LADDER SEE DETAILS ON DWG. D7
 14. INSTALL POST AND CABLE RAILING ON ALL OPEN CHANNEL WALLS AND HEADWALLS, SEE DETAILS ON DWG. D6

Avoid overhead power line contact.
2 working days
Call before you Overhead
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Hazardous Power Environment and Safety Services Department

Avoid cutting underground utility lines. It's costly.
2 working days
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STORM DRAIN PLAN AND PROFILE
SD STA. 33+05.33 TO SD STA. 40+30.00
MISSION DRIVE

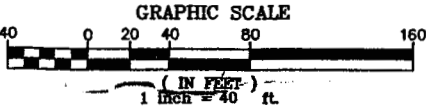
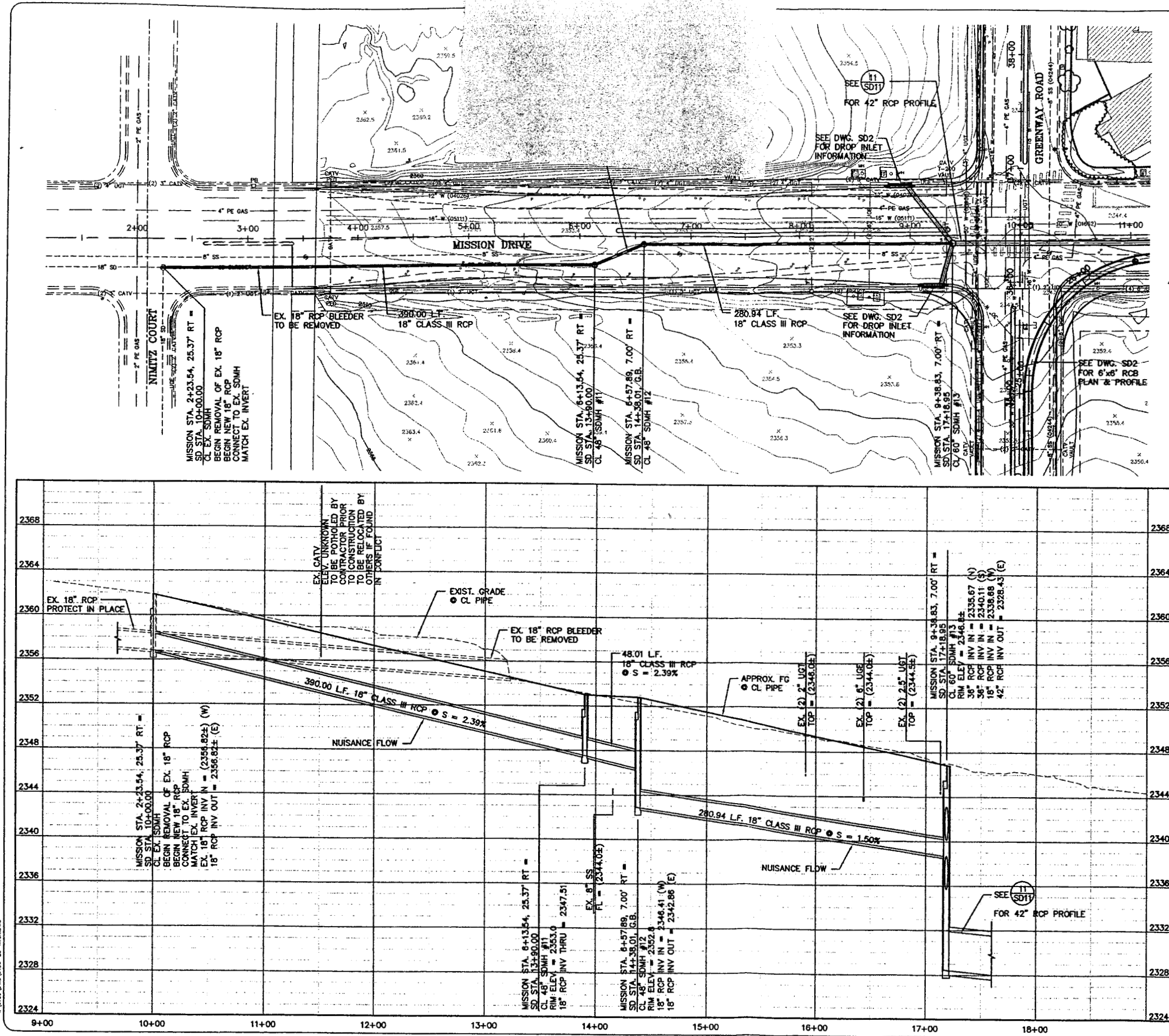
MISSION DRIVE/GREENWAY ROAD IMPROVEMENTS
PARADISE HILLS TO GREENWAY ROAD TO COLLEGE DRIVE

NO. NO. 6139
BY TMK
DATE 09/03/04
SCALE HORIZ. 1"=40'
VERT. 1"=4'

DRAWING SHEET
SD4 OF SHEETS

(06475)

1: 1/8" = 1' (DWG) 1/32" = 1' (PLAN)



- NOTES**
1. SEE DRAWING 12 FOR GENERAL NOTES.
 2. CONTRACTOR SHALL VERIFY ALL HORIZONTAL AND VERTICAL LOCATIONS OF EXISTING UTILITIES PRIOR TO COMMENCEMENT OF CONSTRUCTION.
 3. CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF EXISTING UTILITY RELOCATION'S WITHIN PROPOSED AND EXISTING SIDEWALK, CURB AND GUTTER AREAS WITH THE APPROPRIATE UTILITY COMPANY.
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 5. SEE DRAWINGS D1 - D8 AND ST1 - ST6 FOR STORM DRAIN DETAILS.

2 working days
Call before you Overhead
1-702-593-6111
Nevada Power Environment and Safety Services Department

2 working days
Call before you Dig
1-800-227-2600
Underground Service Alert (USA) (06475)

STORM DRAIN PLAN AND PROFILE
SD STA. 10+00.00 TO SD STA. 17+18.95
MISSION DRIVE

PROJECT
MISSION DRIVE/GREENWAY ROAD IMPROVEMENTS
PARADISE HILLS TO GREENWAY ROAD TO COLLEGE DRIVE

SEAL JEFFREY A. HERRICK CIVIL No. 10455 7/9/2003	
NO. NO.	6139
BY	LMW
DATE	09/03/04
SCALE	HORIZ. 1"=40' VERT. 1"=4'
DRAWING	SHEET
SD5	OF SHEETS

(06475)

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vtm nevada

DEPARTMENT OF PUBLIC WORKS
CITY OF HENDERSON

REVISION
DATE BY

**CARTER BURGESS POST-PROJECT
HEC-RAS MODEL
(FROM FIS STUDY)**

HEC-RAS Version 3.1.3 May 2005
U.S. Army Corp of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

```

X  X  XXXXXX  XXXX  XXXX  XX  XXXX
X  X  X      X  X      X  X  X  X
X  X  X      X  X      X  X  X  X
XXXXXXX XXXX  X  XXX XXXX XXXXXX XXXX
X  X  X      X  X      X  X  X  X
X  X  X      X  X      X  X  X  X
X  X  XXXXXX  XXXX  X  X  X  X  XXXXX

```

PROJECT DATA

Project Title: C-1 Channel System FIS Restudy -Reach 4
Project File : Reach4.prj
Run Date and Time: 10/25/2005 12:49:54 PM

Project in English units

Project Description:
Approximate Methods Hydraulics, Reach 4, d/s of Black Mtn Detention Basin and Mission Hills Interceptor

PLAN DATA

Plan Title: Reach 4

Plan File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\carter burgess FIS\2.2.2.3 REACH 4\Reach4.p01

Geometry Title: C-1 FIS Restudy- Reach 4, Approx Methods

Geometry File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\carter burgess FIS\2.2.2.3 REACH 4\Reach4.g01

Flow Title : Reach 4

Flow File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\carter burgess FIS\2.2.2.3 REACH 4\Reach4.f03

Plan Summary Information:

Number of: Cross Sections = 25 Multiple Openings = 0
Culverts = 0 Inline Structures = 0
Bridges = 0 Lateral Structures = 0

Computational Information

Water surface calculation tolerance = 0.003
Critical depth calculation tolerance = 0.003
Maximum number of iterations = 20
Maximum difference tolerance = 0.1
Flow tolerance factor = 0.001

Computation Options

Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: Reach 4

Flow File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\carter burgess FIS\2.2.2.3 REACH 4\Reach4.f03

Flow Data (cfs)

```

*****
* River      Reach      RS      *      PF 1 *
* Reach 4    CIG2B1 TO CIG2B225 *      286 *
* Reach 4    CIG2B1 TO CIG2B211 *      490 *
* Reach 4    CIG2B1 TO CIG2B26  *      799 *
*****

```

Boundary Conditions

```

*****
* River      Reach      Profile      *      Upstream      Downstream *
*****
* Reach 4    CIG2B1 TO CIG2B2PF 1 *      Normal S = 0.0312      Normal S = 0.0312 *
*****

```

GEOMETRY DATA

Geometry Title: C-1 FIS Restudy- Reach 4, Approx Methods

Geometry File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\carter burgess FIS\2.2.2.3 REACH 4\Reach4.g01

CROSS SECTION

RIVER: Reach 4

REACH: CIG2B1 TO CIG2B2 RS: 25

INPUT

Description: Section Y-Y, Reach 4

Station Elevation Data num= 9

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-100	2575	-58.63	2570.2	-50	2570.3	-25	2570.6	0	2570.8
25	2571.1	50	2571.4	75	2571.7	91.41	2571.9		

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
-100	.03	-100	.03	91.41	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
-100	91.41	550	550	550	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2571.64 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.29 * Wt. n-Val. * * 0.030 * *
* W.S. Elev (ft) * 2571.34 * Reach Len. (ft) * 550.00 * 550.00 * 550.00 *
* Crit W.S. (ft) * 2571.34 * Flow Area (sq ft) * * 65.83 * *
* E.G. Slope (ft/ft) * 0.015979 * Area (sq ft) * * 65.83 * *
* Q Total (cfs) * 286.00 * Flow (cfs) * * 286.00 * *
* Top width (ft) * 113.81 * Top width (ft) * * 113.81 * *
* Vel Total (ft/s) * 4.34 * Avg. Vel. (ft/s) * * 4.34 * *
* Max chl Dpth (ft) * 1.14 * Hydr. Depth (ft) * * 0.58 * *
* Conv. Total (cfs) * 2262.5 * Conv. (cfs) * * 2262.5 * *
* Length Wtd. (ft) * 550.00 * Wetted Per. (ft) * * 113.88 * *
* Min Ch El (ft) * 2570.20 * Shear (lb/sq ft) * * 0.58 * *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 2.51 * *

```

```

* Frctn Loss (ft)      * 9.23 * Cum Volume (acre-ft) * 1.68 * 20.58 * 0.40 *
* C & E Loss (ft)     * 0.02 * Cum SA (acres) * 10.76 * 34.34 * 0.65 *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: CIG2B1 TO CIG2B2 RS: 24

INPUT

Description: Section X-X, Reach 4

```

Station Elevation Data num= 14
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
*****
-142.75 2554.9 -140.25 2554.854 -125.25 2554.6 -100.25 2554.4 -75.25 2554.2
-50.25 2554.8 -25.25 2553.8 0.25 2553.8 25.25 2554.1 50.25 2554.4
75.25 2554.8 100.25 2555.5 107.52 2554.919 118.51 2554.8

```

```

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
*****
-142.75 .03 -140.25 .03 100.25 .03

```

```

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-140 100 400 400 400 .1 .3

```

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2554.76 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.22 * Wt. n-Val. * * 0.030 *
* W.S. Elev (ft) * 2554.55 * Reach Len. (ft) * 400.00 * 400.00 * 400.00 *
* Crit W.S. (ft) * 2554.55 * Flow Area (sq ft) * * 76.29 *
* E.G. Slope (ft/ft) * 0.017628 * Area (sq ft) * * 76.29 *
* Q Total (cfs) * 286.00 * Flow (cfs) * * 286.00 *
* Top Width (ft) * 177.26 * Top Width (ft) * * 177.26 *
* Vel Total (ft/s) * 3.75 * Avg. Vel. (ft/s) * * 3.75 *
* Max Chl Dpth (ft) * 0.75 * Hydr. Depth (ft) * * 0.43 *
* Conv. Total (cfs) * 2154.1 * Conv. (cfs) * * 2154.1 *
* Length Wtd. (ft) * 400.00 * Wetted Per. (ft) * * 177.27 *
* Min Ch El (ft) * 2553.80 * Shear (lb/sq ft) * * 0.47 *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 1.78 *
* Frctn Loss (ft) * 7.17 * Cum Volume (acre-ft) * 1.68 * 19.69 * 0.40 *
* C & E Loss (ft) * 0.00 * Cum SA (acres) * 10.76 * 32.50 * 0.65 *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: CIG2B1 TO CIG2B2 RS: 23

INPUT

Description: Section W-W, Reach 4

```

Station Elevation Data num= 15
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
*****
-151.31 2543.9 -150.25 2543.9 -125.25 2544.2 -100.25 2544.6 -75.25 2545
-50.25 2544.7 -25.25 2544.5 0.25 2544.3 25.25 2544.1 50.25 2544.1
75.25 2544.1 100.25 2544.1 125.25 2544.4 150.25 2544.6 153.52 2544.7

```

```

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
*****
-151.31 .03 -75.25 .03 150.25 .03

```

```

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-75 150 300 300 300 .1 .3

```

Blocked Obstructions

```

Sta L Sta R Elev
*****
-151.31 -75 2545

```

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2544.88 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.20 * Wt. n-Val. * * 0.030 *
* W.S. Elev (ft) * 2544.68 * Reach Len. (ft) * 300.00 * 300.00 * 300.00 *
* Crit W.S. (ft) * 2544.68 * Flow Area (sq ft) * * 78.79 *
* E.G. Slope (ft/ft) * 0.018204 * Area (sq ft) * * 78.79 *
* Q Total (cfs) * 286.00 * Flow (cfs) * * 285.93 *
* Top Width (ft) * 199.53 * Top Width (ft) * * 196.89 *
* Vel Total (ft/s) * 3.63 * Avg. Vel. (ft/s) * * 3.63 *
* Max Chl Dpth (ft) * 0.57 * Hydr. Depth (ft) * * 0.40 *
* Conv. Total (cfs) * 2119.7 * Conv. (cfs) * * 2119.2 *
* Length Wtd. (ft) * 300.00 * Wetted Per. (ft) * * 196.89 *
* Min Ch El (ft) * 2544.10 * Shear (lb/sq ft) * * 0.45 *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 1.65 *
* Frctn Loss (ft) * 5.47 * Cum Volume (acre-ft) * 1.68 * 18.97 * 0.40 *
* C & E Loss (ft) * 0.00 * Cum SA (acres) * 10.76 * 30.78 * 0.64 *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: CIG2B1 TO CIG2B2 RS: 22

INPUT

Description: Section V-V, Reach 4

```

Station Elevation Data num= 15
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
*****
-167.27 2534.9 -150.25 2535 -125.25 2535.1 -100.25 2535.3 -75.25 2535.1
-50.25 2534.9 -25.25 2534.7 0.25 2534.5 25.25 2534.3 50.25 2534.1

```

75 2534.3 100 2534.5 125 2534.7 150 2535 167.27 2535.3 Reach4.rep
Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
-167.27 .03 -100 .03 150 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-100 150 333 386 355 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```
*****
* E.G. Elev (ft)      * 2535.10 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)       * 0.21  * Wt. n-Val.   *      *      *      *
* W.S. Elev (ft)      * 2534.89 * Reach Len. (ft) * 333.00 * 386.00 * 355.00 *
* Crit W.S. (ft)      * 2534.89 * Flow Area (sq ft) *      * 77.56 *      *
* E.G. Slope (ft/ft)  * 0.018293 * Area (sq ft)    *      * 77.56 *      *
* Q Total (cfs)       * 286.00 * Flow (cfs)      *      * 286.00 *      *
* Top Width (ft)      * 189.93 * Top Width (ft)  *      * 189.93 *      *
* Vel Total (ft/s)    * 3.69   * Avg. Vel. (ft/s) *      * 3.69   *      *
* Max Chl Dpth (ft)   * 0.79   * Hydr. Depth (ft) *      * 0.41   *      *
* Conv. Total (cfs)   * 2114.6 * Conv. (cfs)     *      * 2114.6 *      *
* Length Wtd. (ft)    * 386.00 * Wetted Per. (ft) *      * 189.94 *      *
* Min Ch El (ft)      * 2534.10 * Shear (lb/sq ft) *      * 0.47   *      *
* Alpha               * 1.00   * Stream Power (lb/ft s) *      * 1.72   *      *
* Frctn Loss (ft)     * 7.15   * Cum Volume (acre-ft) * 1.68 * 18.44 * 0.40 *
* C & E Loss (ft)     * 0.00   * Cum SA (acres)     * 10.76 * 29.45 * 0.63 *
*****
```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: C1G2B1 TO C1G2B2 RS: 21

INPUT

Description: Section U-U, Reach 4
Station Elevation Data num= 20
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
-225 2525 -218.91 2525 -200 2524.8 -175 2524.5 -150 2524.2
-125 2524 -100 2524 -75 2524 -50 2523.9 -25 2523.8
0 2523.8 25 2524 50 2524.4 75 2524.6 100 2524.7
109.4 2524.7 125 2524.7 150 2524.7 175 2524.7 184.2 2524.7

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
-225 .03 -225 .03 100 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-225 100 300 400 450 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```
*****
* E.G. Elev (ft)      * 2524.57 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)       * 0.20   * Wt. n-Val.   *      *      *      *
* W.S. Elev (ft)      * 2524.37 * Reach Len. (ft) * 300.00 * 400.00 * 450.00 *
* Crit W.S. (ft)      * 2524.37 * Flow Area (sq ft) *      * 80.52 *      *
* E.G. Slope (ft/ft)  * 0.018756 * Area (sq ft)    *      * 80.52 *      *
* Q Total (cfs)       * 286.00 * Flow (cfs)      *      * 286.00 *      *
* Top Width (ft)      * 212.49 * Top Width (ft)  *      * 212.49 *      *
* Vel Total (ft/s)    * 3.55   * Avg. Vel. (ft/s) *      * 3.55   *      *
* Max Chl Dpth (ft)   * 0.57   * Hydr. Depth (ft) *      * 0.38   *      *
* Conv. Total (cfs)   * 2088.3 * Conv. (cfs)     *      * 2088.3 *      *
* Length Wtd. (ft)    * 400.00 * Wetted Per. (ft) *      * 212.50 *      *
* Min Ch El (ft)      * 2523.80 * Shear (lb/sq ft) *      * 0.44   *      *
* Alpha               * 1.00   * Stream Power (lb/ft s) *      * 1.58   *      *
* Frctn Loss (ft)     * 7.33   * Cum Volume (acre-ft) * 10.76 * 17.74 * 0.40 *
* C & E Loss (ft)     * 0.00   * Cum SA (acres)     * 10.76 * 27.67 * 0.63 *
*****
```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: C1G2B1 TO C1G2B2 RS: 20

INPUT

Description: Section T-T, Reach 4
Station Elevation Data num= 25
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
-352.59 2515.1 -350 2515.1 -325 2514.9 -300 2514.7 -275 2514.5
-250 2514.2 -225 2513.8 -200 2513.4 -175 2513.1 -150 2512.7
-125 2512.3 -100 2511.8 -75 2511.2 -50 2510.6 -25 2510
0 2509.9 25 2509.9 50 2510.1 75 2510.1 100 2510
125 2510 150 2510.2 175 2514.3 200 2515 221.15 2515

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
-352.59 .03 -350 .03 200 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-350 200 700 500 400 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```
*****
* E.G. Elev (ft)      * 2510.65 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)       * 0.20   * Wt. n-Val.   *      *      *      *
* W.S. Elev (ft)      * 2510.44 * Reach Len. (ft) * 700.00 * 500.00 * 400.00 *
* Crit W.S. (ft)      * 2510.44 * Flow Area (sq ft) *      * 78.89 *      *
* E.G. Slope (ft/ft)  * 0.017889 * Area (sq ft)    *      * 78.89 *      *
* Q Total (cfs)       * 286.00 * Flow (cfs)      *      * 286.00 *      *
* Top Width (ft)      * 194.84 * Top Width (ft)  *      * 194.84 *      *
* Vel Total (ft/s)    * 3.63   * Avg. Vel. (ft/s) *      * 3.63   *      *
* Max Chl Dpth (ft)   * 0.54   * Hydr. Depth (ft) *      * 0.40   *      *
* Conv. Total (cfs)   * 2138.3 * Conv. (cfs)     *      * 2138.3 *      *
* Length Wtd. (ft)    * 522.84 * Wetted Per. (ft) *      * 194.86 *      *
* Min Ch El (ft)      * 2509.90 * Shear (lb/sq ft) *      * 0.45   *      *
* Alpha               * 1.00   * Stream Power (lb/ft s) *      * 1.64   *      *
* Frctn Loss (ft)     * 5.16   * Cum Volume (acre-ft) * 1.68 * 17.00 * 0.40 *
*****
```

Reach4.rep
* C & E Loss (ft) * 0.03 * Cum SA (acres) * 10.76 * 25.80 * 0.63 *

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: C1G2B1 TO C1G2B2 RS: 19

INPUT

Description: Section S-S, Reach 4

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-720	2485	-500	2487	-207.87	2493.4	-200	2493.5	-175	2493.9
-150	2494.1	-125	2494.3	-100	2494.5	-75	2494.7	-50	2494.8
-25	2494.6	0	2494.3	25	2493.9	50	2493.9	75	2494.6
100	2495.2	125	2497.4	150	2499.8	175	2500	200	2500
207.87	2500	245	2495	410	2500	440	2510		

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
-720 .03 -50 .03 200 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-50 200 400 409 430 .1 .3
Blocked Obstructions num= 1
Sta L Sta R Elev
-720 -50 2494.8

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2495.00	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.09	* wt. n-Val.	* 0.030	* 0.030	*
* W.S. Elev (ft)	* 2494.91	* Reach Len. (ft)	* 400.00	* 409.00	* 430.00
* Crit W.S. (ft)	* 2494.91	* Flow Area (sq ft)	* 73.12	* 80.64	*
* E.G. Slope (ft/ft)	* 0.000642	* Area (sq ft)	* 670.11	* 137.90	*
* Q Total (cfs)	* 286.00	* Flow (cfs)	* 65.34	* 220.66	*
* Top width (ft)	* 807.88	* Top width (ft)	* 670.00	* 137.88	*
* Vel Total (ft/s)	* 1.86	* Avg. vel. (ft/s)	* 0.89	* 2.74	*
* Max chl Dpth (ft)	* 1.01	* Hydr. Depth (ft)	* 0.11	* 0.58	*
* Conv. Total (cfs)	* 3619.9	* Conv. (cfs)	* 827.0	* 2792.9	*
* Length Wtd. (ft)	* 407.97	* Wetted Per. (ft)	* 670.11	* 137.90	*
* Min ch El (ft)	* 2493.90	* Shear (lb/sq ft)	* 0.04	* 0.23	*
* Alpha	* 1.72	* Stream Power (lb/ft s)	* 0.04	* 0.62	*
* Frctn Loss (ft)	* 3.85	* Cum Volume (acre-ft)	* 1.10	* 16.09	* 0.40
* C & E Loss (ft)	* 0.02	* Cum SA (acres)	* 5.37	* 23.89	* 0.63

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The cross-section end points had to be extended vertically for the computed water surface.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: C1G2B1 TO C1G2B2 RS: 18

INPUT

Description: Section R-R, Reach 4

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-200	2481	-50	2480	0	2479.7	120	2477.4
300	2487					220	2480

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
-200 .03 -50 .03 300 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-200 300 400 399 400 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2478.90	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.30	* wt. n-Val.	* 0.030	* 0.030	*
* W.S. Elev (ft)	* 2478.59	* Reach Len. (ft)	* 400.00	* 399.00	* 400.00
* Crit W.S. (ft)	* 2478.59	* Flow Area (sq ft)	* 64.56	* 64.56	*
* E.G. Slope (ft/ft)	* 0.015925	* Area (sq ft)	* 286.00	* 286.00	*
* Q Total (cfs)	* 286.00	* Flow (cfs)	* 108.18	* 108.18	*
* Top width (ft)	* 108.18	* Top width (ft)	* 4.43	* 4.43	*
* Vel Total (ft/s)	* 4.43	* Avg. vel. (ft/s)	* 0.60	* 0.60	*
* Max chl Dpth (ft)	* 1.19	* Hydr. Depth (ft)	* 2266.4	* 108.21	*
* Conv. Total (cfs)	* 2266.4	* Conv. (cfs)	* 108.21	* 0.59	*
* Length Wtd. (ft)	* 399.06	* Wetted Per. (ft)	* 1.00	* 2.63	*
* Min ch El (ft)	* 2477.40	* Shear (lb/sq ft)	* 0.76	* 15.41	* 0.40
* Alpha	* 1.00	* Stream Power (lb/ft s)	* 2.30	* 22.73	*
* Frctn Loss (ft)	* 5.97	* Cum Volume (acre-ft)	* 0.76	* 15.41	* 0.40
* C & E Loss (ft)	* 0.04	* Cum SA (acres)	* 2.30	* 22.73	* 0.63

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: C1G2B1 TO C1G2B2 RS: 17

INPUT

Description: Section Q-Q, Reach 4

Station Elevation Data		num=	18	Sta Elev		Sta Elev	Sta Elev
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-390	2465.9	-175.71	2465.3	-175	2465.3	-150	2465.6
-100	2465.4	-75	2465.2	-50	2465	-25	2465
25	2465	50	2465.8	75	2466.6	100	2468.6
150	2468.6	175	2469	175.71	2469	125	2468.1

Manning's n Values		num=	3	Sta n Val		Sta n Val
Sta	n Val	Sta	n Val	Sta	n Val	Sta
-390	.03	-125	.03	175	.03	

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	-125	175		400	431	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.17	* 0.030	* 0.030	
* W.S. Elev (ft)	* 2465.60	* Reach Len. (ft)	* 400.00	* 528.00
* Crit W.S. (ft)	* 2465.60	* Flow Area (sq ft)	* 20.37	* 72.70
* E.G. Slope (ft/ft)	* 0.014097	* Area (sq ft)	* 20.37	* 72.70
* Q Total (cfs)	* 286.00	* Flow (cfs)	* 34.06	* 251.94
* Top Width (ft)	* 295.09	* Top Width (ft)	* 134.38	* 160.71
* Vel Total (ft/s)	* 3.07	* Avg. Vel. (ft/s)	* 1.67	* 3.47
* Max Chl Dpth (ft)	* 0.60	* Hydr. Depth (ft)	* 0.15	* 0.45
* Conv. Total (cfs)	* 2408.8	* Conv. (cfs)	* 286.9	* 2122.0
* Length Wtd. (ft)	* 429.15	* Wetted Per. (ft)	* 134.38	* 160.72
* Min Ch El (ft)	* 2465.00	* Shear (lb/sq ft)	* 0.13	* 0.40
* Alpha	* 1.16	* Stream Power (lb/ft s)	* 0.22	* 1.38
* Frctn Loss (ft)	* 6.42	* Cum Volume (acre-ft)	* 0.67	* 14.78
* C & E Loss (ft)	* 0.01	* Cum SA (acres)	* 1.68	* 21.50

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 to C1G2B2 RS: 16

Station Elevation Data		num=	19	Sta Elev		Sta Elev	Sta Elev
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-208.12	2453.8	-200	2453.8	-175	2453.8	-150	2453.6
-100	2452.9	-75	2452.4	-50	2452.1	-25	2452.3
25	2453.8	50	2454.4	75	2454.7	100	2454.7
150	2454.9	175	2455	200	2455	208.12	2455.3

Manning's n Values		num=	3	Sta n Val		Sta n Val
Sta	n Val	Sta	n Val	Sta	n Val	Sta
-208.12	.03	-200	.03	200	.03	

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	-200	200		440	414	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 2453.38	* 0.030	* 0.030	
* W.S. Elev (ft)	* 2453.08	* Reach Len. (ft)	* 440.00	* 400.00
* Crit W.S. (ft)	* 2453.08	* Flow Area (sq ft)	* 64.98	
* E.G. Slope (ft/ft)	* 0.015929	* Area (sq ft)	* 64.98	
* Q Total (cfs)	* 286.00	* Flow (cfs)	* 286.00	
* Top Width (ft)	* 109.97	* Top Width (ft)	* 109.97	
* Vel Total (ft/s)	* 4.40	* Avg. Vel. (ft/s)	* 4.40	
* Max Chl Dpth (ft)	* 0.98	* Hydr. Depth (ft)	* 0.59	
* Conv. Total (cfs)	* 2266.0	* Conv. (cfs)	* 2266.0	
* Length Wtd. (ft)	* 414.00	* Wetted Per. (ft)	* 109.99	
* Min Ch El (ft)	* 2452.10	* Shear (lb/sq ft)	* 0.59	
* Alpha	* 1.00	* Stream Power (lb/ft s)	* 2.59	
* Frctn Loss (ft)	* 6.79	* Cum Volume (acre-ft)	* 0.57	* 14.10
* C & E Loss (ft)	* 0.02	* Cum SA (acres)	* 1.06	* 20.16

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 to C1G2B2 RS: 15

Station Elevation Data		num=	43	Sta Elev		Sta Elev	Sta Elev
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-550	2440.7	-538.07	2440.7	-525	2440.5	-500	2440.1
-450	2440	-425	2440	-400	2440	-375	2440.7
-325	2442	-300	2442.1	-275	2442.5	-250	2442.8
-200	2443.5	-175	2443.6	-150	2443.5	-125	2443.5
-75	2444	-50	2444.6	-25	2445	0	2445.8
50	2446.4	75	2447	100	2447.4	125	2447.5
175	2447.7	200	2447.9	225	2448.1	250	2448.5
300	2448.7	325	2448.8	350	2448.9	375	2449.2
425	2449.8	428.39	2449.8	481.7	2449.8	400	2449.5

Manning's n Values		num=	3	Sta n Val		Sta n Val
Sta	n Val	Sta	n Val	Sta	n Val	Sta
-550	.03	-550	.03	400	.03	

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	-550	400		250	561	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 2440.84	* 0.030	* 0.030	
* W.S. Elev (ft)	* 2440.60	* Reach Len. (ft)	* 250.00	* 650.00

```

* Crit W.S. (ft)      * 2440.60 * Flow Area (sq ft) *      * 72.79 *
* E.G. Slope (ft/ft) * 0.016917 * Area (sq ft) *      * 72.79 *
* Q Total (cfs)       * 286.00 * Flow (cfs) *      * 286.00 *
* Top Width (ft)      * 152.83 * Top Width (ft) *      * 152.83 *
* Vel Total (ft/s)     * 3.93 * Avg. Vel. (ft/s) *      * 3.93 *
* Max Chl Dpth (ft)   * 0.60 * Hydr. Depth (ft) *      * 0.48 *
* Conv. Total (cfs)    * 2198.9 * Conv. (cfs) *      * 2198.9 *
* Length Wtd. (ft)     * 561.00 * Wetted Per. (ft) *      * 152.84 *
* Min Ch El (ft)      * 2440.00 * Shear (lb/sq ft) *      * 0.50 *
* Alpha               * 1.00 * Stream Power (lb/ft s) *      * 1.98 *
* Frctn Loss (ft)     * 9.91 * Cum Volume (acre-ft) * 0.57 * 13.44 * 0.40 *
* C & E Loss (ft)     * 0.02 * Cum SA (acres) * 1.06 * 18.91 * 0.63 *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 14

INPUT
 Description: Section N-N, Reach 4
 Station Elevation Data num= 41

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-542.98	2434.2	-525	2433.9	-500	2433.5	-475	2432.8	-450	2432
-425	2431.2	-400	2430.4	-375	2430	-350	2430	-325	2429.7
-300	2429.8	-275	2430	-250	2430.3	-225	2430.5	-200	2430.7
-175	2430.9	-150	2431	-125	2431	-100	2430.9	-75	2430.7
-50	2430.6	-25	2430.4	0	2430.2	25	2430.5	50	2430.6
75	2430.7	100	2431	125	2431.4	150	2431.6	175	2431.7
200	2431.5	225	2431.2	250	2430.8	275	2431.3	300	2433.3
325	2435	350	2435.3	375	2436.1	400	2436.9	425	2437.3
449.25	2436.8								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-542.98	.03	-542.98	.03	425	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -542.98 425 700 397 370 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

* E.G. Elev (ft)      * 2430.65 * Element * Left 08 * Channel * Right 08 *
* Vel Head (ft)       * 0.18 * Wt. n-Val. * 0.030 *
* W.S. Elev (ft)       * 2430.47 * Reach Len. (ft) * 700.00 * 397.00 * 370.00 *
* Crit W.S. (ft)       * 2430.47 * Flow Area (sq ft) * 83.39 *
* E.G. Slope (ft/ft)   * 0.018458 * Area (sq ft) * 83.39 *
* Q Total (cfs)        * 286.00 * Flow (cfs) * 286.00 *
* Top Width (ft)       * 229.15 * Top Width (ft) * 229.15 *
* Vel Total (ft/s)     * 3.43 * Avg. Vel. (ft/s) * 3.43 *
* Max Chl Dpth (ft)    * 0.77 * Hydr. Depth (ft) * 0.36 *
* Conv. Total (cfs)    * 2105.1 * Conv. (cfs) * 2105.1 *
* Length Wtd. (ft)     * 397.00 * Wetted Per. (ft) * 229.16 *
* Min Ch El (ft)       * 2429.70 * Shear (lb/sq ft) * 0.42 *
* Alpha               * 1.00 * Top Volume (acre-ft) * 1.44 *
* Frctn Loss (ft)     * 6.80 * Cum Volume (acre-ft) * 0.57 * 12.44 * 0.40 *
* C & E Loss (ft)     * 0.01 * Cum SA (acres) * 1.06 * 16.45 * 0.63 *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 13

INPUT
 Description: Section M-M, Reach 4
 Station Elevation Data num= 33

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-389.72	2411.2	-375	2411.3	-350	2411	-325	2410.5	-300	2410
-275	2410	-250	2410	-225	2410.8	-200	2411.9	-175	2412.7
-150	2413.5	-125	2414	-100	2414.4	-75	2414.5	-50	2414.6
-25	2414.4	0	2414.5	25	2414.4	50	2414.6	75	2414.6
100	2414.6	125	2415	150	2415.7	175	2417.1	200	2418.7
225	2420.1	250	2420.8	275	2421.2	300	2421.3	325	2421
350	2420.6	375	2420.1	389.72	2419.3				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-389.72	.03	-375	.03	300	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -375 300 368 410 454 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

* E.G. Elev (ft)      * 2411.09 * Element * Left 08 * Channel * Right 08 *
* Vel Head (ft)       * 0.29 * Wt. n-Val. * 0.030 *
* W.S. Elev (ft)       * 2410.80 * Reach Len. (ft) * 368.00 * 410.00 * 454.00 *
* Crit W.S. (ft)       * 2410.80 * Flow Area (sq ft) * 66.15 *
* E.G. Slope (ft/ft)   * 0.015952 * Area (sq ft) * 66.15 *
* Q Total (cfs)        * 286.00 * Flow (cfs) * 286.00 *
* Top Width (ft)       * 115.09 * Top Width (ft) * 115.09 *
* Vel Total (ft/s)     * 4.32 * Avg. Vel. (ft/s) * 4.32 *
* Max Chl Dpth (ft)    * 0.80 * Hydr. Depth (ft) * 0.57 *
* Conv. Total (cfs)    * 2264.4 * Conv. (cfs) * 2264.4 *
* Length Wtd. (ft)     * 410.00 * Wetted Per. (ft) * 115.11 *
* Min Ch El (ft)       * 2410.00 * Shear (lb/sq ft) * 0.57 *
* Alpha               * 1.00 * Stream Power (lb/ft s) * 2.47 *
* Frctn Loss (ft)     * 7.19 * Cum Volume (acre-ft) * 0.57 * 11.75 * 0.40 *
* C & E Loss (ft)     * 0.04 * Cum SA (acres) * 1.06 * 14.88 * 0.63 *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: CIG2B1 TO CIG2B2 RS: 12

INPUT

Description: Section L-L, Reach 4

Station Elevation Data		num= 34		Sta Elev		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-550	2400	-530	2400	-364.06	2398.7	-350	2398.8	-325	2398.7		
-300	2398.7	-275	2398.7	-250	2398.6	-225	2398.6	-200	2398.7		
-175	2398.8	-150	2399	-125	2399.4	-100	2399.7	-75	2399.9		
-50	2400	-25	2400	0	2400	25	2399.9	50	2399.9		
75	2399.8	100	2399.5	125	2399.6	150	2399.8	175	2400		
200	2401.1	225	2401.2	250	2400	275	2400	300	2400		
325	2400.1	350	2401.3	360.92	2401.765	364.06	2401.9				

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
-550	.03	-550	.03	364.06	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	-550	364.06		519	440	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2399.25	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft) <td>* 0.17<td>* Wt. n-Val.<td>* 0.030<td></td><td></td></td></td></td>	* 0.17 <td>* Wt. n-Val.<td>* 0.030<td></td><td></td></td></td>	* Wt. n-Val. <td>* 0.030<td></td><td></td></td>	* 0.030 <td></td> <td></td>		
* W.S. Elev (ft) <td>* 2399.08<td>* Reach Len. (ft)<td>* 519.00<td>* 440.00<td>* 373.00</td></td></td></td></td>	* 2399.08 <td>* Reach Len. (ft)<td>* 519.00<td>* 440.00<td>* 373.00</td></td></td></td>	* Reach Len. (ft) <td>* 519.00<td>* 440.00<td>* 373.00</td></td></td>	* 519.00 <td>* 440.00<td>* 373.00</td></td>	* 440.00 <td>* 373.00</td>	* 373.00
* Crit W.S. (ft) <td>* 2399.08<td>* Flow Area (sq ft)<td></td><td>* 87.45</td><td></td></td></td>	* 2399.08 <td>* Flow Area (sq ft)<td></td><td>* 87.45</td><td></td></td>	* Flow Area (sq ft) <td></td> <td>* 87.45</td> <td></td>		* 87.45	
* E.G. Slope (ft/ft) <td>* 0.019361<td>* Area (sq ft)<td></td><td>* 87.45</td><td></td></td></td>	* 0.019361 <td>* Area (sq ft)<td></td><td>* 87.45</td><td></td></td>	* Area (sq ft) <td></td> <td>* 87.45</td> <td></td>		* 87.45	
* Q Total (cfs) <td>* 286.00<td>* Flow (cfs)<td></td><td>* 286.00</td><td></td></td></td>	* 286.00 <td>* Flow (cfs)<td></td><td>* 286.00</td><td></td></td>	* Flow (cfs) <td></td> <td>* 286.00</td> <td></td>		* 286.00	
* Top Width (ft) <td>* 267.49<td>* Top Width (ft)<td></td><td>* 267.49</td><td></td></td></td>	* 267.49 <td>* Top Width (ft)<td></td><td>* 267.49</td><td></td></td>	* Top Width (ft) <td></td> <td>* 267.49</td> <td></td>		* 267.49	
* Vel Total (ft/s) <td>* 3.27<td>* Avg. Vel. (ft/s)<td></td><td>* 3.27</td><td></td></td></td>	* 3.27 <td>* Avg. Vel. (ft/s)<td></td><td>* 3.27</td><td></td></td>	* Avg. Vel. (ft/s) <td></td> <td>* 3.27</td> <td></td>		* 3.27	
* Max Chl Dpth (ft) <td>* 0.48<td>* Hydr. Depth (ft)<td></td><td>* 0.33</td><td></td></td></td>	* 0.48 <td>* Hydr. Depth (ft)<td></td><td>* 0.33</td><td></td></td>	* Hydr. Depth (ft) <td></td> <td>* 0.33</td> <td></td>		* 0.33	
* Conv. Total (cfs) <td>* 2055.4<td>* Conv. (cfs)<td></td><td>* 2055.4</td><td></td></td></td>	* 2055.4 <td>* Conv. (cfs)<td></td><td>* 2055.4</td><td></td></td>	* Conv. (cfs) <td></td> <td>* 2055.4</td> <td></td>		* 2055.4	
* Length Wtd. (ft) <td>* 440.00<td>* Wetted Per. (ft)<td></td><td>* 267.50</td><td></td></td></td>	* 440.00 <td>* Wetted Per. (ft)<td></td><td>* 267.50</td><td></td></td>	* Wetted Per. (ft) <td></td> <td>* 267.50</td> <td></td>		* 267.50	
* Min Ch El (ft) <td>* 2398.60<td>* Shear (lb/sq ft)<td></td><td>* 0.40</td><td></td></td></td>	* 2398.60 <td>* Shear (lb/sq ft)<td></td><td>* 0.40</td><td></td></td>	* Shear (lb/sq ft) <td></td> <td>* 0.40</td> <td></td>		* 0.40	
* Alpha <td>* 1.00<td>* Stream Power (lb/ft s)<td></td><td>* 1.29</td><td></td></td></td>	* 1.00 <td>* Stream Power (lb/ft s)<td></td><td>* 1.29</td><td></td></td>	* Stream Power (lb/ft s) <td></td> <td>* 1.29</td> <td></td>		* 1.29	
* Frctn Loss (ft) <td>* 7.54<td>* Cum Volume (acre-ft)<td>* 0.57</td><td>* 11.03</td><td>* 0.40</td></td></td>	* 7.54 <td>* Cum Volume (acre-ft)<td>* 0.57</td><td>* 11.03</td><td>* 0.40</td></td>	* Cum Volume (acre-ft) <td>* 0.57</td> <td>* 11.03</td> <td>* 0.40</td>	* 0.57	* 11.03	* 0.40
* C & E Loss (ft) <td>* 0.01<td>* Cum SA (acres)<td>* 1.06</td><td>* 13.08</td><td>* 0.63</td></td></td>	* 0.01 <td>* Cum SA (acres)<td>* 1.06</td><td>* 13.08</td><td>* 0.63</td></td>	* Cum SA (acres) <td>* 1.06</td> <td>* 13.08</td> <td>* 0.63</td>	* 1.06	* 13.08	* 0.63

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: CIG2B1 TO CIG2B2 RS: 11

INPUT

Description: Section K-K, Reach 4

Station Elevation Data		num= 25		Sta Elev		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-287.72	2383.7	-275	2383.4	-250	2383.9	-225	2384.2	-200	2384.2		
-175	2384.1	-150	2383.8	-125	2383.8	-100	2383.6	-75	2383.2		
-50	2383	-25	2383.1	0	2383.4	25	2383.9	50	2384.6		
75	2385	100	2387.8	125	2390.3	150	2391.3	175	2391.6		
200	2391.9	225	2391.8	250	2390.7	275	2390	287.72	2389.6		

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
-287.72	.03	-200	.03	200	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	-200	200		388	420	.1	.3

Blocked obstructions

Sta L Sta R	Elev
-287.72	-200

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2384.34	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft) <td>* 0.29<td>* Wt. n-Val.<td>* 0.030<td></td><td></td></td></td></td>	* 0.29 <td>* Wt. n-Val.<td>* 0.030<td></td><td></td></td></td>	* Wt. n-Val. <td>* 0.030<td></td><td></td></td>	* 0.030 <td></td> <td></td>		
* W.S. Elev (ft) <td>* 2384.06<td>* Reach Len. (ft)<td>* 388.00</td><td>* 420.00</td><td>* 460.00</td></td></td>	* 2384.06 <td>* Reach Len. (ft)<td>* 388.00</td><td>* 420.00</td><td>* 460.00</td></td>	* Reach Len. (ft) <td>* 388.00</td> <td>* 420.00</td> <td>* 460.00</td>	* 388.00	* 420.00	* 460.00
* Crit W.S. (ft) <td>* 2384.06<td>* Flow Area (sq ft)<td></td><td>* 114.29</td><td></td></td></td>	* 2384.06 <td>* Flow Area (sq ft)<td></td><td>* 114.29</td><td></td></td>	* Flow Area (sq ft) <td></td> <td>* 114.29</td> <td></td>		* 114.29	
* E.G. Slope (ft/ft) <td>* 0.016006<td>* Area (sq ft)<td></td><td>* 114.29</td><td></td></td></td>	* 0.016006 <td>* Area (sq ft)<td></td><td>* 114.29</td><td></td></td>	* Area (sq ft) <td></td> <td>* 114.29</td> <td></td>		* 114.29	
* Q Total (cfs) <td>* 490.00<td>* Flow (cfs)<td></td><td>* 490.00</td><td></td></td></td>	* 490.00 <td>* Flow (cfs)<td></td><td>* 490.00</td><td></td></td>	* Flow (cfs) <td></td> <td>* 490.00</td> <td></td>		* 490.00	
* Top Width (ft) <td>* 201.95<td>* Top Width (ft)<td></td><td>* 201.95</td><td></td></td></td>	* 201.95 <td>* Top Width (ft)<td></td><td>* 201.95</td><td></td></td>	* Top Width (ft) <td></td> <td>* 201.95</td> <td></td>		* 201.95	
* Vel Total (ft/s) <td>* 4.29<td>* Avg. Vel. (ft/s)<td></td><td>* 4.29</td><td></td></td></td>	* 4.29 <td>* Avg. Vel. (ft/s)<td></td><td>* 4.29</td><td></td></td>	* Avg. Vel. (ft/s) <td></td> <td>* 4.29</td> <td></td>		* 4.29	
* Max Chl Dpth (ft) <td>* 1.06<td>* Hydr. Depth (ft)<td></td><td>* 0.57</td><td></td></td></td>	* 1.06 <td>* Hydr. Depth (ft)<td></td><td>* 0.57</td><td></td></td>	* Hydr. Depth (ft) <td></td> <td>* 0.57</td> <td></td>		* 0.57	
* Conv. Total (cfs) <td>* 3873.1<td>* Conv. (cfs)<td></td><td>* 3873.1</td><td></td></td></td>	* 3873.1 <td>* Conv. (cfs)<td></td><td>* 3873.1</td><td></td></td>	* Conv. (cfs) <td></td> <td>* 3873.1</td> <td></td>		* 3873.1	
* Length Wtd. (ft) <td>* 420.00<td>* Wetted Per. (ft)<td></td><td>* 201.96</td><td></td></td></td>	* 420.00 <td>* Wetted Per. (ft)<td></td><td>* 201.96</td><td></td></td>	* Wetted Per. (ft) <td></td> <td>* 201.96</td> <td></td>		* 201.96	
* Min Ch El (ft) <td>* 2383.00<td>* Shear (lb/sq ft)<td></td><td>* 0.57</td><td></td></td></td>	* 2383.00 <td>* Shear (lb/sq ft)<td></td><td>* 0.57</td><td></td></td>	* Shear (lb/sq ft) <td></td> <td>* 0.57</td> <td></td>		* 0.57	
* Alpha <td>* 1.00<td>* Stream Power (lb/ft s)<td></td><td>* 2.42</td><td></td></td></td>	* 1.00 <td>* Stream Power (lb/ft s)<td></td><td>* 2.42</td><td></td></td>	* Stream Power (lb/ft s) <td></td> <td>* 2.42</td> <td></td>		* 2.42	
* Frctn Loss (ft) <td>* 6.50<td>* Cum Volume (acre-ft)<td>* 0.57</td><td>* 10.01</td><td>* 0.40</td></td></td>	* 6.50 <td>* Cum Volume (acre-ft)<td>* 0.57</td><td>* 10.01</td><td>* 0.40</td></td>	* Cum Volume (acre-ft) <td>* 0.57</td> <td>* 10.01</td> <td>* 0.40</td>	* 0.57	* 10.01	* 0.40
* C & E Loss (ft) <td>* 0.01<td>* Cum SA (acres)<td>* 1.06</td><td>* 10.71</td><td>* 0.63</td></td></td>	* 0.01 <td>* Cum SA (acres)<td>* 1.06</td><td>* 10.71</td><td>* 0.63</td></td>	* Cum SA (acres) <td>* 1.06</td> <td>* 10.71</td> <td>* 0.63</td>	* 1.06	* 10.71	* 0.63

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
REACH: CIG2B1 TO CIG2B2 RS: 10

INPUT

Description: Section J-J, Reach 4

Station Elevation Data		num= 31		Sta Elev		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-269.77	2371.2	-250	2371.7	-225	2371.9	-200	2372.1	-175	2372		
-150	2371	-125	2371.4	-100	2370.7	-75	2370	-50	2370		

Reach4.rep

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-25	2370.8	0	2371.5	25	2373	50	2375.4
100	2379.7	125	2380	150	2380	175	2378.9
225	2375.7	250	2372.9	269.77	2371	380	2370
470	2365	500	2365	550	2368.4	600	2365
700	2365					650	2367

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-269.77	.03	-200	.03	150	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -200 150 420 413 450 .1 .3
 Blocked Obstructions num= 2
 Sta L Sta R Elev Sta L Sta R Elev
 -269.77 -200 125 700

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2371.72	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.34	* Wt. n-Val.	* 0.030		
* W.S. Elev (ft)	* 2371.37	* Reach Len. (ft)	* 420.00	* 413.00	* 450.00
* Crit W.S. (ft)	* 2371.37	* Flow Area (sq ft)		* 104.05	
* E.G. Slope (ft/ft)	* 0.014980	* Area (sq ft)		* 104.05	
* Q Total (cfs)	* 490.00	* Flow (cfs)		* 490.00	
* Top Width (ft)	* 151.92	* Top Width (ft)		* 151.92	
* Vel Total (ft/s)	* 4.71	* Avg. Vel. (ft/s)		* 4.71	
* Max Chl Dpth (ft)	* 1.37	* Hydr. Depth (ft)		* 0.68	
* Conv. Total (cfs)	* 4003.4	* Conv. (cfs)		* 4003.4	
* Length Wtd. (ft)	* 413.00	* Wetted Per. (ft)		* 151.97	
* Min Ch El (ft)	* 2370.00	* Shear (lb/sq ft)		* 0.64	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 3.02	
* Frctn Loss (ft)	* 5.79	* Cum Volume (acre-ft)	* 0.57	* 8.96	* 0.40
* C & E Loss (ft)	* 0.02	* Cum SA (acres)	* 1.06	* 9.01	* 0.63

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: CIG2B1 TO CIG2B2 RS: 9

INPUT
 Description: Section I-I, Reach 4
 Station Elevation Data num= 27

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-294.68	2359.5	-275	2359.7	-250	2359.9	-225	2359.9	-200	2359.9
-175	2359.2	-150	2358.8	-125	2359	-100	2359.2	-75	2359.5
-50	2360	-25	2360.7	0	2361.3	25	2361.5	50	2361.1
75	2360.7	100	2360.3	125	2357.2	150	2355.2	175	2355
200	2354.3	225	2352.9	250	2353.3	275	2355.9	294.68	2357.1
400	2360	480	2360.9						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-294.68	.03	25	.03	294.68	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 25 294.68 350 403 447 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2355.28	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.53	* Wt. n-Val.	* 0.030		
* W.S. Elev (ft)	* 2354.75	* Reach Len. (ft)	* 350.00	* 403.00	* 447.00
* Crit W.S. (ft)	* 2354.75	* Flow Area (sq ft)		* 83.74	
* E.G. Slope (ft/ft)	* 0.013162	* Area (sq ft)		* 83.74	
* Q Total (cfs)	* 490.00	* Flow (cfs)		* 490.00	
* Top Width (ft)	* 80.02	* Top Width (ft)		* 80.02	
* Vel Total (ft/s)	* 5.85	* Avg. Vel. (ft/s)		* 5.85	
* Max Chl Dpth (ft)	* 1.85	* Hydr. Depth (ft)		* 1.05	
* Conv. Total (cfs)	* 4271.1	* Conv. (cfs)		* 4271.1	
* Length Wtd. (ft)	* 403.00	* Wetted Per. (ft)		* 80.15	
* Min Ch El (ft)	* 2352.90	* Shear (lb/sq ft)		* 0.86	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 5.02	
* Frctn Loss (ft)	* 5.08	* Cum Volume (acre-ft)	* 0.57	* 8.07	* 0.40
* C & E Loss (ft)	* 0.02	* Cum SA (acres)	* 1.06	* 7.91	* 0.63

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: CIG2B1 TO CIG2B2 RS: 8

INPUT
 Description: Section H-H, Reach 4
 Station Elevation Data num= 28

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-305.16	2354.4	-300	2354.3	-275	2354	-250	2353.5
-200	2352.3	-175	2351.5	-150	2350.5	-125	2349.6
-75	2345.4	-50	2346.1	-25	2346.5	0	2346.6
50	2346.1	75	2345.4	100	2345	125	2345
175	2341.4	200	2341.9	225	2345	250	2345
300	2345.6	304.82	2345.693	305.16	2345.7	275	2345

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-305.16	.03	-300	.03	300	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -300 300 412 397 383 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2344.17	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.68 <td>* Wt. n-Val.</td> <td>* 0.030</td> <td></td> <td></td>	* Wt. n-Val.	* 0.030		

		Reach4.rep	
* W.S. Elev (ft)	* 2343.49	* Reach Len. (ft)	* 412.00
* Crit W.S. (ft)	* 2343.49	* Flow Area (sq ft)	* 397.00
* E.G. Slope (ft/ft)	* 0.012078	* Area (sq ft)	* 73.88
* Q Total (cfs)	* 490.00	* Flow (cfs)	* 490.00
* Top Width (ft)	* 54.70	* Top Width (ft)	* 54.70
* Vel Total (ft/s)	* 6.63	* Avg. Vel. (ft/s)	* 6.63
* Max Chl Dpth (ft)	* 2.09	* Hydr. Depth (ft)	* 1.35
* Conv. Total (cfs)	* 4458.5	* Conv. (cfs)	* 4458.5
* Length Wtd. (ft)	* 397.00	* Wetted Per. (ft)	* 54.93
* Min Ch El (ft)	* 2341.40	* Shear (lb/sq ft)	* 1.01
* Alpha	* 1.00	* Stream Power (lb/ft s)	* 6.73
* Frctn Loss (ft)	* 4.95	* Cum Volume (acre-ft)	* 0.57
* C & E Loss (ft)	* 0.04	* Cum SA (acres)	* 1.06

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 7

INPUT
 Description: Section G-G, Reach 4
 Station Elevation Data num= 25

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-292.18	2343.5	-275	2342.7	-250	2341.3	-225	2339.6	-200	2335.7
-175	2335	-150	2335	-125	2335	-100	2335	-75	2335
-50	2335	-25	2335.2	0	2335.9	25	2336	50	2336.2
75	2336.3	100	2336.2	125	2336	150	2335.5	175	2335
200	2332.7	225	2331.6	250	2330.7	275	2332.1	292.18	2334.8

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-292.18	.03	-275	.03	292.18	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -275 292.18 422 411 404 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

		Element		Left OB		Channel		Right OB	
* E.G. Elev (ft)	* 2333.20	* Element	* 422.00	* Channel	* 404.00	* Right OB	* 404.00	* 404.00	* 404.00
* Vel Head (ft)	* 0.54	* Wt. n-Val.	* 0.030	* 0.030	* 0.030	* 0.030	* 0.030	* 0.030	* 0.030
* W.S. Elev (ft)	* 2332.66	* Reach Len. (ft)	* 422.00	* 411.00	* 411.00	* 411.00	* 411.00	* 411.00	* 411.00
* Crit W.S. (ft)	* 2332.66	* Flow Area (sq ft)	* 83.33	* 83.33	* 83.33	* 83.33	* 83.33	* 83.33	* 83.33
* E.G. Slope (ft/ft)	* 0.012883	* Area (sq ft)	* 490.00	* 490.00	* 490.00	* 490.00	* 490.00	* 490.00	* 490.00
* Q Total (cfs)	* 490.00	* Flow (cfs)	* 77.77	* 77.77	* 77.77	* 77.77	* 77.77	* 77.77	* 77.77
* Top Width (ft)	* 77.77	* Top Width (ft)	* 5.88	* 5.88	* 5.88	* 5.88	* 5.88	* 5.88	* 5.88
* Vel Total (ft/s)	* 5.88	* Avg. Vel. (ft/s)	* 1.07	* 1.07	* 1.07	* 1.07	* 1.07	* 1.07	* 1.07
* Max Chl Dpth (ft)	* 1.96	* Hydr. Depth (ft)	* 4317.1	* 4317.1	* 4317.1	* 4317.1	* 4317.1	* 4317.1	* 4317.1
* Conv. Total (cfs)	* 4317.1	* Conv. (cfs)	* 77.90	* 77.90	* 77.90	* 77.90	* 77.90	* 77.90	* 77.90
* Length Wtd. (ft)	* 411.00	* Wetted Per. (ft)	* 0.86	* 0.86	* 0.86	* 0.86	* 0.86	* 0.86	* 0.86
* Min Ch El (ft)	* 2330.70	* Shear (lb/sq ft)	* 5.06	* 5.06	* 5.06	* 5.06	* 5.06	* 5.06	* 5.06
* Alpha	* 1.00	* Stream Power (lb/ft s)	* 6.62	* 6.62	* 6.62	* 6.62	* 6.62	* 6.62	* 6.62
* Frctn Loss (ft)	* 5.24	* Cum Volume (acre-ft)	* 0.57	* 0.57	* 0.57	* 0.57	* 0.57	* 0.57	* 0.57
* C & E Loss (ft)	* 0.01	* Cum SA (acres)	* 1.06	* 1.06	* 1.06	* 1.06	* 1.06	* 1.06	* 1.06

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 6

INPUT
 Description: Section F-F, Reach 4
 Station Elevation Data num= 25

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-258.62	2326.7	-250	2326.1	-225	2324.9	-200	2322.4	-175	2322.4
-150	2323.5	-125	2325	-100	2325	-75	2325	-50	2324.5
-25	2324.1	0	2324	25	2324.4	50	2324.9	75	2325
100	2325	125	2322.8	150	2320	175	2321	200	2323.5
225	2326.2	250	2329.4	258.62	2330	300	2332.7	370	2330

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-258.62	.03	-250	.03	250	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -250 250 350 414 470 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

		Element		Left OB		Channel		Right OB	
* E.G. Elev (ft)	* 2323.47	* Element	* 350.00	* Channel	* 470.00	* Right OB	* 470.00	* 470.00	* 470.00
* Vel Head (ft)	* 0.60	* Wt. n-Val.	* 0.030	* 0.030	* 0.030	* 0.030	* 0.030	* 0.030	* 0.030
* W.S. Elev (ft)	* 2322.87	* Reach Len. (ft)	* 414.00	* 414.00	* 414.00	* 414.00	* 414.00	* 414.00	* 414.00
* Crit W.S. (ft)	* 2322.87	* Flow Area (sq ft)	* 129.00	* 129.00	* 129.00	* 129.00	* 129.00	* 129.00	* 129.00
* E.G. Slope (ft/ft)	* 0.012682	* Area (sq ft)	* 799.00	* 799.00	* 799.00	* 799.00	* 799.00	* 799.00	* 799.00
* Q Total (cfs)	* 799.00	* Flow (cfs)	* 109.94	* 109.94	* 109.94	* 109.94	* 109.94	* 109.94	* 109.94
* Top Width (ft)	* 109.94	* Top Width (ft)	* 6.19	* 6.19	* 6.19	* 6.19	* 6.19	* 6.19	* 6.19
* Vel Total (ft/s)	* 6.19	* Avg. Vel. (ft/s)	* 1.17	* 1.17	* 1.17	* 1.17	* 1.17	* 1.17	* 1.17
* Max Chl Dpth (ft)	* 2.87	* Hydr. Depth (ft)	* 7095.0	* 7095.0	* 7095.0	* 7095.0	* 7095.0	* 7095.0	* 7095.0
* Conv. Total (cfs)	* 7095.0	* Conv. (cfs)	* 110.24	* 110.24	* 110.24	* 110.24	* 110.24	* 110.24	* 110.24
* Length Wtd. (ft)	* 414.00	* Wetted Per. (ft)	* 0.93	* 0.93	* 0.93	* 0.93	* 0.93	* 0.93	* 0.93
* Min Ch El (ft)	* 2320.00	* Shear (lb/sq ft)	* 5.74	* 5.74	* 5.74	* 5.74	* 5.74	* 5.74	* 5.74
* Alpha	* 1.00	* Stream Power (lb/ft s)	* 5.62	* 5.62	* 5.62	* 5.62	* 5.62	* 5.62	* 5.62
* Frctn Loss (ft)	* 5.13	* Cum Volume (acre-ft)	* 0.57	* 0.57	* 0.57	* 0.57	* 0.57	* 0.57	* 0.57
* C & E Loss (ft)	* 0.01	* Cum SA (acres)	* 1.06	* 1.06	* 1.06	* 1.06	* 1.06	* 1.06	* 1.06

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 5

INPUT

Description: Section E-E, Reach 4

Station Elevation Data		num= 19		Sta Elev		Sta Elev		Sta Elev		Sta Elev	
-187.5	2314.7	-175	2314.8	-150	2314.7	-125	2314.7	-100	2314.6		
-75	2314.7	-50	2315	-25	2315	0	2314.4	25	2315.5		
50	2312.2	75	2310.4	100	2310	125	2310	150	2312.2		
175	2314.4	187.5	2315.5	250	2320	330	2320.6				

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 -187.5 .03 25 .03 187.5 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 25 187.5 500 401 480 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)		* 2312.52		* Element		* Left OB		* Channel		* Right OB	
* Vel Head (ft)	* 0.67	* wt. n-Val.									
* W.S. Elev (ft)	* 2311.85	* Reach Len. (ft)				500.00		401.00		480.00	
* Crit W.S. (ft)	* 2311.85	* Flow Area (sq ft)						121.25			
* E.G. Slope (ft/ft)	* 0.012111	* Area (sq ft)						121.25			
* Q Total (cfs)	* 799.00	* Flow (cfs)						799.00			
* Top Width (ft)	* 91.08	* Top Width (ft)						91.08			
* Vel Total (ft/s)	* 6.59	* Avg. Vel. (ft/s)						6.59			
* Max chl Dpth (ft)	* 1.85	* Hydr. Depth (ft)						1.33			
* Conv. Total (cfs)	* 7260.2	* Conv. (cfs)						7260.2			
* Length Wtd (ft)	* 401.00	* Wetted Per. (ft)						91.22			
* Min Ch El (ft)	* 2310.00	* Shear (lb/sq ft)						1.01			
* Alpha	* 1.00	* Stream Power (lb/ft s)						6.62			
* Frctn Loss (ft)	* 5.59	* Cum Volume (acre-ft)				0.57		4.43		0.40	
* C & E Loss (ft)	* 0.11	* Cum SA (acres)				1.06		4.84		0.63	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 4

INPUT

Description: Section D-D, Reach 4

Station Elevation Data		num= 20		Sta Elev		Sta Elev		Sta Elev		Sta Elev	
-450	2308.2	-300	2305	-220	2298.3	-188.96	2300.5	-175	2300.6		
-150	2300.8	-125	2300.1	-100	2300.3	-75	2300.6	-50	2300.8		
-25	2301	0	2300.3	25	2300	50	2300.4	75	2301.5		
100	2302.6	125	2303.8	150	2305	175	2308.5	188.97	2310		

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 -450 .03 -300 .03 175 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -300 175 403 437 470 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)		* 2301.18		* Element		* Left OB		* Channel		* Right OB	
* Vel Head (ft)	* 0.32	* wt. n-Val.									
* W.S. Elev (ft)	* 2300.86	* Reach Len. (ft)				403.00		437.00		470.00	
* Crit W.S. (ft)	* 2300.86	* Flow Area (sq ft)						176.06			
* E.G. Slope (ft/ft)	* 0.016227	* Area (sq ft)						176.06			
* Q Total (cfs)	* 799.00	* Flow (cfs)						799.00			
* Top Width (ft)	* 288.40	* Top Width (ft)						288.40			
* Vel Total (ft/s)	* 4.54	* Avg. Vel. (ft/s)						4.54			
* Max chl Dpth (ft)	* 2.56	* Hydr. Depth (ft)						0.61			
* Conv. Total (cfs)	* 6272.3	* Conv. (cfs)						6272.3			
* Length Wtd (ft)	* 436.56	* Wetted Per. (ft)						288.62			
* Min Ch El (ft)	* 2298.30	* Shear (lb/sq ft)						0.62			
* Alpha	* 1.00	* Stream Power (lb/ft s)						2.80			
* Frctn Loss (ft)	* 4.40	* Cum Volume (acre-ft)				0.57		3.07		0.40	
* C & E Loss (ft)	* 0.01	* Cum SA (acres)				1.06		3.09		0.63	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: Divided flow computed for this cross-section.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 3

INPUT

Description: Section C-C, Reach 4

Station Elevation Data		num= 24		Sta Elev		Sta Elev		Sta Elev		Sta Elev	
-350	2295	-262.19	2290.9	-250	2290.7	-225	2290.4	-200	2290		
-175	2290	-150	2290	-125	2288	-100	2290	-75	2290		
-50	2290	-25	2291	0	2292	25	2292.9	50	2293.9		
75	2294.8	100	2296	125	2297.1	150	2297.6	175	2298.1		
200	2298.7	225	2298.8	250	2299.5	262.2	2299.8				

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 -350 .03 -150 .03 -100 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft)      * 2291.14 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)      * 0.40  * Wt. n-Val.  * 0.030  * 0.030  * 0.030  *
* W.S. Elev (ft)      * 2290.74 * Reach Len. (ft) * 502.00 * 401.00 * 330.00 *
* Crit W.S. (ft)      * 2290.74 * Flow Area (sq ft) * 55.33  * 87.01  * 43.86  *
* E.G. Slope (ft/ft)  * 0.006852 * Area (sq ft)    * 55.33  * 87.01  * 43.86  *
* Q Total (cfs)       * 799.00  * Flow (cfs)      * 150.41 * 515.03 * 133.56 *
* Top Width (ft)      * 220.96  * Top Width (ft)   * 102.46 * 50.00  * 68.51  *
* Vel Total (ft/s)    * 4.29    * Avg. Vel. (ft/s) * 2.72   * 5.92   * 3.05   *
* Max Chl Dpth (ft)   * 2.74    * Hydr. Depth (ft) * 0.54   * 1.74   * 0.64   *
* Conv. Total (cfs)   * 9652.7  * Conv. (cfs)      * 1817.1 * 6222.0 * 1613.6 *
* Length Wtd. (ft)    * 404.57  * Wetted Per. (ft) * 102.46 * 50.16  * 68.52  *
* Min Ch El (ft)      * 2288.00 * Shear (lb/sq ft) * 0.23   * 4.39   * 0.83   *
* Alpha              * 1.39    * Stream Power (lb/ft s) * 0.63   * 4.39   * 0.83   *
* Frctn Loss (ft)     * 3.51    * Cum Volume (acre-ft) * 0.32   * 1.75   * 0.17   *
* C & E Loss (ft)     * 0.04    * Cum SA (acres)    * 0.59   * 1.40   * 0.26   *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 2

INPUT
 Description: Section B-B, Reach 4
 Station Elevation Data num= 21

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-244.72	2277.8	-225	2278.7	-200	2280	-175	2280
-125	2277.3	-100	2275	-75	2275.7	-50	2280
0	2281.2	25	2282.3	50	2284.3	75	2285
125	2285.7	150	2286.2	175	2286.7	200	2287.3
244.72	2288.6					225	2288

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-244.72	.03	-200	.03	-50	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

Left	Right	Lengths	Left Channel	Right	Coeff Contr.	Expan.
-200	-50		301	275	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft)      * 2278.52 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)      * 0.84  * Wt. n-Val.  * 0.030  * 0.030  * 0.030  *
* W.S. Elev (ft)      * 2277.68 * Reach Len. (ft) * 301.00 * 275.00 * 254.00 *
* Crit W.S. (ft)      * 2277.68 * Flow Area (sq ft) * 108.65 * 108.65 * 108.65 *
* E.G. Slope (ft/ft)  * 0.01367 * Area (sq ft)    * 108.65 * 108.65 * 108.65 *
* Q Total (cfs)       * 799.00  * Flow (cfs)      * 799.00 * 799.00 * 799.00 *
* Top Width (ft)      * 65.81  * Top Width (ft)   * 65.81  * 65.81  * 65.81  *
* Vel Total (ft/s)    * 7.35   * Avg. Vel. (ft/s) * 7.35   * 7.35   * 7.35   *
* Max Chl Dpth (ft)   * 2.68   * Hydr. Depth (ft) * 1.65   * 1.65   * 1.65   *
* Conv. Total (cfs)   * 7494.2 * Conv. (cfs)      * 7494.2 * 7494.2 * 7494.2 *
* Length Wtd. (ft)    * 275.00 * Wetted Per. (ft) * 66.11  * 66.11  * 66.11  *
* Min Ch El (ft)      * 2275.00 * Shear (lb/sq ft) * 1.17   * 1.17   * 1.17   *
* Alpha              * 1.00    * Stream Power (lb/ft s) * 8.58   * 8.58   * 8.58   *
* Frctn Loss (ft)     * 3.54    * Cum Volume (acre-ft) * 0.85   * 0.85   * 0.85   *
* C & E Loss (ft)     * 0.13    * Cum SA (acres)    * 0.86   * 0.86   * 0.86   *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Reach 4
 REACH: C1G2B1 TO C1G2B2 RS: 1

INPUT
 Description: Section A-A, Reach 4
 Station Elevation Data num= 20

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-244.13	2279.8	-225	2279.5	-200	2278.1	-175	2275.4
-125	2264	-100	2263.6	-75	2265	-50	2265
25	2265	50	2265	75	2265.6	100	2274
150	2276.4	175	2277.3	200	2278.3	225	2280

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-244.13	.03	-225	.03	225	.03

Bank Sta: Left Right Coeff Contr. Expan.

Left	Right	Coeff Contr.	Expan.
-225	225	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft)      * 2265.95 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)      * 0.39  * Wt. n-Val.  * 0.030  * 0.030  * 0.030  *
* W.S. Elev (ft)      * 2265.56 * Reach Len. (ft) * 159.13 * 159.13 * 159.13 *
* Crit W.S. (ft)      * 2265.56 * Flow Area (sq ft) * 159.13 * 159.13 * 159.13 *
* E.G. Slope (ft/ft)  * 0.014663 * Area (sq ft)    * 159.13 * 159.13 * 159.13 *
* Q Total (cfs)       * 799.00  * Flow (cfs)      * 799.00 * 799.00 * 799.00 *
* Top Width (ft)      * 207.58 * Top Width (ft)   * 207.58 * 207.58 * 207.58 *
* Vel Total (ft/s)    * 5.02   * Avg. Vel. (ft/s) * 5.02   * 5.02   * 5.02   *
* Max Chl Dpth (ft)   * 1.96   * Hydr. Depth (ft) * 1.77   * 1.77   * 1.77   *
* Conv. Total (cfs)   * 6598.3 * Conv. (cfs)      * 6598.3 * 6598.3 * 6598.3 *
* Length Wtd. (ft)    * 207.76 * Wetted Per. (ft) * 207.76 * 207.76 * 207.76 *
* Min Ch El (ft)      * 2263.60 * Shear (lb/sq ft) * 0.70   * 0.70   * 0.70   *
* Alpha              * 1.00    * Stream Power (lb/ft s) * 3.52   * 3.52   * 3.52   *
* Frctn Loss (ft)     * 1.00    * Cum Volume (acre-ft) * 3.52   * 3.52   * 3.52   *
* C & E Loss (ft)     * 0.13    * Cum SA (acres)    * 0.86   * 0.86   * 0.86   *
*****

```

Warning: Slope too steep for slope area to converge during supercritical flow calculations (normal depth is below critical depth). Water surface set to critical depth.

SUMMARY OF MANNING'S N VALUES

River: Reach 4

```

*****
* Reach * River Sta. * n1 * n2 * n3 *
*****
*ClG2B1 TO ClG2B2* 25 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 24 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 23 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 22 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 21 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 20 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 19 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 18 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 17 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 16 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 15 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 14 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 13 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 12 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 11 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 10 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 9 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 8 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 7 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 6 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 5 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 4 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 3 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 2 * .03* .03* .03*
*ClG2B1 TO ClG2B2* 1 * .03* .03* .03*
*****

```

SUMMARY OF REACH LENGTHS

River: Reach 4

```

*****
* Reach * River Sta. * Left * Channel * Right *
*****
*ClG2B1 TO ClG2B2* 25 * 550* 550* 550*
*ClG2B1 TO ClG2B2* 24 * 400* 400* 400*
*ClG2B1 TO ClG2B2* 23 * 300* 300* 300*
*ClG2B1 TO ClG2B2* 22 * 333* 386* 355*
*ClG2B1 TO ClG2B2* 21 * 300* 400* 450*
*ClG2B1 TO ClG2B2* 20 * 700* 500* 400*
*ClG2B1 TO ClG2B2* 19 * 400* 409* 430*
*ClG2B1 TO ClG2B2* 18 * 400* 399* 400*
*ClG2B1 TO ClG2B2* 17 * 400* 431* 528*
*ClG2B1 TO ClG2B2* 16 * 440* 414* 400*
*ClG2B1 TO ClG2B2* 15 * 250* 561* 650*
*ClG2B1 TO ClG2B2* 14 * 700* 397* 370*
*ClG2B1 TO ClG2B2* 13 * 368* 410* 454*
*ClG2B1 TO ClG2B2* 12 * 519* 440* 373*
*ClG2B1 TO ClG2B2* 11 * 388* 420* 460*
*ClG2B1 TO ClG2B2* 10 * 420* 413* 450*
*ClG2B1 TO ClG2B2* 9 * 350* 403* 447*
*ClG2B1 TO ClG2B2* 8 * 412* 397* 383*
*ClG2B1 TO ClG2B2* 7 * 422* 411* 404*
*ClG2B1 TO ClG2B2* 6 * 350* 414* 470*
*ClG2B1 TO ClG2B2* 5 * 500* 401* 480*
*ClG2B1 TO ClG2B2* 4 * 403* 437* 470*
*ClG2B1 TO ClG2B2* 3 * 502* 401* 330*
*ClG2B1 TO ClG2B2* 2 * 301* 275* 254*
*ClG2B1 TO ClG2B2* 1 * * * *
*****

```

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Reach 4

```

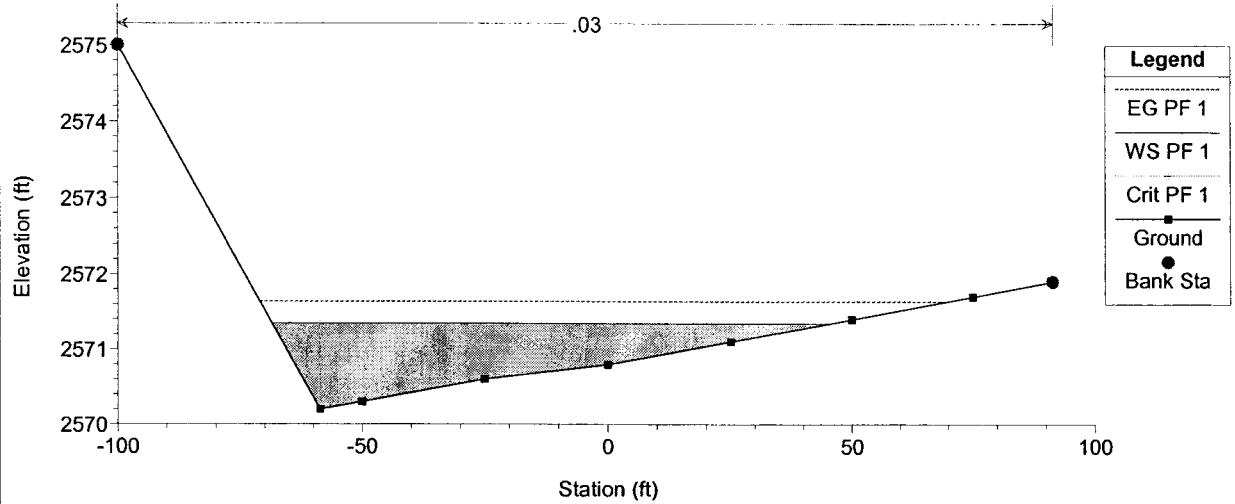
*****
* Reach * River Sta. * Contr. * Expan. *
*****
*ClG2B1 TO ClG2B2* 25 * .1* .3*
*ClG2B1 TO ClG2B2* 24 * .1* .3*
*ClG2B1 TO ClG2B2* 23 * .1* .3*
*ClG2B1 TO ClG2B2* 22 * .1* .3*
*ClG2B1 TO ClG2B2* 21 * .1* .3*
*ClG2B1 TO ClG2B2* 20 * .1* .3*
*ClG2B1 TO ClG2B2* 19 * .1* .3*
*ClG2B1 TO ClG2B2* 18 * .1* .3*
*ClG2B1 TO ClG2B2* 17 * .1* .3*
*ClG2B1 TO ClG2B2* 16 * .1* .3*
*ClG2B1 TO ClG2B2* 15 * .1* .3*
*ClG2B1 TO ClG2B2* 14 * .1* .3*
*ClG2B1 TO ClG2B2* 13 * .1* .3*
*ClG2B1 TO ClG2B2* 12 * .1* .3*
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*ClG2B1 TO ClG2B2* 9 * .1* .3*
*ClG2B1 TO ClG2B2* 8 * .1* .3*
*ClG2B1 TO ClG2B2* 7 * .1* .3*
*ClG2B1 TO ClG2B2* 6 * .1* .3*
*ClG2B1 TO ClG2B2* 5 * .1* .3*
*ClG2B1 TO ClG2B2* 4 * .1* .3*
*ClG2B1 TO ClG2B2* 3 * .1* .3*
*ClG2B1 TO ClG2B2* 2 * .1* .3*
*ClG2B1 TO ClG2B2* 1 * .1* .3*
*****

```

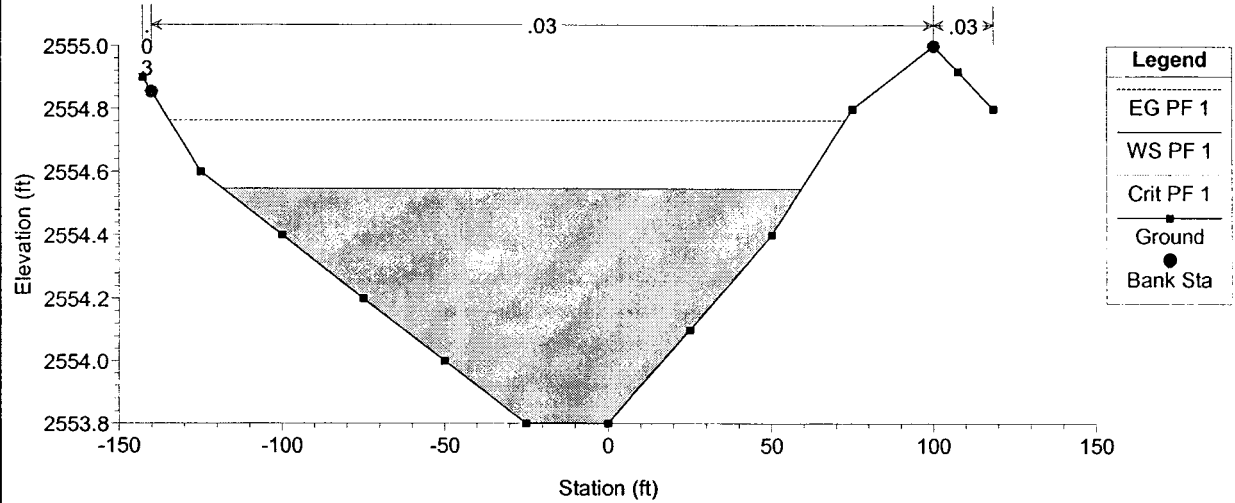
HEC-RAS Plan: Reach 6 River: Reach 4 Reach: C1G2B1 TO C1G2B2 Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
C1G2B1 TO C1G2B2	25	PF 1	286.00	2570.20	2571.34	2571.34	2571.64	0.015979	4.34	65.83	113.81	1.01
C1G2B1 TO C1G2B2	24	PF 1	286.00	2553.80	2554.55	2554.55	2554.76	0.017628	3.75	76.29	177.26	1.01
C1G2B1 TO C1G2B2	23	PF 1	286.00	2544.10	2544.68	2544.68	2544.88	0.018204	3.63	78.89	199.53	1.01
C1G2B1 TO C1G2B2	22	PF 1	286.00	2534.10	2534.89	2534.89	2535.10	0.018293	3.69	77.56	189.93	1.02
C1G2B1 TO C1G2B2	21	PF 1	286.00	2523.80	2524.37	2524.37	2524.57	0.018756	3.55	80.52	212.49	1.02
C1G2B1 TO C1G2B2	20	PF 1	286.00	2509.90	2510.44	2510.44	2510.65	0.017889	3.63	78.89	194.84	1.00
C1G2B1 TO C1G2B2	19	PF 1	286.00	2493.90	2494.91	2494.91	2495.00	0.006242	2.74	153.76	807.88	0.63
C1G2B1 TO C1G2B2	18	PF 1	286.00	2477.40	2478.59	2478.59	2478.90	0.015925	4.43	64.56	108.18	1.01
C1G2B1 TO C1G2B2	17	PF 1	286.00	2465.00	2465.60	2465.60	2465.77	0.014097	3.47	93.07	295.09	0.91
C1G2B1 TO C1G2B2	16	PF 1	286.00	2452.10	2453.08	2453.08	2453.38	0.015929	4.40	64.98	109.97	1.01
C1G2B1 TO C1G2B2	15	PF 1	286.00	2440.00	2440.60	2440.60	2440.84	0.016917	3.93	72.79	152.83	1.00
C1G2B1 TO C1G2B2	14	PF 1	286.00	2429.70	2430.47	2430.47	2430.65	0.018458	3.43	83.39	229.15	1.00
C1G2B1 TO C1G2B2	13	PF 1	286.00	2410.00	2410.80	2410.80	2411.09	0.015952	4.32	66.15	115.09	1.01
C1G2B1 TO C1G2B2	12	PF 1	286.00	2398.60	2399.08	2399.08	2399.25	0.019361	3.27	87.45	267.49	1.01
C1G2B1 TO C1G2B2	11	PF 1	490.00	2383.00	2384.06	2384.06	2384.34	0.016006	4.29	114.29	201.95	1.00
C1G2B1 TO C1G2B2	10	PF 1	490.00	2370.00	2371.37	2371.37	2371.72	0.014980	4.71	104.05	151.92	1.00
C1G2B1 TO C1G2B2	9	PF 1	490.00	2352.90	2354.75	2354.75	2355.28	0.013162	5.85	83.74	80.02	1.01
C1G2B1 TO C1G2B2	8	PF 1	490.00	2341.40	2343.49	2343.49	2344.17	0.012078	6.63	73.88	54.70	1.01
C1G2B1 TO C1G2B2	7	PF 1	490.00	2330.70	2332.66	2332.66	2333.20	0.012883	5.88	83.33	77.77	1.00
C1G2B1 TO C1G2B2	6	PF 1	799.00	2320.00	2322.87	2322.87	2323.47	0.012682	6.19	129.00	109.94	1.01
C1G2B1 TO C1G2B2	5	PF 1	799.00	2310.00	2311.85	2311.85	2312.52	0.012111	6.59	121.25	91.08	1.01
C1G2B1 TO C1G2B2	4	PF 1	799.00	2298.30	2300.86	2300.86	2301.18	0.016227	4.54	176.06	288.40	1.02
C1G2B1 TO C1G2B2	3	PF 1	799.00	2288.00	2290.74	2290.74	2291.14	0.006852	5.92	186.20	220.96	0.79
C1G2B1 TO C1G2B2	2	PF 1	799.00	2275.00	2277.68	2277.68	2278.52	0.011367	7.35	108.65	65.81	1.01
C1G2B1 TO C1G2B2	1	PF 1	799.00	2263.60	2265.56	2265.56	2265.95	0.014663	5.02	159.13	207.58	1.01

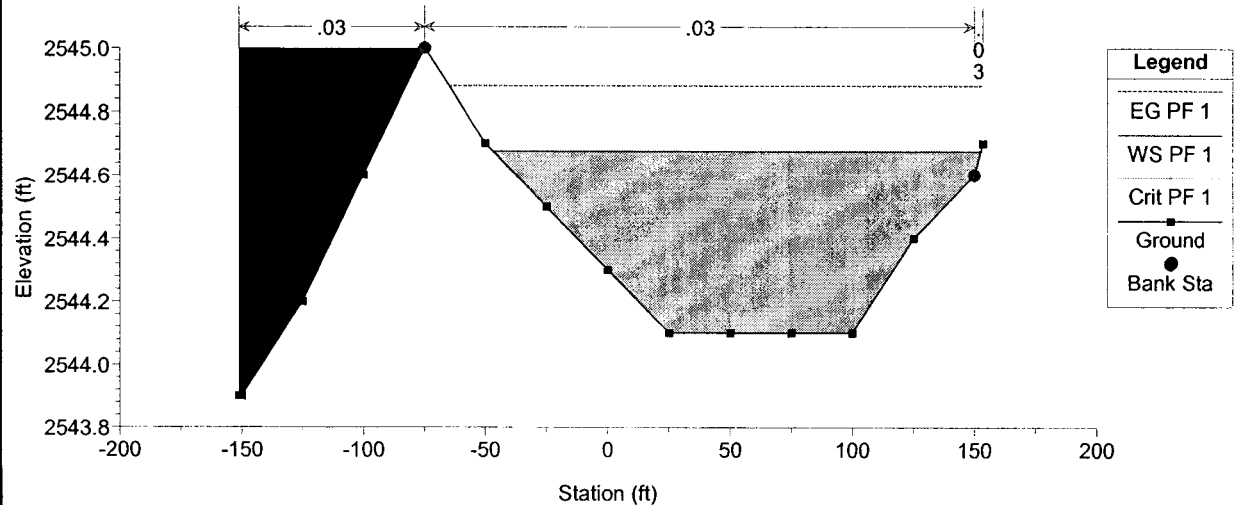
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section Y-Y, Reach 4



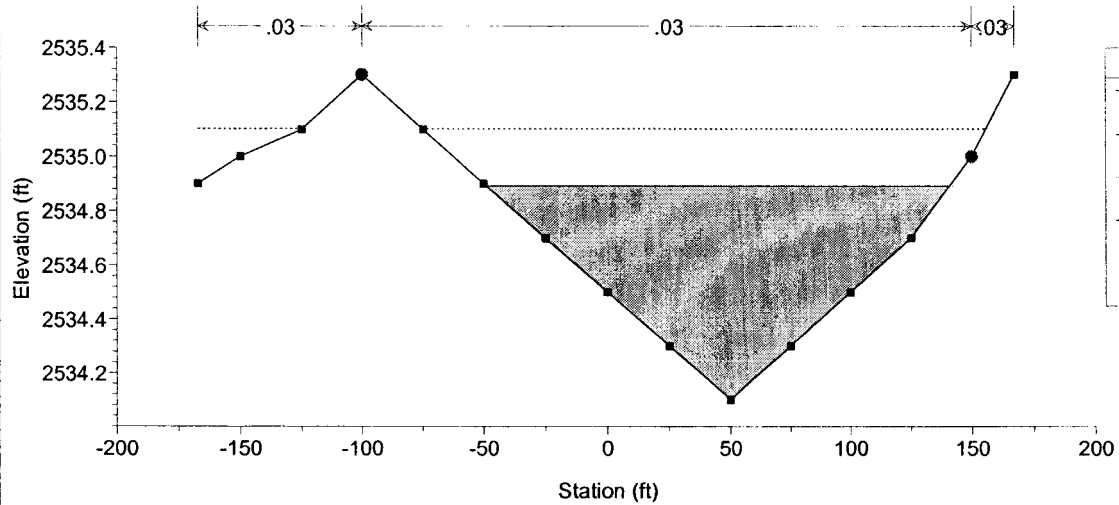
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Section X-X, Reach 4



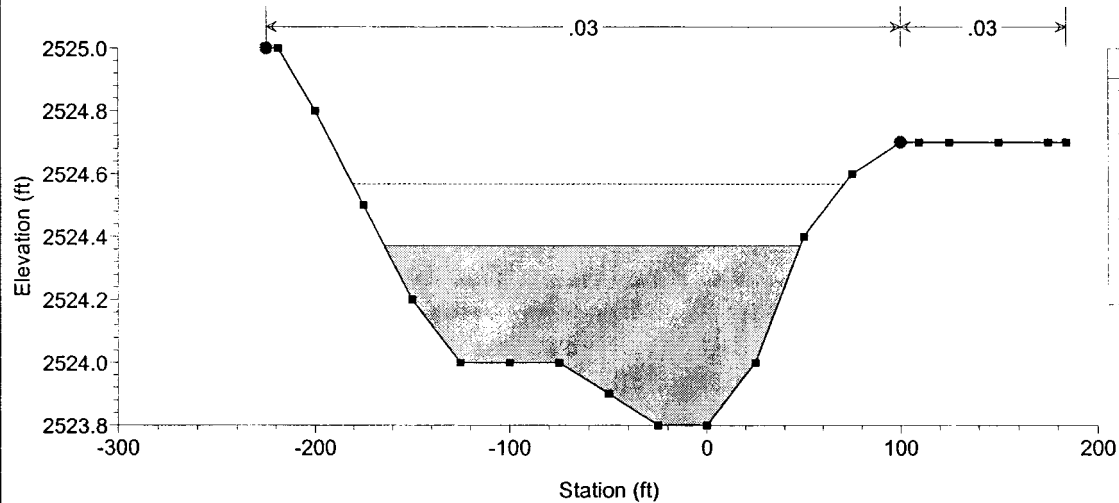
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section W-W, Reach 4



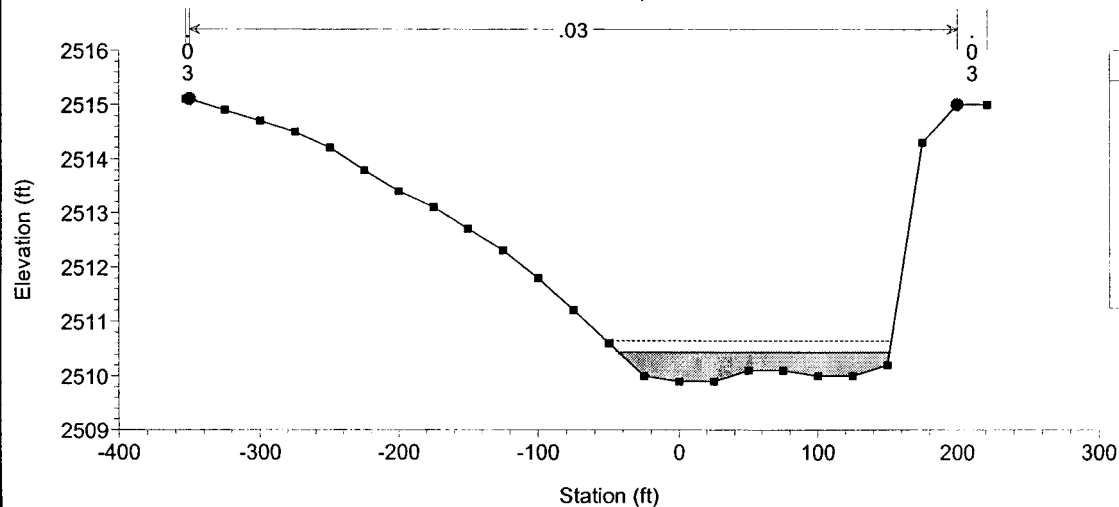
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section V-V, Reach 4



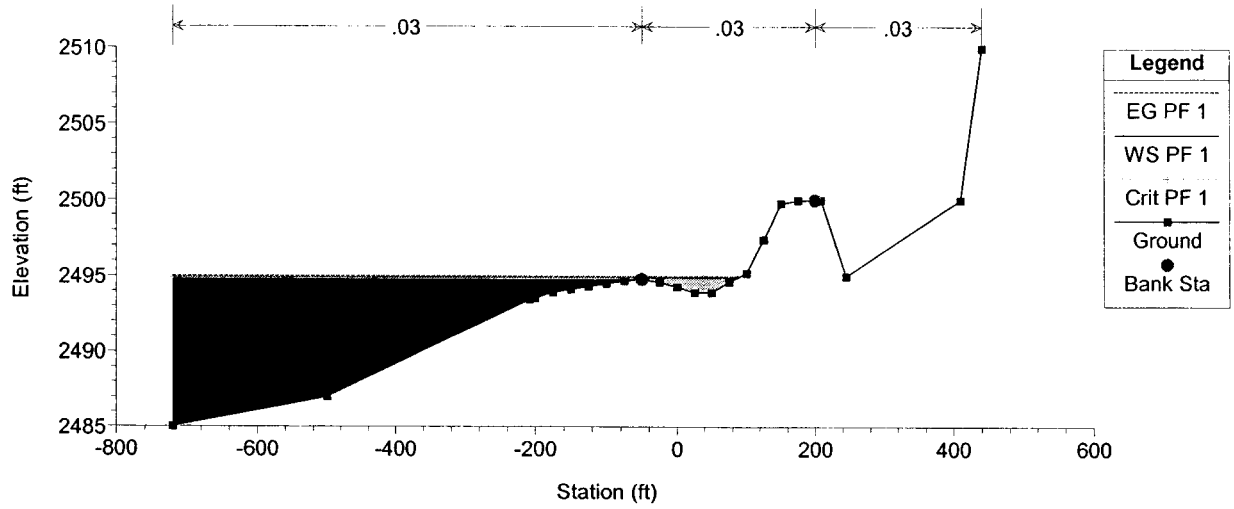
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section U-U, Reach 4



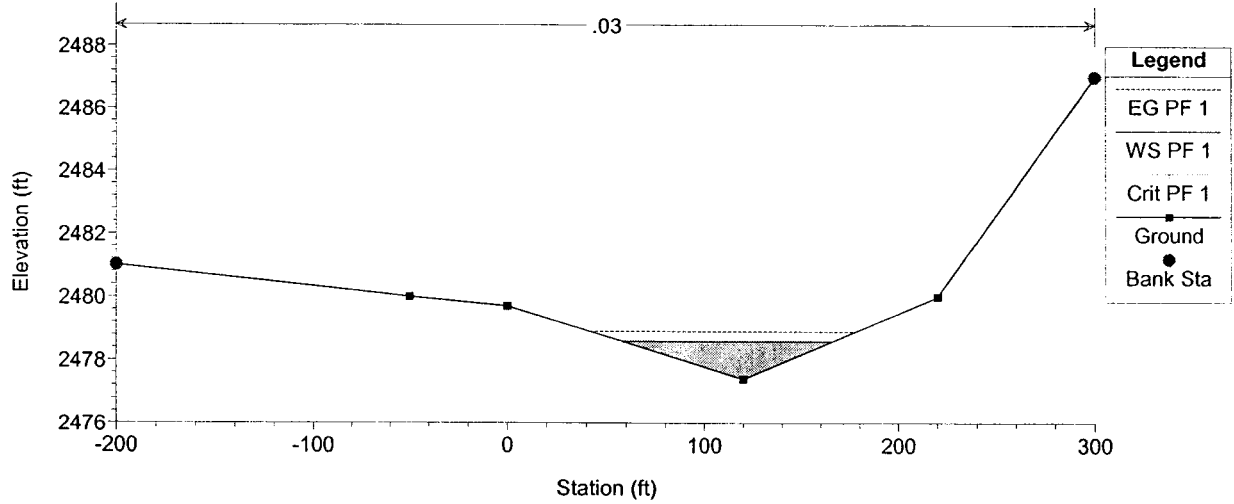
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section T-T, Reach 4



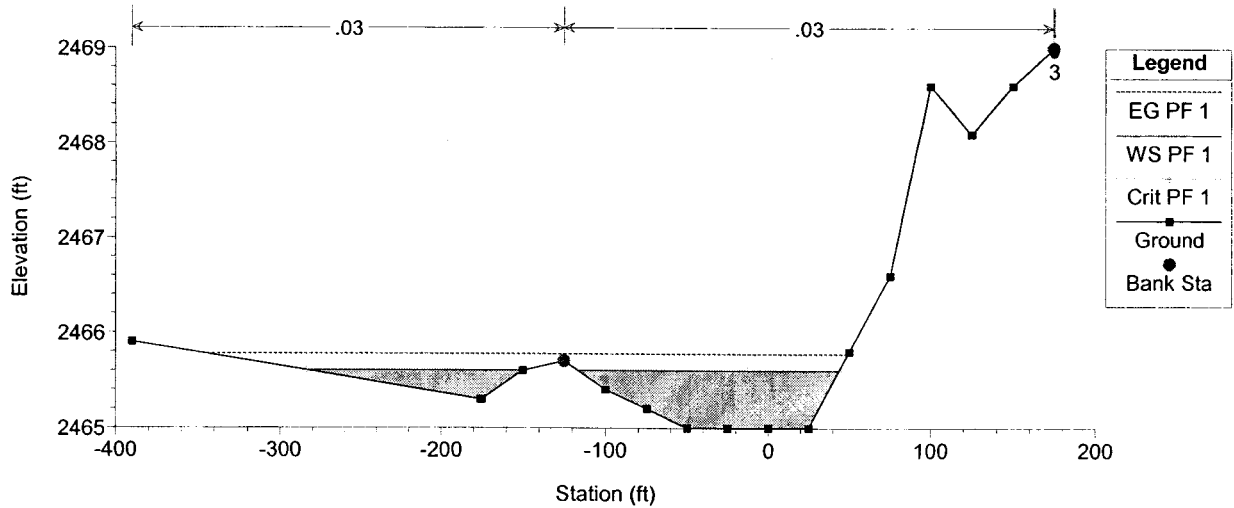
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section S-S, Reach 4



C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section R-R, Reach 4

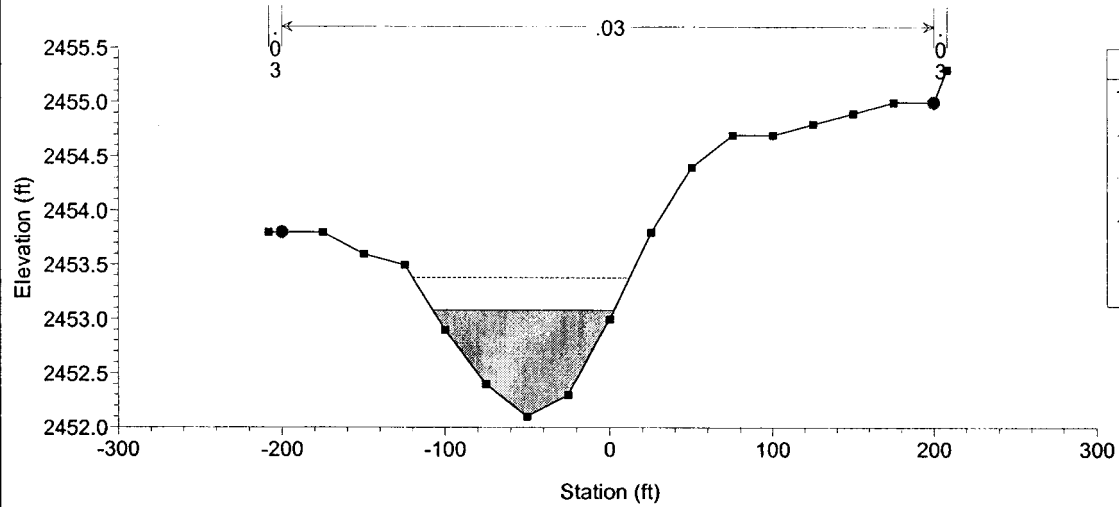


C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section Q-Q, Reach 4



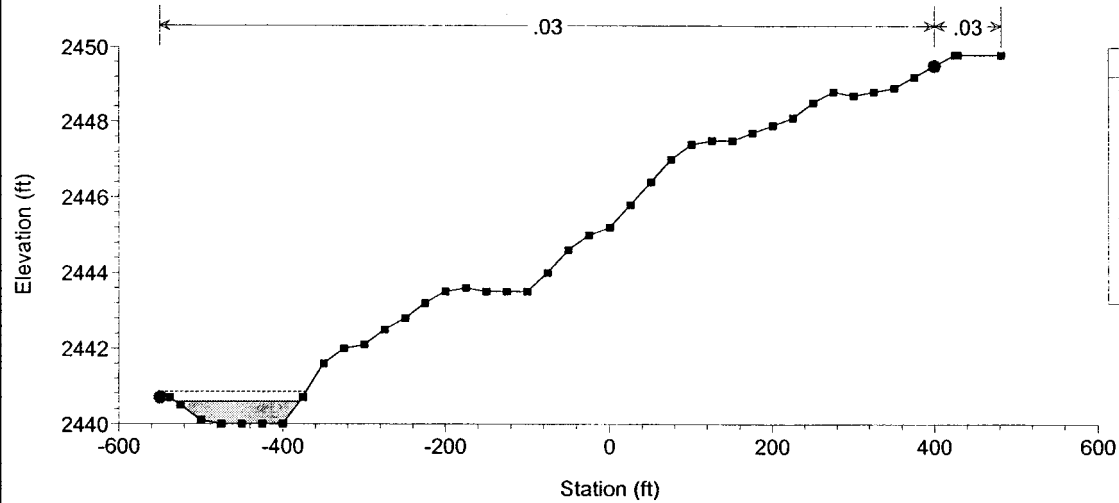
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005

Section P-P, Reach



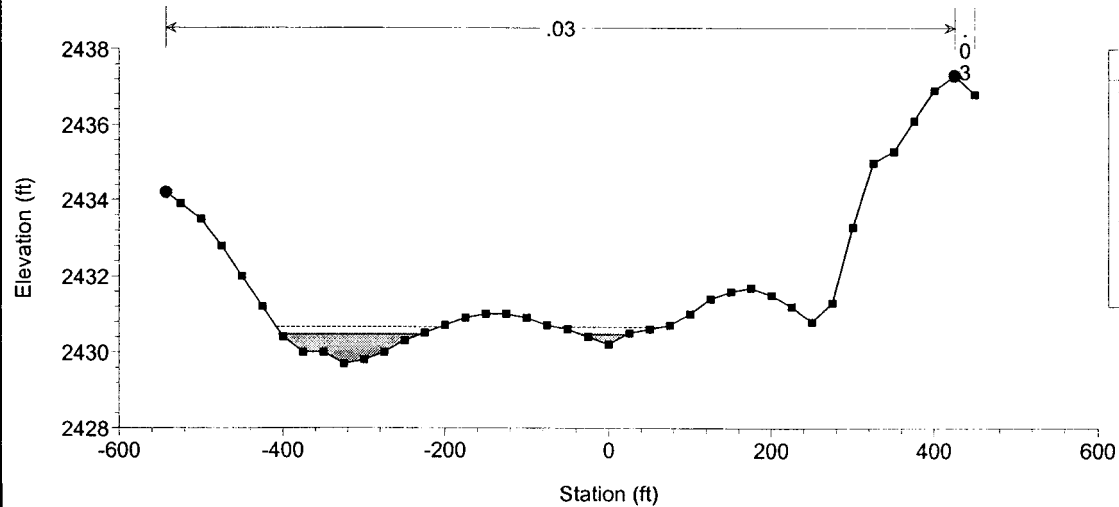
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005

Section O-O, Reach 4

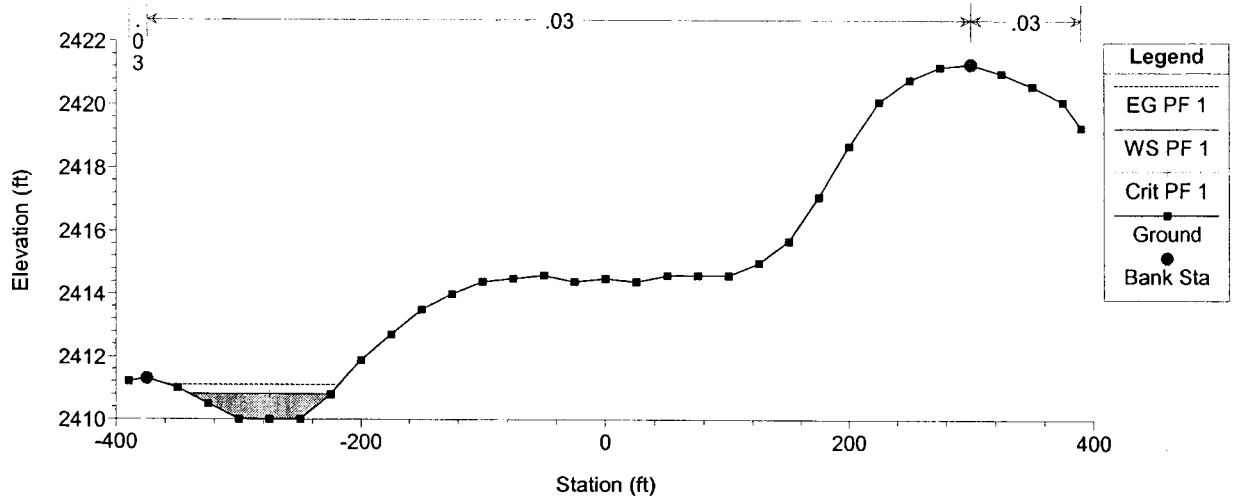


C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005

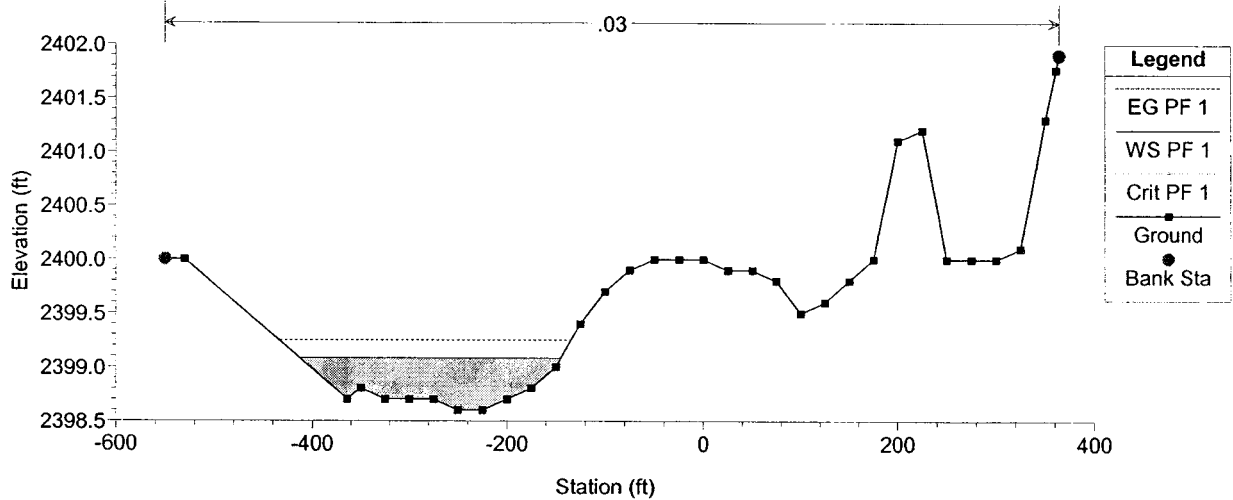
Section N-N, Reach 4



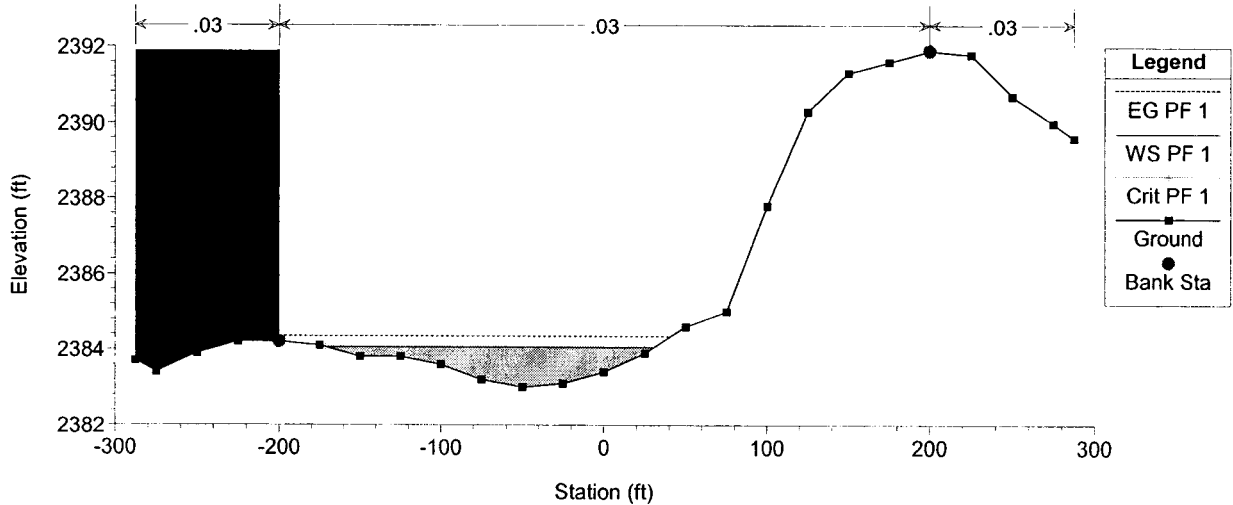
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Section M-M, Reach 4



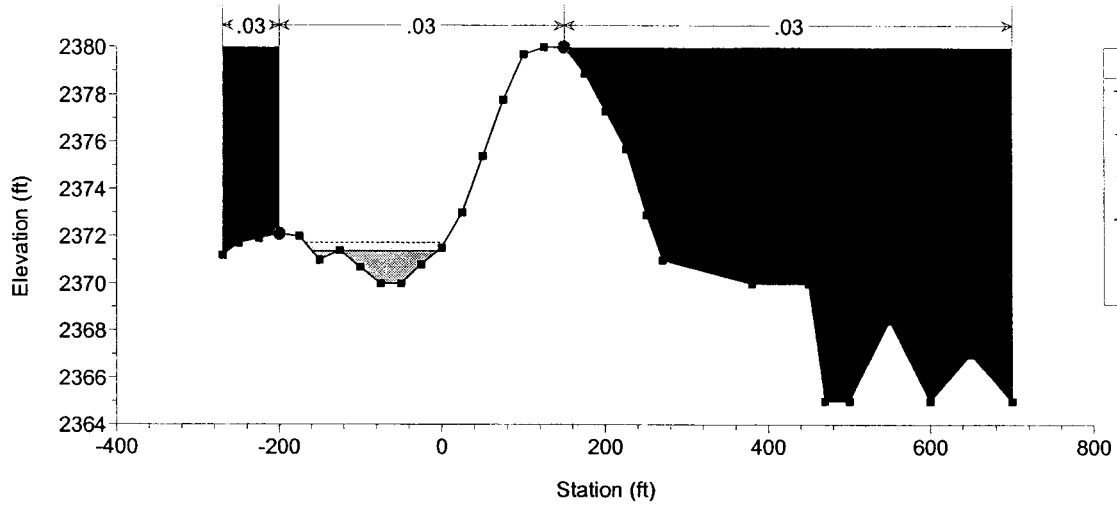
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section L-L, Reach 4



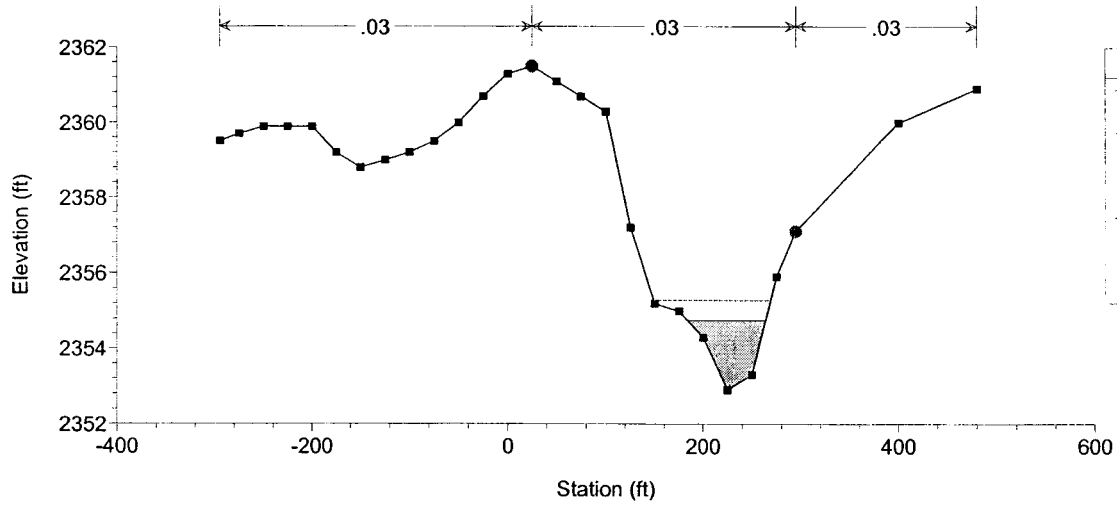
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section K-K, Reach 4



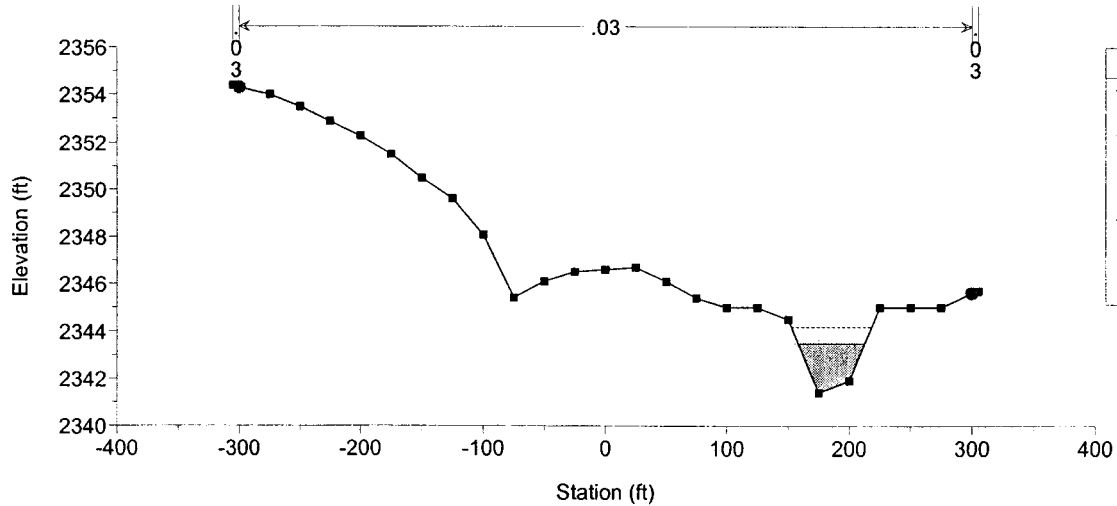
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section J-J, Reach 4



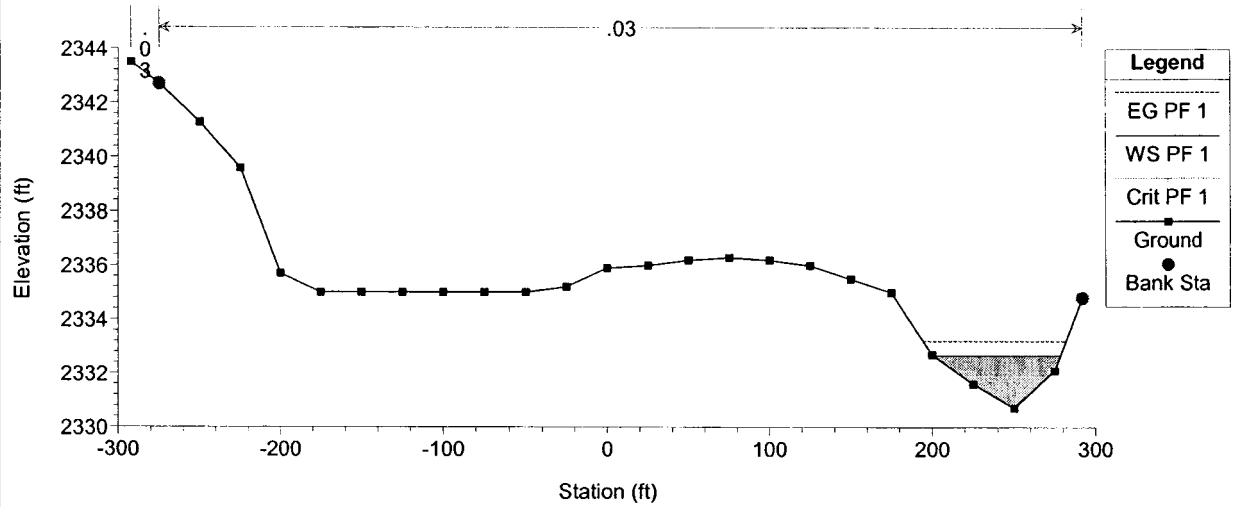
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section I-I, Reach 4



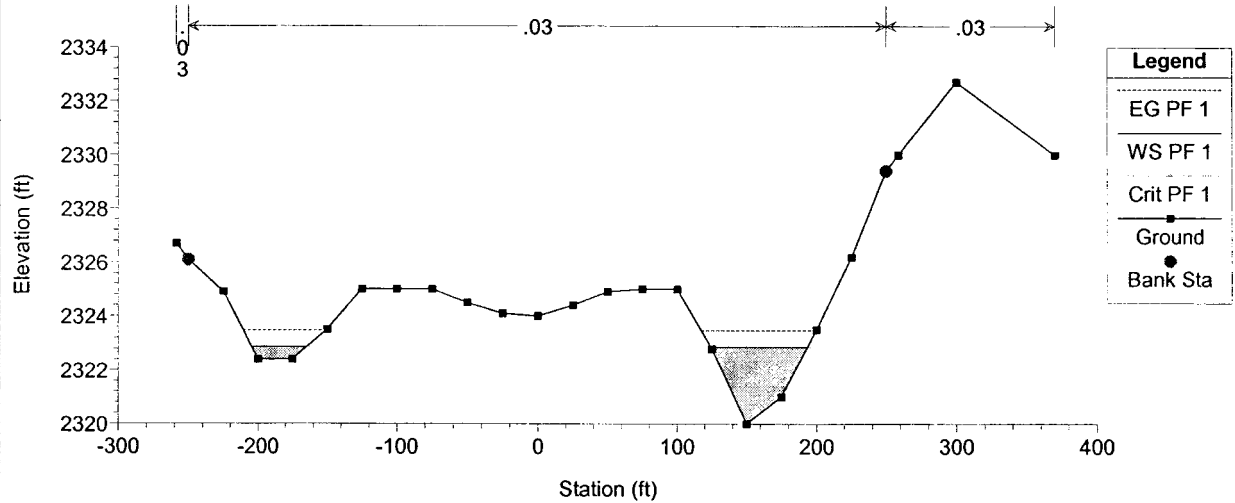
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section H-H, Reach 4



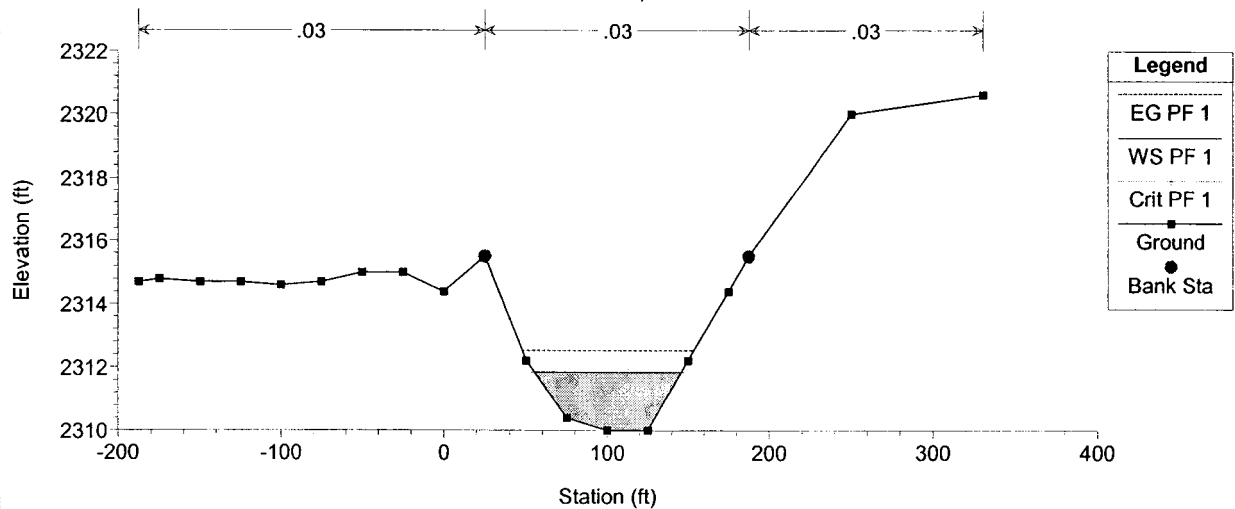
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section G-G, Reach 4



C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section F-F, Reach 4

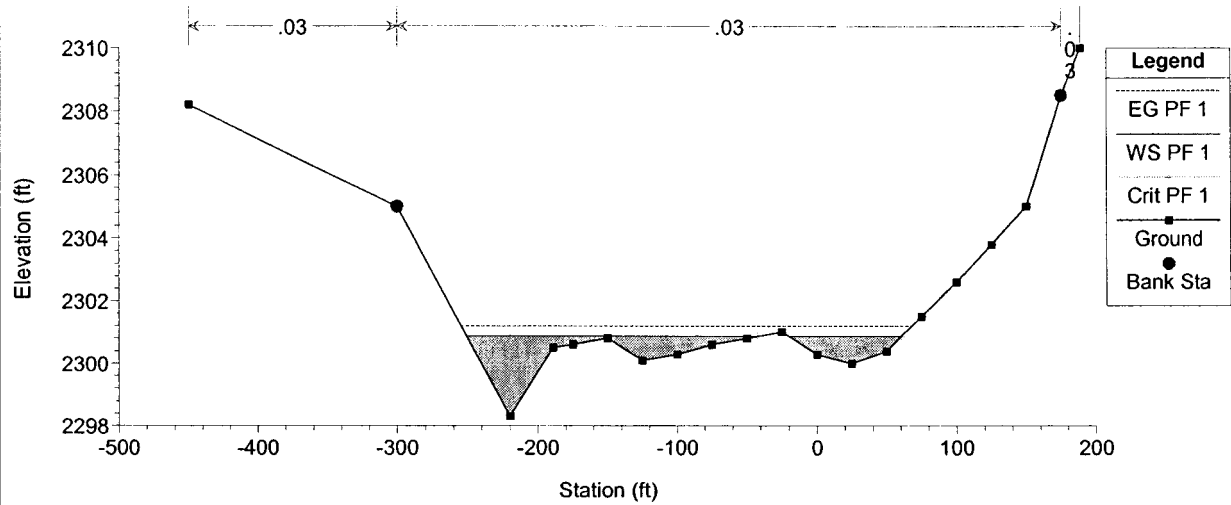


C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section E-E, Reach 4



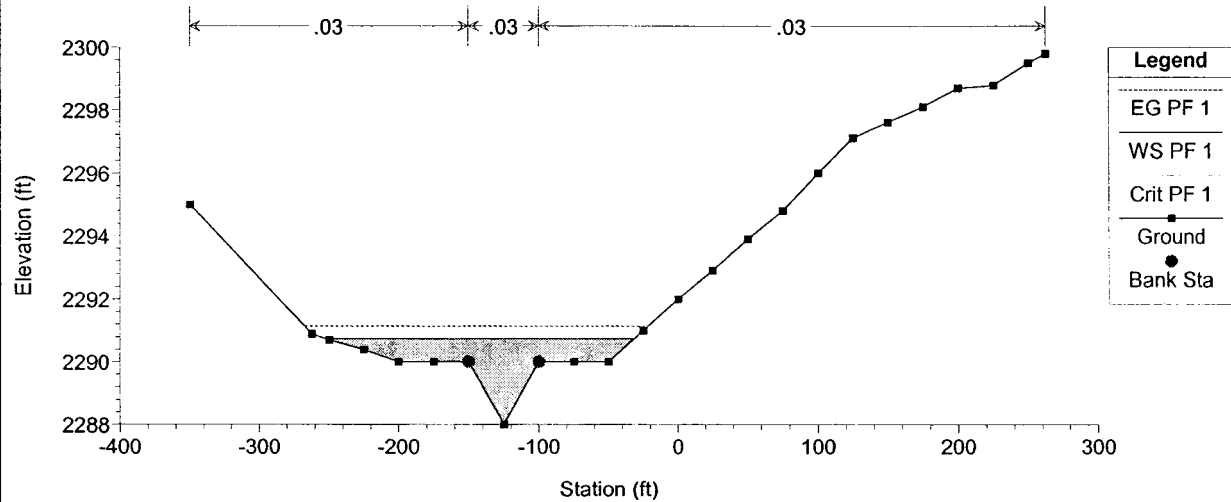
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005

Section D-D, Reach 4



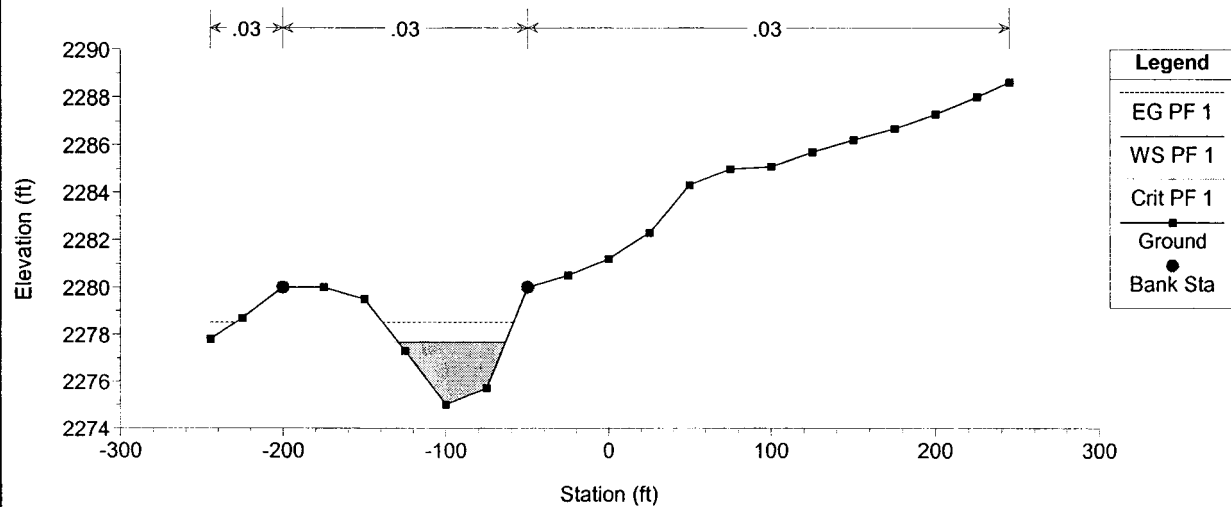
C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005

Section C-C, Reach 4

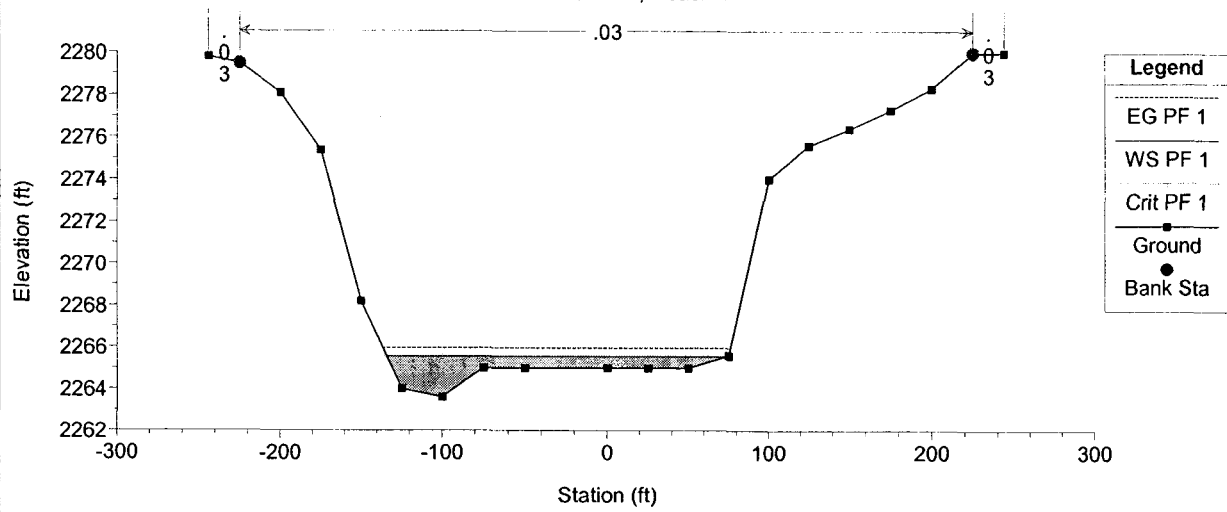


C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005

Section B-B, Reach 4



C-1 Channel System FIS Restudy -Reach 4 Plan: Reach 4 10/25/2005
Section A-A, Reach 4



**CORRECTIVE/EFFECTIVE
PRE-PROJECT CONDITIONS (VTN): HEC-RAS OUTPUT
W/ CARTER BURGESS FLOWS
(USED HEC-1 CARTER BURGESS
POST-DEVELOPMENT FLOWS FOR VTN PRE-PROJECT
CONDITIONS)**

HEC-RAS Version 3.1.3 May 2005
 U.S. Army Corp of Engineers
 Hydrologic Engineering Center
 609 Second Street
 Davis, California

```

X   X   XXXXXX   XXXX   XXXX   XX   XXXX
X   X   X       X   X   X   X   X   X
X   X   X       X   X   X   X   X   X
XXXXXXX XXXX   X   XXX XXXX   XXXXXX   XXXX
X   X   X   X   X   X   X   X   X   X
X   X   X   X   X   X   X   X   X   X
X   X   XXXXXX   XXXX   X   X   X   XXXXX

```

PROJECT DATA

Project Title: VTN-Pre-Project w/Carter Burgess Flows
 Project File : 022206.prj
 Run Date and Time: 2/22/2006 6:08:43 PM

Project in English units

Project Description:

Mission LOMR: VTN Post-Project w/ Carter Burgess Flow (Ref)

PLAN DATA

Plan Title: Plan 16

Plan File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.p16

Geometry Title: 02-22-06

Geometry File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.g12

Flow Title : Carter Burgess Flows

Flow File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.f04

Plan Summary Information:

Number of: Cross Sections = 27 Multiple Openings = 0
 Culverts = 1 Inline Structures = 0
 Bridges = 0 Lateral Structures = 0

Computational Information

Water surface calculation tolerance = 0.01
 Critical depth calculation tolerance = 0.01
 Maximum number of iterations = 20
 Maximum difference tolerance = 0.3
 Flow tolerance factor = 0.001

Computation Options

Critical depth computed only where necessary
 Conveyance Calculation Method: At breaks in n values only
 Friction Slope Method: Average Conveyance
 Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: Carter Burgess Flows

Flow File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.f04

Flow Data (cfs)

```

*****
* River      Reach      RS      *      PF 1 *
* FIS Flood Zone Mission 48      *      286 *
* FIS Flood Zone Mission 26      *      490 *
* FIS Flood Zone Mission 19      *      799 *
*****

```

Boundary Conditions

```

*****
* River      Reach      Profile      *      Upstream      Downstream *
*****
* FIS Flood Zone Mission PF 1      *      Critical      Normal S = 0.0229 *
*****

```

GEOMETRY DATA

Geometry Title: 02-22-06

Geometry File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.g12

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 48

INPUT

Description: 0+100

Station Elevation Data num= 27

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-173.84	2392	-118.84	2391.68	-58.01	2388	-42.83	2387.43
28.51	2383	38.23	2383.92	97.69	2385.67	123.66	2384.09
256.2	2378.52	338.85	2376	371.85	2381.52	376.8	2380
423.32	2374.68	446.53	2376	457.06	2378	484.25	2378
524.94	2376	555.62	2376	567.65	2370	591.28	2370
628.27	2372	682.75	2401.51				

Manning's n Values

num= 3
 Sta n Val Sta n Val Sta n Val
 -173.84 .035 -118.84 .035 97.69 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -118.84 97.69 200 200 .1 .3
 Left Levee Station= -42.83 Elevation= 2387.43
 Right Levee Station= 97.69 Elevation= 2385.67

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft)      * 2384.56 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)      * 0.55   * Wt. n-Val.  * " 0.035 * " " "
* W.S. Elev (ft)      * 2384.01 * Reach Len. (ft) * 200.00 * 200.00 * 200.00 *
* Crit W.S. (ft)      * 2384.01 * Flow Area (sq ft) * 48.10 * " " "
* E.G. Slope (ft/ft)  * 0.017231 * Area (sq ft) * 48.10 * " " "
* Q Total (cfs)       * 286.00 * Flow (cfs) * 286.00 * " " "
* Top Width (ft)      * 43.38 * Top Width (ft) * 43.38 * " " "
* Vel Total (ft/s)    * 5.95 * Avg. Vel. (ft/s) * 5.95 * " " "
*****

```

```

* Max Chl Dpth (ft) * 14.01 * Hydr. Depth (ft) * * 022206.rep *
* Conv. Total (cfs) * 2178.8 * Conv. (cfs) * * 1.11 *
* Length Wtd. (Ft) * 200.00 * Wetted Per. (ft) * * 2178.8 *
* Min Ch El (ft) * 2382.00 * Shear (lb/sq ft) * * 43.66 *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 1.19 *
* Frctn Loss (ft) * 0.00 * Cum Volume (acre-ft) * 0.02 * 7.05 *
* C & E Loss (ft) * 0.05 * Cum SA (acres) * 0.09 * 10.17 *
* * * * * 7.84 *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 46

INPUT

Description: 0+300

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-84.97	2384.63	6.45	2378.12	25.09	2376.04	53.39	2374	64.77	2374
117.96	2377.87	218.54	2376	266.82	2367.72	294.84	2367.11	312.32	2368
366.86	2367.89	383.36	2368.35	447.53	2368	474.66	2367.16	514.95	2379.89
554.18	2380.42	601.91	2379.58	617.76	2376	641.09	2376.13	683.46	2387.18

Sta	n Val	Sta	n Val	Sta	n Val
-84.97	.035	6.45	.035	117.96	.035

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff Contr.	Expan.
6.45	117.96	200	200	.1	.3
Left Levee	Station= 6.45	Elevation= 2378.12			
Right Levee	Station= 117.96	Elevation= 2377.87			

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2376.04	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.47	* Wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2375.57	* Reach Len. (ft)	* 200.00	* 200.00	* 200.00
* Crit W.S. (ft)	* 2375.57	* Flow Area (sq ft)		* 52.03	
* E.G. Slope (ft/ft)	* 0.018018	* Area (sq ft)		* 52.03	
* Q Total (cfs)	* 286.00	* Flow (cfs)		* 286.00	
* Top Width (ft)	* 54.80	* Top Width (ft)		* 54.80	
* Vel Total (ft/s)	* 5.50	* Avg. Vel. (ft/s)		* 5.50	
* Max Chl Dpth (ft)	* 8.46	* Hydr. Depth (ft)		* 0.95	
* Conv. Total (cfs)	* 2130.6	* Conv. (cfs)		* 2130.6	
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)		* 54.91	
* Min Ch El (ft)	* 2374.00	* Shear (lb/sq ft)		* 1.07	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 5.86	
* Frctn Loss (ft)	* 0.95	* Cum Volume (acre-ft)	* 0.02	* 9.94	
* C & E Loss (ft)	* 0.04	* Cum SA (acres)	* 0.09	* 7.62	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 44

INPUT

Description: 0+500

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-49.81	2378.58	46.88	2373.73	87.47	2363.08	121.51	2362	160.53	2368
195.41	2369.5	229.76	2368	247.29	2362	299.43	2362	354.98	2366
437.9	2366	457.32	2358.25	476.17	2356.64	598.56	2368.16	646.7	2368
681.22	2382								

Sta	n Val	Sta	n Val	Sta	n Val
-49.81	.035	46.88	.035	195.41	.035

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff Contr.	Expan.
46.88	195.41	400	210	.1	.3
Left Levee	Station= 46.88	Elevation= 2373.73			
Right Levee	Station= 195.41	Elevation= 2369.5			

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2364.22	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.51	* Wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2363.70	* Reach Len. (ft)	* 400.00	* 210.00	* 200.00
* Crit W.S. (ft)	* 2363.70	* Flow Area (sq ft)		* 49.67	
* E.G. Slope (ft/ft)	* 0.017427	* Area (sq ft)		* 49.67	
* Q Total (cfs)	* 286.00	* Flow (cfs)		* 286.00	
* Top Width (ft)	* 47.47	* Top Width (ft)		* 47.47	
* Vel Total (ft/s)	* 5.76	* Avg. Vel. (ft/s)		* 5.76	
* Max Chl Dpth (ft)	* 7.06	* Hydr. Depth (ft)		* 1.05	
* Conv. Total (cfs)	* 2166.5	* Conv. (cfs)		* 2166.5	
* Length Wtd. (ft)	* 210.00	* Wetted Per. (ft)		* 47.70	
* Min Ch El (ft)	* 2362.00	* Shear (lb/sq ft)		* 1.13	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 6.52	
* Frctn Loss (ft)	* 1.63	* Cum Volume (acre-ft)	* 0.02	* 9.70	
* C & E Loss (ft)	* 0.04	* Cum SA (acres)	* 0.09	* 7.38	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 42

INPUT

Description: 0+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-3.26	2370.96	20.48	2360	109.52	2357.99	127.31	2354	136.96	2354
166.31	2357.9	208.45	2358.52	227.77	2360	247.65	2360	277.16	2361.97
277.27	2361.97	277.77	2361.97	331.57	2362	383.73	2364	399.01	2364
442.36	2362	462.45	2363	479.15	2352.13	490.21	2352	515.36	2354
540	2352	597	2350	627.49	2362				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-3.26	.035	20.48	.035	227.77	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 20.48 227.77 220 220 350 .1 .3
 Left Levee Station= 20.48 Elevation= 2360
 Right Levee Station= 227.77 Elevation= 2360

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2356.68	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.65	* Wt. n-Val.	* 220.00	* 0.035	* 350.00
* W.S. Elev (ft)	* 2356.03	* Reach Len. (ft)		* 220.00	
* Crit W.S. (ft)	* 2356.03	* Flow Area (sq ft)		* 44.13	
* E.G. Slope (ft/ft)	* 0.016645	* Area (sq ft)		* 44.13	
* Q Total (cfs)	* 286.00	* Flow (cfs)		* 286.00	
* Top Width (ft)	* 33.92	* Top Width (ft)		* 33.92	
* Vel Total (ft/s)	* 6.48	* Avg. Vel. (ft/s)		* 6.48	
* Max Chl Dpth (ft)	* 6.03	* Hydr. Depth (ft)		* 1.30	
* Conv. Total (cfs)	* 2216.8	* Conv. (cfs)		* 2216.8	
* Length Wtd. (ft)	* 220.00	* Wetted Per. (ft)		* 34.28	
* Min Ch El (ft)	* 2354.00	* Shear (lb/sq ft)		* 1.34	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 8.67	
* Frctn Loss (ft)	* 2.99	* Cum Volume (acre-ft)	* 0.02	* 9.48	
* C & E Loss (ft)	* 0.01	* Cum SA (acres)	* 0.09	* 7.18	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 40

INPUT

Description: 0+900

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
40.76	2357.87	138.91	2350	152.31	2350	169.69	2356	217.32	2356.04
265.62	2357.42	382.86	2358	382.96	2358	425.96	2356	502.96	2359.06
524.35	2358								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
40.76	.035	40.76	.035	382.96	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 40.76 382.96 300 300 300 .1 .3
 Left Levee Station= 40.76 Elevation= 2357.87
 Right Levee Station= 265.62 Elevation= 2357.42

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2352.33	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.57	* Wt. n-Val.	* 300.00	* 0.035	* 300.00
* W.S. Elev (ft)	* 2351.75	* Reach Len. (ft)		* 300.00	
* Crit W.S. (ft)	* 2351.75	* Flow Area (sq ft)		* 47.11	
* E.G. Slope (ft/ft)	* 0.016829	* Area (sq ft)		* 47.11	
* Q Total (cfs)	* 286.00	* Flow (cfs)		* 286.00	
* Top Width (ft)	* 40.34	* Top Width (ft)		* 40.34	
* Vel Total (ft/s)	* 6.07	* Avg. Vel. (ft/s)		* 6.07	
* Max Chl Dpth (ft)	* 1.75	* Hydr. Depth (ft)		* 1.17	
* Conv. Total (cfs)	* 2204.6	* Conv. (cfs)		* 2204.6	
* Length Wtd. (ft)	* 300.00	* Wetted Per. (ft)		* 40.71	
* Min Ch El (ft)	* 2350.00	* Shear (lb/sq ft)		* 1.22	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 7.38	
* Frctn Loss (ft)	* 4.99	* Cum Volume (acre-ft)	* 0.02	* 9.25	
* C & E Loss (ft)	* 0.02	* Cum SA (acres)	* 0.09	* 7.00	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 37

INPUT

Description: 1+200

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-73.3	2350	-64.13	2348	17.29	2348	31.09	2350.31	43.06	2350.77
67.84	2350	109.53	2349.52	129.54	2348	141.96	2348	160.5	2347.44
203.41	2347.05	213.19	2346.2	231.47	2345.27	237.84	2343.07	254.96	2344
263.97	2348	292.81	2348.8	430.54	2347.99	447.09	2346.43	482.21	2348.76
508.61	2349.28	538.41	2348.38	604.11	2349.14	661.33	2347.98		

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val

 -73.3 .035 43.06 .035 508.61 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 43.06 508.61 100 100 100 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft)      * 2346.12 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)      * 0.73  * Wt. n-Val.   *      *      *      *
* W.S. Elev (ft)      * 2345.39 * Reach Len. (ft) * 100.00 * 100.00 * 100.00 *
* Crit W.S. (ft)      * 2345.39 * Flow Area (sq ft) *      * 41.74 *      *
* E.G. Slope (ft/ft)  * 0.016839 * Area (sq ft) *      * 41.74 *      *
* Q Total (cfs)       * 286.00 * Flow (cfs) *      * 286.00 *      *
* Top Width (ft)      * 28.90 * Top Width (ft) *      * 28.90 *      *
* Vel Total (ft/s)    * 6.85 * Avg. Vel. (ft/s) *      * 6.85 *      *
* Max Chl Dpth (ft)   * 2.32 * Hydr. Depth (ft) *      * 1.44 *      *
* Conv. Total (cfs)   * 2228.7 * Conv. (cfs) *      * 2228.7 *      *
* Length Wtd. (ft)    * 100.00 * Wetted Per. (ft) *      * 29.59 *      *
* Min Ch El (ft)      * 2343.07 * Shear (lb/sq ft) *      * 1.45 *      *
* Alpha              * 1.00 * Stream Power (lb/ft s) *      * 9.94 *      *
* Frctn Loss (ft)     * 1.67 * Cum Volume (acre-ft) * 0.02 * 8.94 *      *
* C & E Loss (ft)     * 0.01 * Cum SA (acres) * 0.09 * 6.76 *      *
*****
  
```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone

REACH: Mission RS: 36

INPUT

Description: 1+300

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
45.57	2347.92	159.01	2344	180.69	2344	189.27	2340
230.59	2346.93	271.17	2348	280.07	2346.31	427.63	2344
512.55	2346.25	652.62	2345.86				

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
45.57	.035	45.57	.035	456.67	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 45.57 456.67 200 200 200 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft)      * 2342.18 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)      * 0.68  * Wt. n-Val.   *      *      *      *
* W.S. Elev (ft)      * 2341.50 * Reach Len. (ft) * 200.00 * 200.00 * 200.00 *
* Crit W.S. (ft)      * 2341.50 * Flow Area (sq ft) *      * 43.20 *      *
* E.G. Slope (ft/ft)  * 0.016839 * Area (sq ft) *      * 43.20 *      *
* Q Total (cfs)       * 286.00 * Flow (cfs) *      * 286.00 *      *
* Top Width (ft)      * 32.14 * Top Width (ft) *      * 32.14 *      *
* Vel Total (ft/s)    * 6.62 * Avg. Vel. (ft/s) *      * 6.62 *      *
* Max Chl Dpth (ft)   * 1.50 * Hydr. Depth (ft) *      * 1.34 *      *
* Conv. Total (cfs)   * 2204.0 * Conv. (cfs) *      * 2204.0 *      *
* Length Wtd. (ft)    * 200.00 * Wetted Per. (ft) *      * 32.79 *      *
* Min Ch El (ft)      * 2340.00 * Shear (lb/sq ft) *      * 1.38 *      *
* Alpha              * 1.00 * Stream Power (lb/ft s) *      * 9.17 *      *
* Frctn Loss (ft)     * 3.63 * Cum Volume (acre-ft) * 0.02 * 8.84 *      *
* C & E Loss (ft)     * 0.09 * Cum SA (acres) * 0.09 * 6.69 *      *
*****
  
```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone

REACH: Mission RS: 34

INPUT

Description: 1+500

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-186.26	2346	-148.74	2345.86	-54.8	2339.88	22.59	2339.59
115.82	2340.55	160.63	2340.07	209.66	2338	219.09	2336
273.6	2340.11	310.56	2340	331.1	2336	349.75	2336.04
448.56	2345.82	490.03	2346.79	514.61	2346.13	602.59	2338

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
-186.26	.035	-148.74	.035	448.56	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -148.74 448.56 250 200 200 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft)      * 2337.30 * Element      * Left OB * Channel * Right OB *
* Vel Head (ft)      * 0.39  * Wt. n-Val.   *      *      *      *
* W.S. Elev (ft)      * 2336.91 * Reach Len. (ft) * 250.00 * 200.00 * 200.00 *
* Crit W.S. (ft)      * 2336.91 * Flow Area (sq ft) *      * 56.81 *      *
* E.G. Slope (ft/ft)  * 0.019602 * Area (sq ft) *      * 56.81 *      *
* Q Total (cfs)       * 286.00 * Flow (cfs) *      * 286.00 *      *
* Top Width (ft)      * 72.54 * Top Width (ft) *      * 72.54 *      *
* Vel Total (ft/s)    * 5.03 * Avg. Vel. (ft/s) *      * 5.03 *      *
* Max Chl Dpth (ft)   * 0.91 * Hydr. Depth (ft) *      * 0.78 *      *
* Conv. Total (cfs)   * 2042.7 * Conv. (cfs) *      * 2042.7 *      *
* Length Wtd. (ft)    * 200.00 * Wetted Per. (ft) *      * 72.89 *      *
* Min Ch El (ft)      * 2336.00 * Shear (lb/sq ft) *      * 0.95 *      *
* Alpha              * 1.00 * Stream Power (lb/ft s) *      * 4.80 *      *
* Frctn Loss (ft)     * 3.90 * Cum Volume (acre-ft) * 0.02 * 8.61 *      *
* C & E Loss (ft)     * 0.00 * Cum SA (acres) * 0.09 * 6.45 *      *
*****
  
```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: Divided flow computed for this cross-section.

022206.rep
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 32

INPUT

Description: 1+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-284.04	2344	-243.74	2344	-118.46	2337.35	-75.6	2336.84	-46.51	2334
-13.99	2334	27.6	2335.17	168.04	2334.99	253.22	2333.67	295.68	2330
348.33	2330.04	360.87	2334	437.29	2338	497.79	2339.78	616.37	2334
631.42	2333.89	653.39	2332.06	689.8	2321.85				

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
-284.04 .035 -243.74 .035 497.79 .035

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff Contr.	Expan.
-243.74	497.79	200	200	200	.1	.3
Left Levee Station=	-243.74	Elevation=	2344			
Right Levee Station=	497.79	Elevation=	2339.78			

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2331.36	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.42	* Wt. n-Val.			
* W.S. Elev (ft)	* 2330.94	* Reach Len. (ft)	* 200.00	* 200.00	* 200.00
* Crit W.S. (ft)	* 2330.94	* Flow Area (sq ft)		* 55.01	
* E.G. Slope (ft/ft)	* 0.019354	* Area (sq ft)		* 55.01	
* Q Total (cfs)	* 286.00	* Flow (cfs)		* 286.00	
* Top Width (ft)	* 66.41	* Top Width (ft)		* 66.41	
* Vel Total (ft/s)	* 5.20	* Avg. Vel. (ft/s)		* 5.19	
* Max Chl Dpth (ft)	* 9.09	* Hydr. Depth (ft)		* 0.83	
* Conv. Total (cfs)	* 2055.8	* Conv. (cfs)		* 2055.8	
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)		* 66.59	
* Min Ch El (ft)	* 2330.00	* Shear (lb/sq ft)		* 1.00	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 5.19	
* Frctn Loss (ft)	* 0.44	* Cum Volume (acre-ft)	* 0.02	* 8.36	
* C & E Loss (ft)	* 0.04	* Cum SA (acres)	* 0.09	* 6.13	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 30

INPUT

Description: 1+900

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-250.32	2336.65	-126.77	2334	-102.3	2328	-79.42	2326.47	-53.84	2328
15.58	2329.84	173.54	2329.68	248.4	2330	274.21	2326	307.47	2324
329.12	2326.06	356.58	2326	431.57	2334.48	494.85	2334.48	604.27	2328
621.53	2328.89	638.68	2328.1						

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
-250.32 .035 -126.77 .035 431.57 .035

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff Contr.	Expan.
-126.77	431.57	200	200	200	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2326.43	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.49	* Wt. n-Val.			
* W.S. Elev (ft)	* 2325.93	* Reach Len. (ft)	* 200.00	* 200.00	* 200.00
* Crit W.S. (ft)	* 2325.93	* Flow Area (sq ft)		* 50.67	
* E.G. Slope (ft/ft)	* 0.018576	* Area (sq ft)		* 50.67	
* Q Total (cfs)	* 286.00	* Flow (cfs)		* 286.00	
* Top Width (ft)	* 52.44	* Top Width (ft)		* 52.44	
* Vel Total (ft/s)	* 5.64	* Avg. Vel. (ft/s)		* 5.64	
* Max Chl Dpth (ft)	* 1.93	* Hydr. Depth (ft)		* 0.97	
* Conv. Total (cfs)	* 2098.4	* Conv. (cfs)		* 2098.4	
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)		* 52.59	
* Min Ch El (ft)	* 2324.00	* Shear (lb/sq ft)		* 1.12	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 6.31	
* Frctn Loss (ft)	* 3.59	* Cum Volume (acre-ft)	* 0.02	* 8.11	
* C & E Loss (ft)	* 0.00	* Cum SA (acres)	* 0.09	* 5.86	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 28

INPUT

Description: 2+100

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-233.84	2330.43	-84.24	2324	-66.89	2324	-53.02	2320	-18.78	2321.74
3.04	2324	16.5	2322	25.01	2324	63.16	2323.8	91.57	2322.33
170.95	2322.22	247.57	2324	273.66	2320	296.16	2320	360	2325
420.77	2329.64	473.24	2330.78	579.4	2322	646.84	2321.94	675.91	2312.1

Manning's n Values num= 3

Sta n Val Sta n Val Sta n Val
 -233.84 .035 -233.84 .035 420.77 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -233.84 420.77 210 200 200 .1 .3
 Left Levee Station= 247.57 Elevation= 2324
 Right Levee Station= 420.77 Elevation= 2329.64

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2321.90 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.30 * Wt. n-Val. * * 0.035 *
* W.S. Elev (ft) * 2321.40 * Reach Len. (ft) * 210.00 * 200.00 * 200.00 *
* Crit W.S. (ft) * 2321.40 * Flow Area (sq ft) * * 50.54 *
* E.G. Slope (ft/ft) * 0.017379 * Area (sq ft) * * 50.54 *
* Q Total (cfs) * 286.00 * Flow (cfs) * * 286.00 *
* Top Width (ft) * 49.56 * Top width (ft) * * 49.56 *
* Vel Total (ft/s) * 5.66 * Avg. Vel. (ft/s) * * 5.66 *
* Max Chl Dpth (ft) * 9.90 * Hydr. Depth (ft) * * 1.02 *
* Conv. Total (cfs) * 2169.5 * Conv. (cfs) * * 2169.5 *
* Length Wtd. (ft) * 200.00 * Wetted Per. (ft) * * 49.72 *
* Min Ch El (ft) * 2320.00 * Shear (lb/sq ft) * * 1.10 *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 6.24 *
* Frctn Loss (ft) * 0.96 * Cum Volume (acre-ft) * 0.02 * 7.88 *
* C & E Loss (ft) * 0.07 * Cum SA (acres) * 0.09 * 5.62 *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 26

INPUT

Description: 2+300

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-332.09	232.62	-266.12	2322.02	-239	2320.3	-195.8	2319.85	-171.96	2317.86
-141.05	2318	-89.33	2319.39	8.82	2319.2	50.01	2318	62.61	2314
89.81	2314	132.42	2317.69	158.02	2316	168.26	2315.97	200.86	2319.7
272.99	2316.02	284.41	2313.88	317.24	2313.84	334.2	2320	386.09	2326
465.37	2326	491.34	2322.53	509.9	2321.9	558.51	2316	606.32	2315.97
632.67	2312.82								

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 -332.09 .035 8.82 .035 386.09 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 8.82 386.09 300 300 330 .1 .3
 Left Levee Station= 200.86 Elevation= 2319.7
 Right Levee Station= 334.2 Elevation= 2320

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2316.38 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.74 * Wt. n-Val. * * 0.035 *
* W.S. Elev (ft) * 2315.63 * Reach Len. (ft) * 300.00 * 300.00 * 330.00 *
* Crit W.S. (ft) * 2315.63 * Flow Area (sq ft) * * 70.82 *
* E.G. Slope (ft/ft) * 0.015833 * Area (sq ft) * * 70.82 *
* Q Total (cfs) * 490.00 * Flow (cfs) * * 490.00 *
* Top Width (ft) * 47.12 * Top width (ft) * * 47.12 *
* Vel Total (ft/s) * 6.92 * Avg. Vel. (ft/s) * * 6.92 *
* Max Chl Dpth (ft) * 2.81 * Hydr. Depth (ft) * * 1.50 *
* Conv. Total (cfs) * 3919.0 * Conv. (cfs) * * 3919.0 *
* Length Wtd. (ft) * 300.00 * Wetted Per. (ft) * * 47.60 *
* Min Ch El (ft) * 2313.84 * Shear (lb/sq ft) * * 1.45 *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 10.05 *
* Frctn Loss (ft) * 4.68 * Cum Volume (acre-ft) * 0.02 * 7.60 *
* C & E Loss (ft) * 0.01 * Cum SA (acres) * 0.09 * 5.40 *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 24

INPUT

Description: 2+500

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-695	2315	-645	2317	-555	2318	-500	2315	-466	2316
-415	2312	-393	2312	-313	2316	-285	2316	-240	2312
-123	2314	85	2313.5	140	2311	155	2308	185	2308
207	2312	340	2319	435	2319.5	482	2317.2	538	2308
658	2309	705	2306						

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 -695 .035 -555 .035 340 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -555 340 220 220 270 .1 .3
 Left Levee Station= -555 Elevation= 2318
 Right Levee Station= 340 Elevation= 2319

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2310.54 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.72 * Wt. n-Val. * * 0.035 *
* W.S. Elev (ft) * 2309.82 * Reach Len. (ft) * 220.00 * 220.00 * 270.00 *
*****

```

```

* Crit W.S. (ft) * 2309.82 * Flow Area (sq ft) * * 71.98 * *
* E.G. Slope (ft/ft) * 0.01585 * Area (sq ft) * * 71.98 * *
* Q Total (cfs) * 490.00 * Flow (cfs) * * 490.00 * *
* Top Width (ft) * 49.11 * Top Width (ft) * * 49.11 * *
* Vel Total (ft/s) * 6.81 * Avg. Vel. (ft/s) * * 6.81 * *
* Max chl Dpth (ft) * 3.82 * Hydr. Depth (ft) * * 1.47 * *
* Conv. Total (cfs) * 3925.0 * Conv. (cfs) * * 3925.0 * *
* Length Wtd. (ft) * 220.00 * Wetted Per. (ft) * * 49.45 * *
* Min Ch El (ft) * 2308.00 * Shear (lb/sq ft) * * 1.42 * *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 9.64 * *
* Frctn Loss (ft) * 3.58 * Cum Volume (acre-ft) * 0.02 * 7.11 * *
* C & E Loss (ft) * 0.03 * Cum SA (acres) * 0.09 * 5.07 * *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 22

INPUT

Description: 2+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-690	2308	-660	2312	-575	2312	-500	2314	-375	2309
-305	2304	-287	2304	-210	2307.5	55	2307.5	65	2304
85	2303	125	2305	152	2307.5	195	2308	237	2313
280	2313	320	2310	358	2309	460	2310.5	530	2310
570	2302.5	585	2298	600	2298	620	2300	640	2300

Sta	n Val	Sta	n Val	Sta	n Val
-690	.035	-375	.035	195	.035

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff Contr.	Expan.
-375	195	230	240	.1	.3
Left Levee Station=	Station=	55	Elevation=	2307.5	
Right Levee Station=	Station=	152	Elevation=	2307.5	

CROSS SECTION OUTPUT Profile #PF 1

```

* E.G. Elev (ft) * 2305.72 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.61 * Wt. n-Val. * * 0.035 * *
* W.S. Elev (ft) * 2305.10 * Reach Len. (ft) * 230.00 * 240.00 * 240.00 *
* Crit W.S. (ft) * 2305.10 * Flow Area (sq ft) * * 77.98 * *
* E.G. Slope (ft/ft) * 0.017022 * Area (sq ft) * * 77.98 * *
* Q Total (cfs) * 490.00 * Flow (cfs) * * 490.00 * *
* Top Width (ft) * 64.26 * Top Width (ft) * * 64.26 * *
* Vel Total (ft/s) * 6.28 * Avg. Vel. (ft/s) * * 6.28 * *
* Max chl Dpth (ft) * 7.10 * Hydr. Depth (ft) * * 1.21 * *
* Conv. Total (cfs) * 3755.7 * Conv. (cfs) * * 3755.7 * *
* Length Wtd. (ft) * 240.00 * Wetted Per. (ft) * * 64.53 * *
* Min Ch El (ft) * 2303.00 * Shear (lb/sq ft) * * 1.28 * *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 8.07 * *
* Frctn Loss (ft) * 2.67 * Cum Volume (acre-ft) * 0.02 * 6.73 * *
* C & E Loss (ft) * 0.01 * Cum SA (acres) * 0.09 * 4.78 * *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 20

INPUT

Description: 2+900

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-620	2308	-580	2308	-520	2306	-470	2305.75	-450	2307
-360	2306	-220	2300	-210	2298	-195	2298	-180	2300
-165	2300	-150	2298	-130	2303	-60	2302.8	-25	2299.8
-15	2299.8	-10	2298	20	2298	50	2300	120	2302
180	2310	260	2310.8	480	2298.5	510	2298	580	2300

Sta	n Val	Sta	n Val	Sta	n Val
-620	.035	-450	.035	180	.035

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff Contr.	Expan.
-450	180	200	200	.1	.3
Left Levee Station=	Station=	-360	Elevation=	2306	
Right Levee Station=	Station=	180	Elevation=	2310	

CROSS SECTION OUTPUT Profile #PF 1

```

* E.G. Elev (ft) * 2299.72 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.46 * Wt. n-Val. * * 0.035 * *
* W.S. Elev (ft) * 2299.27 * Reach Len. (ft) * 200.00 * 200.00 * 200.00 *
* Crit W.S. (ft) * 2299.27 * Flow Area (sq ft) * * 90.41 * *
* E.G. Slope (ft/ft) * 0.018289 * Area (sq ft) * * 90.41 * *
* Q Total (cfs) * 490.00 * Flow (cfs) * * 490.00 * *
* Top Width (ft) * 97.87 * Top Width (ft) * * 97.87 * *
* Vel Total (ft/s) * 5.42 * Avg. Vel. (ft/s) * * 5.42 * *
* Max chl Dpth (ft) * 1.27 * Hydr. Depth (ft) * * 0.92 * *
* Conv. Total (cfs) * 3623.3 * Conv. (cfs) * * 3623.3 * *
* Length Wtd. (ft) * 200.00 * Wetted Per. (ft) * * 98.59 * *
* Min Ch El (ft) * 2298.00 * Shear (lb/sq ft) * * 1.05 * *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 5.67 * *
* Frctn Loss (ft) * 3.71 * Cum Volume (acre-ft) * 0.02 * 6.27 * *
* C & E Loss (ft) * 0.00 * Cum SA (acres) * 0.09 * 4.34 * *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

022206.rep
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 19

INPUT

Description: 3+000

Station Elevation Data		num= 12		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
52.74	2299.74	81.63	2298.73	100.84	2296	152.59	2295.81	199	2294
210.08	2292	247.52	2292	252.8	2291.63	258.56	2292	349.01	2292
362.72	2294	420.28	2295.25						

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
52.74	.035	199	.035	362.72	.035		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
199	362.72		100	100	100	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2293.46	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.49	* Wt. n-Val.	* 100.00	* 0.035	* 100.00
* W.S. Elev (ft)	* 2292.97	* Reach Len. (ft)			
* Crit W.S. (ft)	* 2292.97	* Flow Area (sq ft)		* 142.93	
* E.G. Slope (ft/ft)	* 0.018683	* Area (sq ft)		* 142.93	
* Q Total (cfs)	* 799.00	* Flow (cfs)		* 799.00	
* Top Width (ft)	* 150.98	* Top Width (ft)		* 150.98	
* Vel Total (ft/s)	* 5.59	* Avg. Vel. (ft/s)		* 5.59	
* Max Chl Dpth (ft)	* 1.34	* Hydr. Depth (ft)		* 0.95	
* Conv. Total (cfs)	* 5845.6	* Conv. (cfs)		* 5845.6	
* Length Wtd. (ft)	* 100.00	* Wetted Per. (ft)		* 151.16	
* Min Ch El (ft)	* 2291.63	* Shear (lb/sq ft)		* 1.10	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 6.17	
* Frctn Loss (ft)	* 1.77	* Cum Volume (acre-ft)	* 0.02	* 5.73	
* C & E Loss (ft)	* 0.02	* Cum SA (acres)	* 0.09	* 3.76	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 18

INPUT

Description: 3+100

Station Elevation Data		num= 14		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
41.32	2296	62.28	2296	80.22	2293.9	112.9	2292.5	168.47	2292
214.86	2286	227.03	2286	237.92	2288	303.24	2290	322.54	2290
347.5	2291	369.05	2290.98	404.01	2290	432.4	2290		

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
41.32	.035	168.47	.035	347.5	.035		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
168.47	347.5		165	165	165	.1	.3	

Cross Section Lid

num= 2		Sta Hi Cord Lo Cord		Sta Hi Cord Lo Cord			
Sta	Hi	Cord	Lo	Sta	Hi	Cord	Lo
232.61	2291	2290	236.61	2291	2290		

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2289.82	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.70	* Wt. n-Val.	* 165.00	* 0.035	* 165.00
* W.S. Elev (ft)	* 2289.11	* Reach Len. (ft)			
* Crit W.S. (ft)	* 2289.11	* Flow Area (sq ft)		* 118.63	
* E.G. Slope (ft/ft)	* 0.016733	* Area (sq ft)		* 118.63	
* Q Total (cfs)	* 799.00	* Flow (cfs)		* 799.00	
* Top Width (ft)	* 83.50	* Top Width (ft)		* 83.50	
* Vel Total (ft/s)	* 6.74	* Avg. Vel. (ft/s)		* 6.74	
* Max Chl Dpth (ft)	* 2.09	* Hydr. Depth (ft)		* 1.42	
* Conv. Total (cfs)	* 6176.8	* Conv. (cfs)		* 6176.8	
* Length Wtd. (ft)	* 165.00	* Wetted Per. (ft)		* 87.34	
* Min Ch El (ft)	* 2287.03	* Shear (lb/sq ft)		* 1.42	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 9.56	
* Frctn Loss (ft)	*	* Cum Volume (acre-ft)	* 0.02	* 5.43	
* C & E Loss (ft)	*	* Cum SA (acres)	* 0.09	* 3.50	

Warning: During subcritical analysis, the water surface upstream of culvert went to critical depth.

CULVERT

RIVER: FIS Flood Zone
REACH: Mission RS: 17

INPUT

Description:

Distance from Upstream XS = 100

Deck/Roadway Width = 4

Weir Coefficient = 2.6

Upstream Deck/Roadway Coordinates

num= 2		Sta Hi Cord Lo Cord		Sta Hi Cord Lo Cord			
Sta	Hi	Cord	Lo	Sta	Hi	Cord	Lo
221.03	2291	2290	225.03	2291	2290		

Upstream Bridge Cross Section Data

Station Elevation Data		num= 14		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev

```

*****
41.32  2296  62.28  2296  80.22  2293.9  112.9  2292.5  168.47  2292
214.86  2286  227.03  2286  237.92  2288  303.24  2290  322.54  2290
347.5  2291  369.05  2290.98  404.01  2290  432.4  2290
*****

```

```

Manning's n Values      num= 3
Sta  n Val  Sta  n Val  Sta  n Val
*****
41.32  .035  168.47  .035  347.5  .035
*****

```

```

Bank Sta: Left  Right  Coeff Contr.  Expan.
168.47  347.5  .1  .3

```

Downstream Deck/Roadway Coordinates

```

num= 2
Sta Hi Cord Lo Cord  Sta Hi Cord Lo Cord
*****
260.31  2289.6  2288.6  264.31  2289.6  2288.6
*****

```

Downstream Bridge Cross Section Data

```

Station Elevation Data  num= 15
Sta  Elev  Sta  Elev  Sta  Elev  Sta  Elev  Sta  Elev
*****
48.08  2294  58.34  2294  98.13  2292  111.08  2290  200.49  2286
206.56  2286  249.41  2284.03  258.31  2282  260.61  2282  278.52  2286
301  2285.51  321.73  2285.46  350.14  2284.8  369.37  2286  413.53  2286.45
*****

```

```

Manning's n Values      num= 3
Sta  n Val  Sta  n Val  Sta  n Val
*****
48.08  .035  200.49  .035  413.53  .035
*****

```

```

Bank Sta: Left  Right  Coeff Contr.  Expan.
200.49  413.53  .1  .3

```

```

Upstream Embankment side slope = 0 horiz. to 1.0 vertical
Downstream Embankment side slope = 0 horiz. to 1.0 vertical
Maximum allowable submergence for weir flow = .95
Elevation at which weir flow begins =
Energy head used in spillway design =
Spillway height used in design =
Weir crest shape = Broad Crested

```

Number of Culverts = 1

```

Culvert Name  Shape  Rise  Span
Culvert #1  Box  7  4
FHWA Chart # 8 - flared wingwalls
FHWA Scale # 1 - wingwall flared 30 to 75 deg.
Solution Criteria = Highest U.S. EG
Culvert Upstrm Dist  Length  Top n  Bottom n  Depth Blocked  Entrance Loss Coef  Exit Loss Coef
35  100  .014  .014  0  .05  1
Upstream Elevation = 2283
Centerline Station = 223.03
Downstream Elevation = 2281.6
Centerline Station = 262.31

```

CULVERT OUTPUT Profile #PF 1 Culv Group: Culvert #1

```

*****
* Q culv group (cfs) * 196.19 * Culv Full Len (ft) *
* # Barrels * 1 * Culv Vel US (ft/s) * 11.65 *
* Q Barrel (cfs) * 196.19 * Culv Vel DS (ft/s) * 14.10 *
* E.G. US. (ft) * 2289.75 * Culv Inv El Up (ft) * 2283.00 *
* W.S. US. (ft) * 2289.11 * Culv Inv El Dn (ft) * 2281.60 *
* E.G. DS (ft) * 2286.34 * Culv Frctn Ls (ft) * 1.15 *
* W.S. DS (ft) * 2285.85 * Culv Exit Loss (ft) * 1.83 *
* Delta EG (ft) * 3.41 * Culv Entr Loss (ft) * 0.43 *
* Delta WS (ft) * 3.26 * Q Weir (cfs) * 602.81 *
* E.G. IC (ft) * 2289.75 * Weir Sta Lft (ft) * 185.79 *
* E.G. OC (ft) * 2289.42 * Weir Sta Rgt (ft) * 295.39 *
* Culvert Control * inlet * Weir Submerg * 0.00 *
* Culv WS Inlet (ft) * 2287.21 * Weir Max Depth (ft) * 3.76 *
* Culv WS Outlet (ft) * 2285.08 * Weir Avg Depth (ft) * 1.57 *
* Culv Nml Depth (ft) * 3.36 * Weir Flow Area (sq ft) * 165.99 *
* Culv CRT Depth (ft) * 4.21 * Min El Weir Flow (ft) * 2286.01 *
*****

```

Warning: During subcritical analysis, the water surface upstream of culvert went to critical depth.
 Note: The flow in the culvert is entirely supercritical.

CROSS SECTION

```

RIVER: FIS Flood Zone
REACH: Mission RS: 16

```

INPUT

Description: 3+300

```

Station Elevation Data  num= 15
Sta  Elev  Sta  Elev  Sta  Elev  Sta  Elev  Sta  Elev
*****
48.08  2294  58.34  2294  98.13  2292  111.08  2290  200.49  2286
206.56  2286  249.41  2284.03  258.31  2282  260.61  2282  278.52  2286
301  2285.51  321.73  2285.46  350.14  2284.8  369.37  2286  413.53  2286.45
*****

```

```

Manning's n Values      num= 3
Sta  n Val  Sta  n Val  Sta  n Val
*****
48.08  .035  200.49  .035  413.53  .035
*****

```

```

Bank Sta: Left  Right  Lengths: Left Channel  Right  Coeff Contr.  Expan.
200.49  413.53  100  100  110  .1  .3

```

Cross Section L1d

```

num= 2
Sta Hi Cord Lo Cord  Sta Hi Cord Lo Cord
*****
232.61  2289.6  2288.6  236.61  2289.6  2288.6
*****

```

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2286.34 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.49 * Wt. n-Val. * 0.035 *
* W.S. Elev (ft) * 2285.85 * Reach Len. (ft) * 100.00 * 110.00 *
* Crit W.S. (ft) * 2285.85 * Flow Area (sq ft) * 142.72 *
* E.G. Slope (ft/ft) * 0.019006 * Area (sq ft) * 142.72 *
* Q Total (cfs) * 799.00 * Flow (cfs) * 799.00 *
* Top Width (ft) * 149.54 * Top Width (ft) * 149.54 *
* Vel Total (ft/s) * 5.60 * Avg. Vel. (ft/s) * 5.60 *
* Max Chl Dpth (ft) * 1.23 * Hydr. Depth (ft) * 0.95 *
* Conv. Total (cfs) * 5795.7 * Conv. (cfs) * 5795.7 *
* Length Wtd. (ft) * 100.00 * Wetted Per. (ft) * 152.55 *
* Min Ch El (ft) * 2284.62 * Shear (lb/sq ft) * 1.11 *
* Alpha * 1.00 * Stream Power (lb/ft s) * 6.21 *
* Frctn Loss (ft) * 1.78 * Cum Volume (acre-ft) * 0.02 * 4.94 *
* C & E Loss (ft) * 0.01 * Cum SA (acres) * 0.09 * 3.05 *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

022206.rep
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 15

INPUT

Description: 3+400

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
17.71	2286.97	26.99	2286.94	54.39	2282	65.42	2282	85.7	2284
108.83	2284	132.46	2281.98	167.75	2280	178.3	2280	192.04	2280.74
214.38	2280.54	219.45	2280.29	230.34	2282	251.22	2282	260.86	2284
278.16	2286	332.59	2286						

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
17.71 .035 108.83 .035 278.16 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
108.83 278.16 60 60 .1 .3
Left Levee Station= 108.83 Elevation= 2284

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2282.61	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.55	* wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2282.07	* Reach Len. (ft)	* 60.00	* 60.00	
* Crit W.S. (ft)	* 2282.07	* Flow Area (sq ft)		* 134.75	
* E.G. Slope (ft/ft)	* 0.016770	* Area (sq ft)		* 134.75	
* Q Total (cfs)	* 799.00	* Flow (cfs)		* 799.00	
* Top Width (ft)	* 120.08	* Top width (ft)		* 120.08	
* Vel Total (ft/s)	* 5.93	* Avg. Vel. (ft/s)		* 5.93	
* Max Chl Dpth (ft)	* 2.07	* Hydr. Depth (ft)		* 1.12	
* Conv. Total (cfs)	* 6169.9	* Conv. (cfs)		* 6169.9	
* Length Wtd. (ft)	* 60.00	* Wetted Per. (ft)		* 120.31	
* Min Ch El (ft)	* 2280.00	* Shear (lb/sq ft)		* 1.17	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 6.95	
* Frctn Loss (ft)	* 0.96	* Cum Volume (acre-ft)	* 0.02	* 4.62	
* C & E Loss (ft)	* 0.03	* Cum SA (acres)	* 0.09	* 2.74	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 14

INPUT

Description: 3+500

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
28.41	2280	52.78	2282	95.32	2282	128.99	2280
169.48	2279.49	204.01	2278	221.5	2276	237.94	2276
300.4	2284	325.65	2284.53				

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
28.41 .035 95.32 .035 263.15 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
95.32 263.15 240 260 .1 .3
Left Levee Station= 95.32 Elevation= 2282

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2279.75	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.81	* wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2278.94	* Reach Len. (ft)	* 240.00	* 260.00	* 390.00
* Crit W.S. (ft)	* 2278.94	* Flow Area (sq ft)		* 110.29	
* E.G. Slope (ft/ft)	* 0.015398	* Area (sq ft)		* 110.29	
* Q Total (cfs)	* 799.00	* Flow (cfs)		* 799.00	
* Top Width (ft)	* 67.92	* Top width (ft)		* 67.92	
* Vel Total (ft/s)	* 7.24	* Avg. Vel. (ft/s)		* 7.24	
* Max Chl Dpth (ft)	* 2.93	* Hydr. Depth (ft)		* 1.62	
* Conv. Total (cfs)	* 6438.9	* Conv. (cfs)		* 6438.9	
* Length Wtd. (ft)	* 260.00	* Wetted Per. (ft)		* 68.40	
* Min Ch El (ft)	* 2276.00	* Shear (lb/sq ft)		* 1.55	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 11.23	
* Frctn Loss (ft)	* 2.33	* Cum Volume (acre-ft)	* 0.02	* 4.45	
* C & E Loss (ft)	* 0.15	* Cum SA (acres)	* 0.09	* 2.61	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 12

INPUT

Description: 3+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-300	2280	-280	2282	-170	2282	-65	2278
						-47	2275

022206.rep

-30	2266	40	2266.5	75	2268	100	2275	150	2270
160	2270	200	2280	220	2280	255	2282	370	2286
500	2286	530	2294						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-300	.035	-65	.035	200	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

-65	200	140	90	120	.1	.3
-----	-----	-----	----	-----	----	----

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2268.55	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.31	* Wt. n-Val.	* *	* 0.035	* *
* W.S. Elev (ft)	* 2268.24	* Reach Len. (ft)	* 140.00	* 90.00	* 120.00
* Crit W.S. (ft)	* *	* Flow Area (sq ft)	* *	* 178.76	* *
* E.G. Slope (ft/ft)	* 0.005851	* Area (sq ft)	* *	* 178.76	* *
* Q Total (cfs)	* 799.00	* Flow (cfs)	* *	* 799.00	* *
* Top Width (ft)	* 110.09	* Top Width (ft)	* *	* 110.09	* *
* Vel Total (ft/s)	* 4.47	* Avg. Vel. (ft/s)	* *	* 4.47	* *
* Max Chl Dpth (ft)	* 2.24	* Hydr. Depth (ft)	* *	* 1.62	* *
* Conv. Total (cfs)	* 10445.6	* Conv. (cfs)	* *	* 10445.6	* *
* Length Wtd. (ft)	* 90.00	* Wetted Per. (ft)	* *	* 110.71	* *
* Min Ch El (ft)	* 2266.00	* Shear (lb/sq ft)	* *	* 0.59	* *
* Alpha	* 1.00	* Stream Power (lb/ft s)	* *	* 2.64	* *
* Frctn Loss (ft)	* 0.85	* Cum Volume (acre-ft)	* 0.02	* 3.59	* *
* C & E Loss (ft)	* 0.03	* Cum SA (acres)	* 0.09	* 2.08	* *

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 10

INPUT
Description: 3+900

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-370	2273.5	-300	2282	-185	2282	-110	2276	-45	2276
-30	2274	-10	2266	70	2265.5	90	2266.5	120	2280
180	2282	240	2283	345	2286	490	2286		

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-370	.035	-185	.035	120	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

-185	120	110	120	125	.1	.3
Left Levee	Station=	-185	Elevation=	2282		
Right Levee	Station=	120	Elevation=	2280		

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2267.67	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.64	* Wt. n-Val.	* *	* 0.035	* *
* W.S. Elev (ft)	* 2267.03	* Reach Len. (ft)	* 110.00	* 120.00	* 125.00
* Crit W.S. (ft)	* *	* Flow Area (sq ft)	* *	* 124.87	* *
* E.G. Slope (ft/ft)	* 0.017824	* Area (sq ft)	* *	* 124.87	* *
* Q Total (cfs)	* 799.00	* Flow (cfs)	* *	* 799.00	* *
* Top Width (ft)	* 103.76	* Top Width (ft)	* *	* 103.76	* *
* Vel Total (ft/s)	* 6.40	* Avg. Vel. (ft/s)	* *	* 6.40	* *
* Max Chl Dpth (ft)	* 1.53	* Hydr. Depth (ft)	* *	* 1.20	* *
* Conv. Total (cfs)	* 5984.7	* Conv. (cfs)	* *	* 5984.7	* *
* Length Wtd. (ft)	* 120.00	* Wetted Per. (ft)	* *	* 104.10	* *
* Min Ch El (ft)	* 2265.50	* Shear (lb/sq ft)	* *	* 1.33	* *
* Alpha	* 1.00	* Stream Power (lb/ft s)	* *	* 8.54	* *
* Frctn Loss (ft)	* 2.03	* Cum Volume (acre-ft)	* 0.02	* 3.27	* *
* C & E Loss (ft)	* 0.01	* Cum SA (acres)	* 0.09	* 1.86	* *

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 08

INPUT
Description: 4+100

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-365	2282	-240	2282	-140	2274	-80	2274	-45	2262
38	2262	58	2264	90	2279	160	2280	300	2286
305	2286								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-365	.035	-80	.035	90	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

-80	90	200	200	200	.1	.3
-----	----	-----	-----	-----	----	----

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2264.00	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.61	* Wt. n-Val.	* *	* 0.035	* *
* W.S. Elev (ft)	* 2263.39	* Reach Len. (ft)	* 200.00	* 200.00	* 200.00
* Crit W.S. (ft)	* 2263.37	* Flow Area (sq ft)	* *	* 127.52	* *
* E.G. Slope (ft/ft)	* 0.016007	* Area (sq ft)	* *	* 127.52	* *
* Q Total (cfs)	* 799.00	* Flow (cfs)	* *	* 799.00	* *
* Top Width (ft)	* 100.91	* Top Width (ft)	* *	* 100.91	* *
* Vel Total (ft/s)	* 6.27	* Avg. Vel. (ft/s)	* *	* 6.27	* *
* Max Chl Dpth (ft)	* 1.39	* Hydr. Depth (ft)	* *	* 1.26	* *
* Conv. Total (cfs)	* 6315.2	* Conv. (cfs)	* *	* 6315.2	* *
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)	* *	* 101.21	* *
* Min Ch El (ft)	* 2262.00	* Shear (lb/sq ft)	* *	* 1.26	* *
* Alpha	* 1.00	* Stream Power (lb/ft s)	* *	* 7.89	* *
* Frctn Loss (ft)	* 3.35	* Cum Volume (acre-ft)	* 0.02	* 2.93	* *
* C & E Loss (ft)	* 0.00	* Cum SA (acres)	* 0.09	* 1.58	* *

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 06

INPUT

Description: 4+300

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-345	2284	-280	2282	-155	2270.5	-80	2270	-65	2268
-45	2258	-30	2258	60	2260	90	2278	100	2280
120	2280	240	2284	260	2285				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-345	.035	-80	.035	90	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-80 90 200 200 200 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	2260.64	* Element	Left OB	Channel	Right OB				
* Vel Head (ft)	0.61	* Wt. n-Val.		0.035					
* W.S. Elev (ft)	2260.04	* Reach Len. (ft)	200.00		200.00				
* Crit W.S. (ft)	2260.04	* Flow Area (sq ft)		127.99					
* E.G. Slope (ft/ft)	0.017590	* Area (sq ft)		127.99					
* Q Total (cfs)	799.00	* Flow (cfs)		799.00					
* Top Width (ft)	109.13	* Top Width (ft)		109.13					
* Vel Total (ft/s)	6.24	* Avg. Vel. (ft/s)		6.24					
* Max Chl Dpth (ft)	2.04	* Hydr. Depth (ft)		1.17					
* Conv. Total (cfs)	6024.4	* Conv. (cfs)		6024.4					
* Length Wtd. (ft)	200.00	* Wetted Per. (ft)		109.65					
* Min Ch El (ft)	2258.00	* Shear (lb/sq ft)		1.28					
* Alpha	1.00	* Stream Power (lb/ft s)		8.00					
* Frctn Loss (ft)	0.73	* Cum Volume (acre-ft)	0.02	2.34					
* C & E Loss (ft)	0.14	* Cum SA (acres)	0.09	1.10					

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 04

INPUT

Description: 4+500

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-475	2282	-340	2282	-335	2279	-160	2264	-75	2264
-50	2254	30	2254	60	2256	80	2266.5	100	2267.5
120	2267	130	2268	160	2268	250	2274	280	2274.5
330	2274	520	2280						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-475	.035	-75	.035	80	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-75 80 200 200 200 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	2256.82	* Element	Left OB	Channel	Right OB				
* Vel Head (ft)	0.13	* Wt. n-Val.		0.035					
* W.S. Elev (ft)	2256.69	* Reach Len. (ft)	200.00		200.00				
* Crit W.S. (ft)	2256.69	* Flow Area (sq ft)		275.22					
* E.G. Slope (ft/ft)	0.001525	* Area (sq ft)		275.22					
* Q Total (cfs)	799.00	* Flow (cfs)		799.00					
* Top Width (ft)	118.03	* Top Width (ft)		118.03					
* Vel Total (ft/s)	2.90	* Avg. Vel. (ft/s)		2.90					
* Max Chl Dpth (ft)	2.69	* Hydr. Depth (ft)		2.33					
* Conv. Total (cfs)	20458.7	* Conv. (cfs)		20458.7					
* Length Wtd. (ft)	200.00	* Wetted Per. (ft)		118.79					
* Min Ch El (ft)	2254.00	* Shear (lb/sq ft)		0.22					
* Alpha	1.00	* Stream Power (lb/ft s)		0.64					
* Frctn Loss (ft)	0.27	* Cum Volume (acre-ft)	0.02	1.41					
* C & E Loss (ft)	0.00	* Cum SA (acres)	0.09	0.58					

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 02

INPUT

Description: 4+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-430	2262.5	-400	2256	-360	2256.5	-320	2258	-280	2258
-220	2260.5	-200	2260	-110	2260	-100	2260.5	-60	2260
-38	2253	30	2253.5	60	2256	88	2270	130	2272
180	2268	250	2271	260	2274	360	2276		

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-430	.035	-100	.035	88	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-100 88 29 29 29 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	2256.54	* Element	Left OB	Channel	Right OB				
* Vel Head (ft)	0.12	* Wt. n-Val.		0.035					
* W.S. Elev (ft)	2256.42	* Reach Len. (ft)	29.00		29.00				
* Crit W.S. (ft)	2256.42	* Flow Area (sq ft)	7.56		284.50				

```

* E.G. Slope (ft/ft)      * 0.001225 * Area (sq ft)          * 7.56 * 284.50 *
* Q Total (cfs)          * 799.00 * Flow (cfs)            * 3.98 * 795.02 *
* Top Width (ft)         * 145.36 * Top Width (ft)        * 35.76 * 109.60 *
* Vel Total (ft/s)       * 2.74   * Avg. Vel. (ft/s)     * 0.53 * 2.79 *
* Max Chl Dpth (ft)     * 3.42   * Hydr. Depth (ft)     * 0.21 * 2.60 *
* Conv. Total (cfs)     * 22825.5 * Wetted Per. (ft)    * 113.7 * 22711.8 *
* Length Wtd (ft)       * 29.00 * Shear (lb/sq ft)    * 35.81 * 110.34 *
* Min Ch El (ft)        * 2253.00 * Stream Power (lb/ft s) * 0.02 * 0.20 *
* Alpha                 * 1.04   * Cum Volume (acre-ft) * 0.01 * 0.55 *
* Frctn Loss (ft)       * 0.09   * Cum SA (acres)       * 0.00 * 0.13 *
* C & E Loss (ft)       * 0.08   *                      * 0.01 * 0.05 *

```

Warning: Divided flow computed for this cross-section.
Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 01

INPUT

Description: 4+729

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-220	2260	-50	2260	-30	2258	-20	2252	-15	2252
0	2255	10	2254.9	15	2252	20	2252	30	2256
60	2258.5	90	2269	130	2270.5	160	2270	195	2268
240	2270								

Sta	n val	Sta	n val	Sta	n val
-220	.035	-30	.035	60	.035

Bank Sta: Left -30 Right 60
Coeff Contr. .1 Expan. .3

CROSS SECTION OUTPUT Profile #PF 1

Element	Left 08	Channel	Right 08
E.G. Elev (ft)	2256.37		
Vel Head (ft)	0.94	0.035	
W.S. Elev (ft)	2255.43		
Crit W.S. (ft)	2255.43		
E.G. Slope (ft/ft)	0.015443		
Q Total (cfs)	799.00		
Top Width (ft)	54.29		
Vel Total (ft/s)	7.80		
Max Chl Dpth (ft)	3.43		
Conv. Total (cfs)	6429.5		
Length Wtd. (ft)			
Min Ch El (ft)	2252.00		
Alpha	1.00		
Frctn Loss (ft)			
C & E Loss (ft)			

Warning: Slope too steep for slope area to converge during supercritical flow calculations (normal depth is below critical depth). Water surface set to critical depth.

SUMMARY OF MANNING'S N VALUES

River: FIS Flood Zone

Reach	River Sta.	n1	n2	n3
Mission	48	.035*	.035*	.035*
Mission	46	.035*	.035*	.035*
Mission	44	.035*	.035*	.035*
Mission	42	.035*	.035*	.035*
Mission	40	.035*	.035*	.035*
Mission	37	.035*	.035*	.035*
Mission	36	.035*	.035*	.035*
Mission	34	.035*	.035*	.035*
Mission	32	.035*	.035*	.035*
Mission	30	.035*	.035*	.035*
Mission	28	.035*	.035*	.035*
Mission	26	.035*	.035*	.035*
Mission	24	.035*	.035*	.035*
Mission	22	.035*	.035*	.035*
Mission	20	.035*	.035*	.035*
Mission	19	.035*	.035*	.035*
Mission	18	.035*	.035*	.035*
Mission	17	*culvert		
Mission	16	.035*	.035*	.035*
Mission	15	.035*	.035*	.035*
Mission	14	.035*	.035*	.035*
Mission	12	.035*	.035*	.035*
Mission	10	.035*	.035*	.035*
Mission	08	.035*	.035*	.035*
Mission	06	.035*	.035*	.035*
Mission	04	.035*	.035*	.035*
Mission	02	.035*	.035*	.035*
Mission	01	.035*	.035*	.035*

SUMMARY OF REACH LENGTHS

River: FIS Flood Zone

Reach	River Sta.	Left	Channel	Right
Mission	48	200*	200*	200*
Mission	46	200*	200*	200*
Mission	44	400*	210*	200*
Mission	42	220*	220*	350*
Mission	40	300*	300*	300*
Mission	37	100*	100*	100*
Mission	36	200*	200*	200*
Mission	34	250*	200*	200*
Mission	32	200*	200*	200*
Mission	30	200*	200*	200*
Mission	28	210*	200*	200*
Mission	26	300*	300*	330*
Mission	24	220*	220*	270*
Mission	22	230*	240*	240*
Mission	20	200*	200*	200*
Mission	19	100*	100*	100*
Mission	18	165*	165*	165*
Mission	17	*Culvert		

*Mission	*	16	*	100*	100*	110*
*Mission	*	15	*	60*	60*	60*
*Mission	*	14	*	240*	260*	390*
*Mission	*	12	*	140*	90*	120*
*Mission	*	10	*	110*	120*	125*
*Mission	*	08	*	200*	200*	200*
*Mission	*	06	*	200*	200*	200*
*Mission	*	04	*	200*	200*	200*
*Mission	*	02	*	29*	29*	29*
*Mission	*	01	*	*	*	*

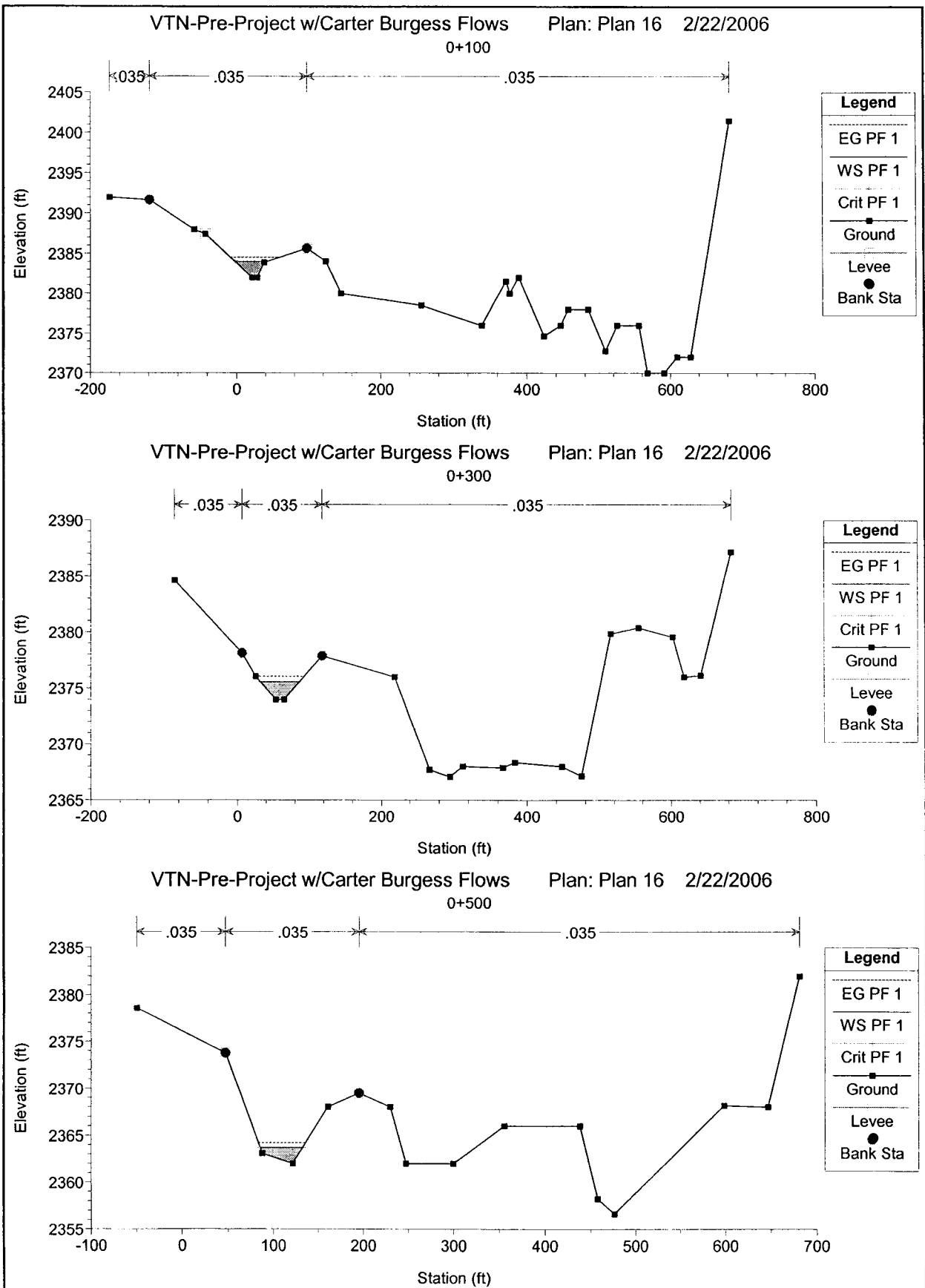
SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

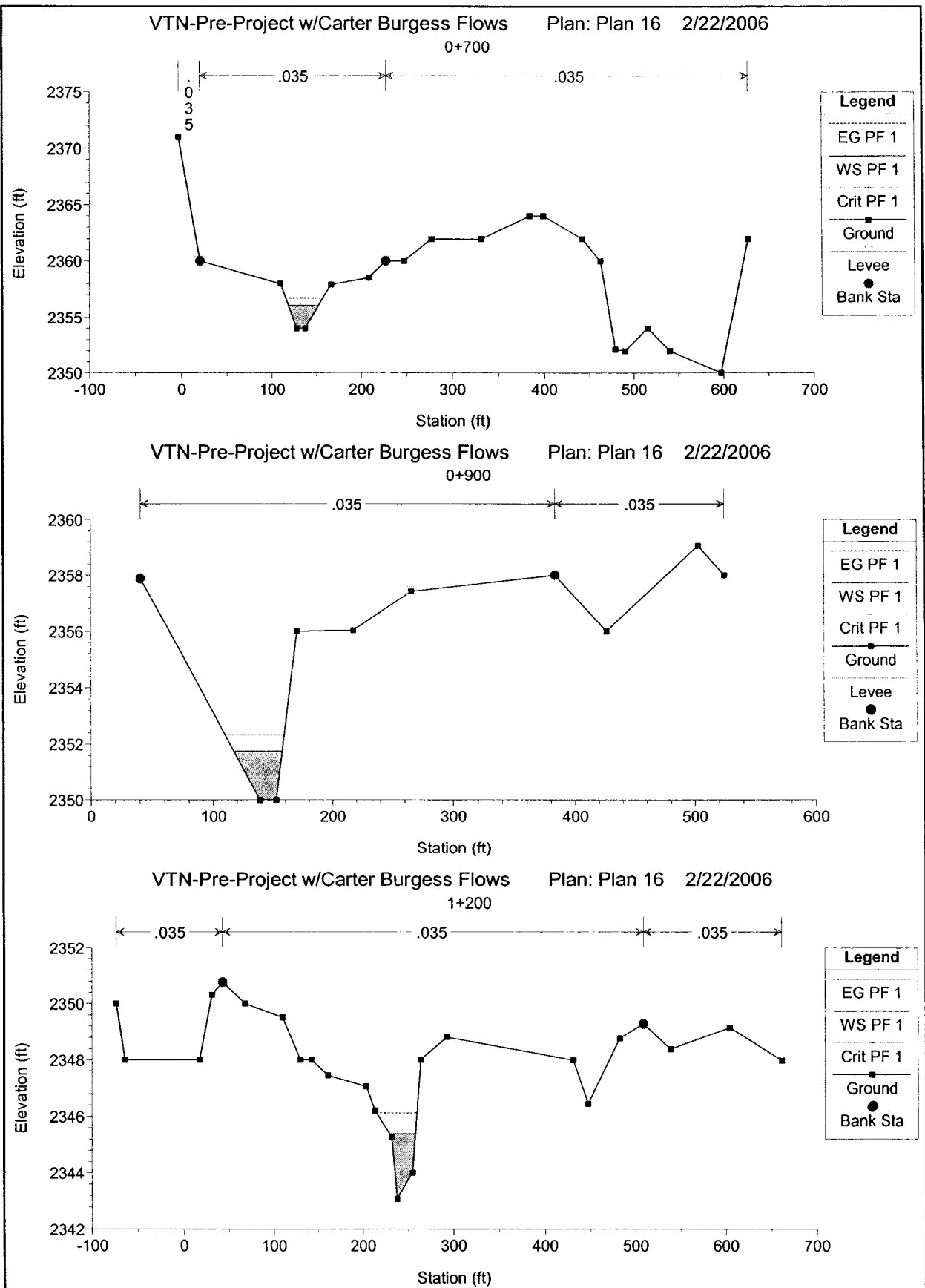
River: FIS Flood Zone

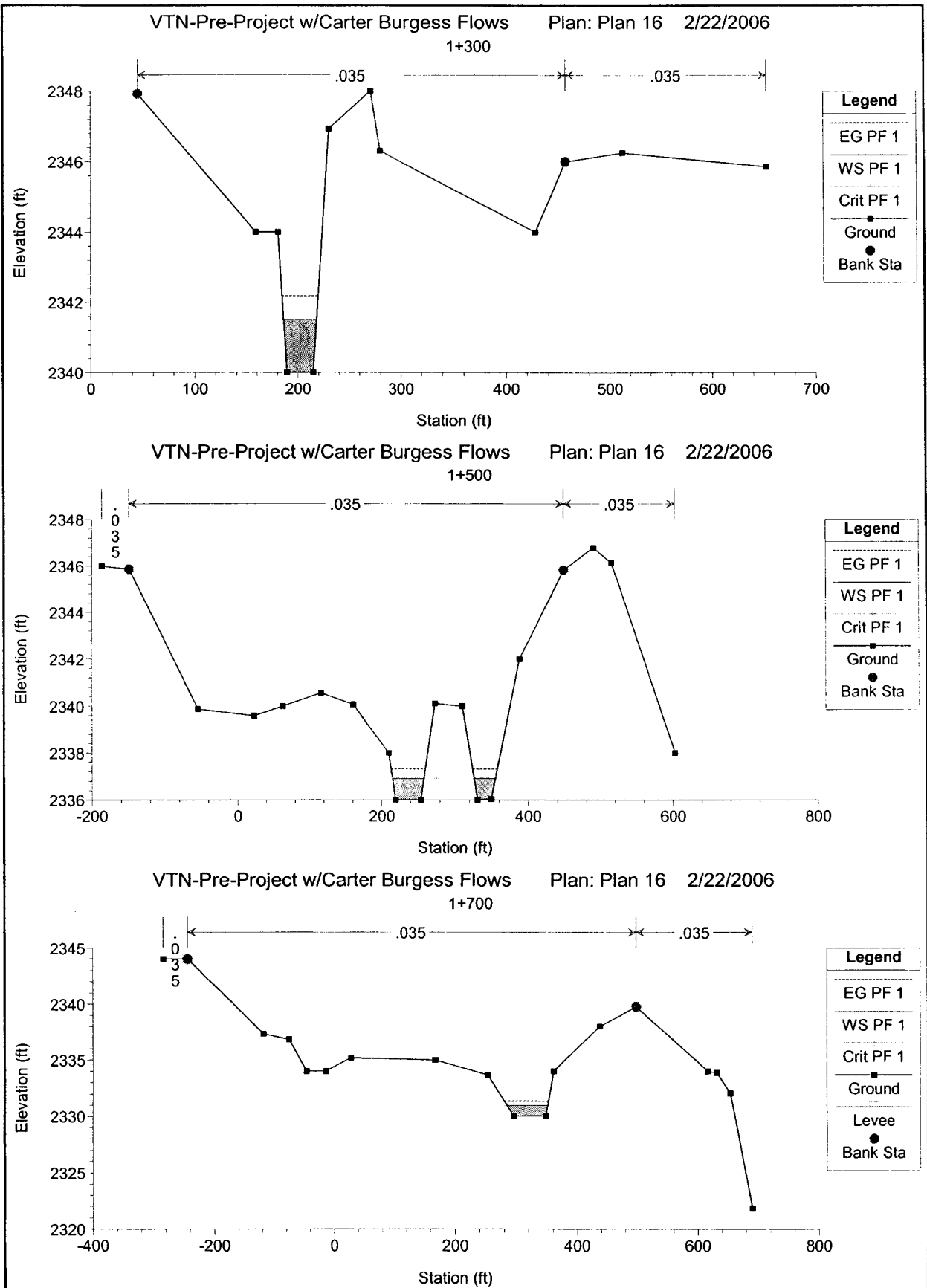
*****	*****	*****	*****	*****	*****
Reach	*	River Sta.	* Contr.	* Expan.	*
*****	*****	*****	*****	*****	*****
*Mission	*	48	*	.1*	.3*
*Mission	*	46	*	.1*	.3*
*Mission	*	44	*	.1*	.3*
*Mission	*	42	*	.1*	.3*
*Mission	*	40	*	.1*	.3*
*Mission	*	37	*	.1*	.3*
*Mission	*	36	*	.1*	.3*
*Mission	*	34	*	.1*	.3*
*Mission	*	32	*	.1*	.3*
*Mission	*	30	*	.1*	.3*
*Mission	*	28	*	.1*	.3*
*Mission	*	26	*	.1*	.3*
*Mission	*	24	*	.1*	.3*
*Mission	*	22	*	.1*	.3*
*Mission	*	20	*	.1*	.3*
*Mission	*	19	*	.1*	.3*
*Mission	*	18	*	.1*	.3*
*Mission	*	17	*culvert	*	*
*Mission	*	16	*	.1*	.3*
*Mission	*	15	*	.1*	.3*
*Mission	*	14	*	.1*	.3*
*Mission	*	12	*	.1*	.3*
*Mission	*	10	*	.1*	.3*
*Mission	*	08	*	.1*	.3*
*Mission	*	06	*	.1*	.3*
*Mission	*	04	*	.1*	.3*
*Mission	*	02	*	.1*	.3*
*Mission	*	01	*	.1*	.3*

HEC-RAS Plan: Plan 16 River: FIS Flood Zone Reach: Mission Profile: PF 1

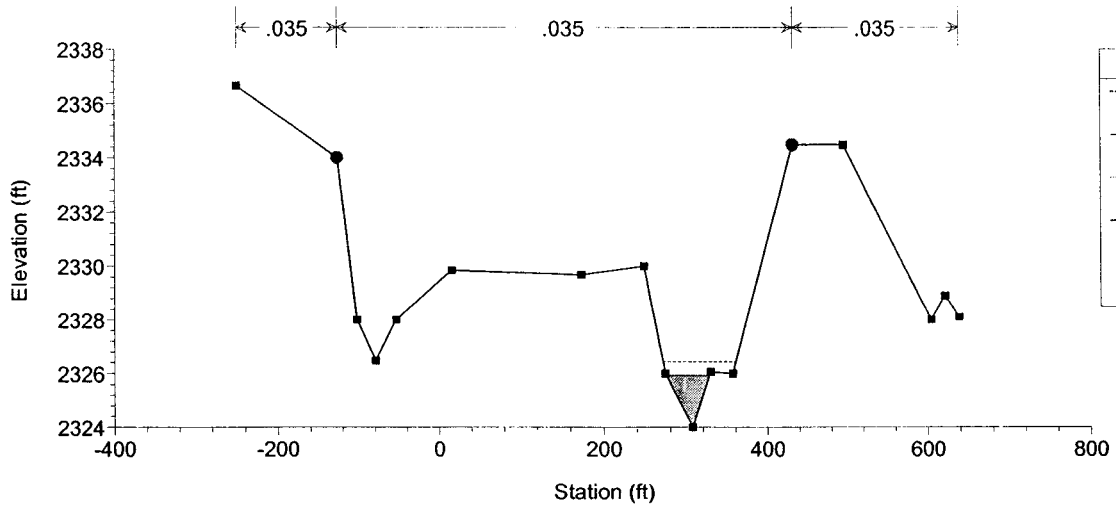
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl	Hydr Depth (ft)
Mission	48	PF 1	286.00	2382.00	2384.01	2384.01	2384.56	0.017231	5.95	48.10	43.38	0.99	1.11
Mission	48	PF 1	286.00	2374.00	2375.57	2375.57	2376.04	0.018018	5.50	52.03	54.80	0.99	0.95
Mission	44	PF 1	286.00	2362.00	2363.70	2363.70	2364.22	0.017427	5.76	49.67	47.47	0.99	1.05
Mission	42	PF 1	286.00	2354.00	2356.03	2356.03	2356.68	0.016845	6.48	44.13	33.92	1.00	1.30
Mission	40	PF 1	286.00	2350.00	2351.75	2351.75	2352.33	0.016829	6.07	47.11	40.34	0.99	1.17
Mission	37	PF 1	286.00	2343.07	2345.39	2345.39	2346.12	0.016468	6.85	41.74	28.90	1.00	1.44
Mission	36	PF 1	286.00	2340.00	2341.50	2341.50	2342.18	0.016839	6.62	43.20	32.14	1.01	1.34
Mission	34	PF 1	286.00	2336.00	2336.91	2336.91	2337.30	0.019602	5.03	56.81	72.54	1.00	0.78
Mission	32	PF 1	286.00	2330.00	2330.94	2330.94	2331.36	0.019354	5.20	55.01	66.41	1.01	0.83
Mission	30	PF 1	286.00	2324.00	2325.93	2325.93	2326.43	0.018576	5.64	50.67	52.44	1.01	0.97
Mission	28	PF 1	286.00	2320.00	2321.40	2321.40	2321.90	0.017379	5.66	50.54	49.56	0.99	1.02
Mission	26	PF 1	490.00	2313.84	2315.63	2315.63	2316.38	0.015633	6.92	70.82	47.12	0.99	1.50
Mission	24	PF 1	490.00	2308.00	2309.82	2309.82	2310.54	0.015585	6.81	71.98	49.11	0.99	1.47
Mission	22	PF 1	490.00	2303.00	2305.10	2305.10	2305.72	0.017022	6.28	77.98	64.26	1.01	1.21
Mission	20	PF 1	490.00	2298.00	2299.27	2299.27	2299.72	0.018289	5.42	90.41	97.87	0.99	0.92
Mission	19	PF 1	799.00	2291.63	2292.97	2292.97	2293.46	0.018683	5.59	142.93	150.98	1.01	0.95
Mission	18	PF 1	799.00	2287.03	2289.11	2289.11	2289.82	0.016733	6.74	118.63	83.50	0.90	1.42
Mission	17			Culvert									
Mission	16	PF 1	799.00	2284.62	2285.85	2285.85	2286.34	0.019006	5.60	142.72	149.54	0.92	0.95
Mission	15	PF 1	799.00	2280.00	2282.07	2282.07	2282.61	0.016770	5.93	134.75	120.08	0.99	1.12
Mission	14	PF 1	799.00	2276.00	2278.94	2278.94	2279.75	0.015398	7.24	110.29	67.92	1.00	1.62
Mission	12	PF 1	799.00	2266.00	2268.24		2268.55	0.005851	4.47	178.76	110.09	0.62	1.62
Mission	10	PF 1	799.00	2265.50	2267.03	2267.03	2267.67	0.017824	6.40	124.87	103.76	1.03	1.20
Mission	08	PF 1	799.00	2262.00	2263.39	2263.37	2264.00	0.016007	6.27	127.52	100.91	0.98	1.26
Mission	06	PF 1	799.00	2258.00	2260.04	2260.04	2260.64	0.017590	6.24	127.99	109.13	1.02	1.17
Mission	04	PF 1	799.00	2254.00	2256.69		2256.82	0.001525	2.90	275.22	118.03	0.34	2.33
Mission	02	PF 1	799.00	2253.00	2256.42		2256.54	0.001225	2.79	292.06	145.36	0.31	2.01
Mission	01	PF 1	799.00	2252.00	2255.43	2255.43	2256.37	0.015443	7.80	102.43	54.29	1.00	1.89



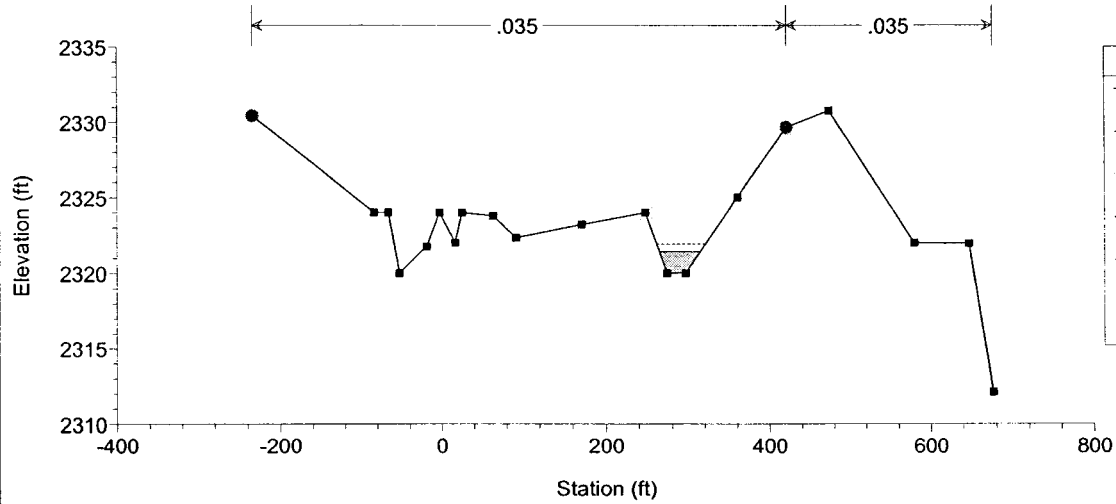




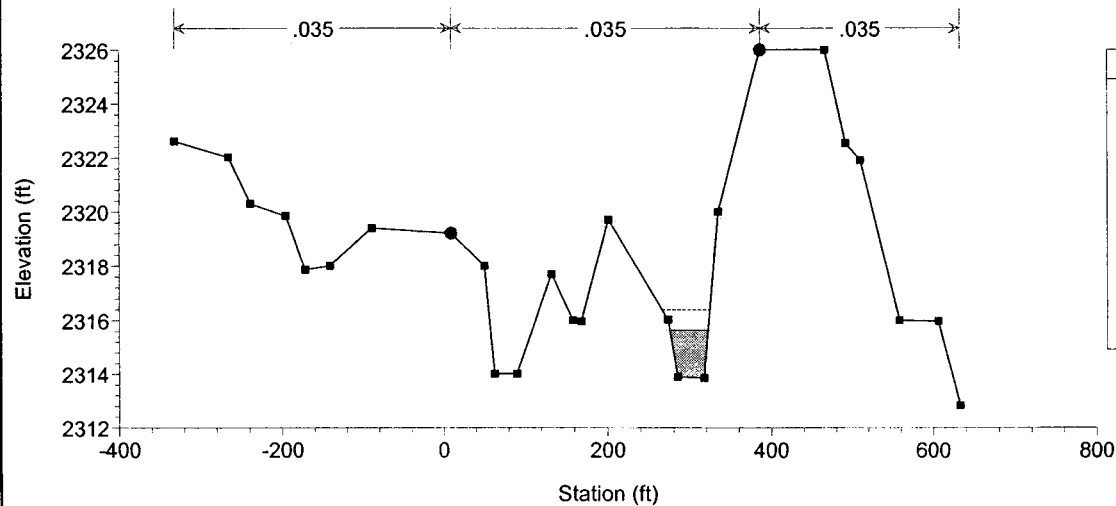
VTN-Pre-Project w/Carter Burgess Flows Plan: Plan 16 2/22/2006
1+900

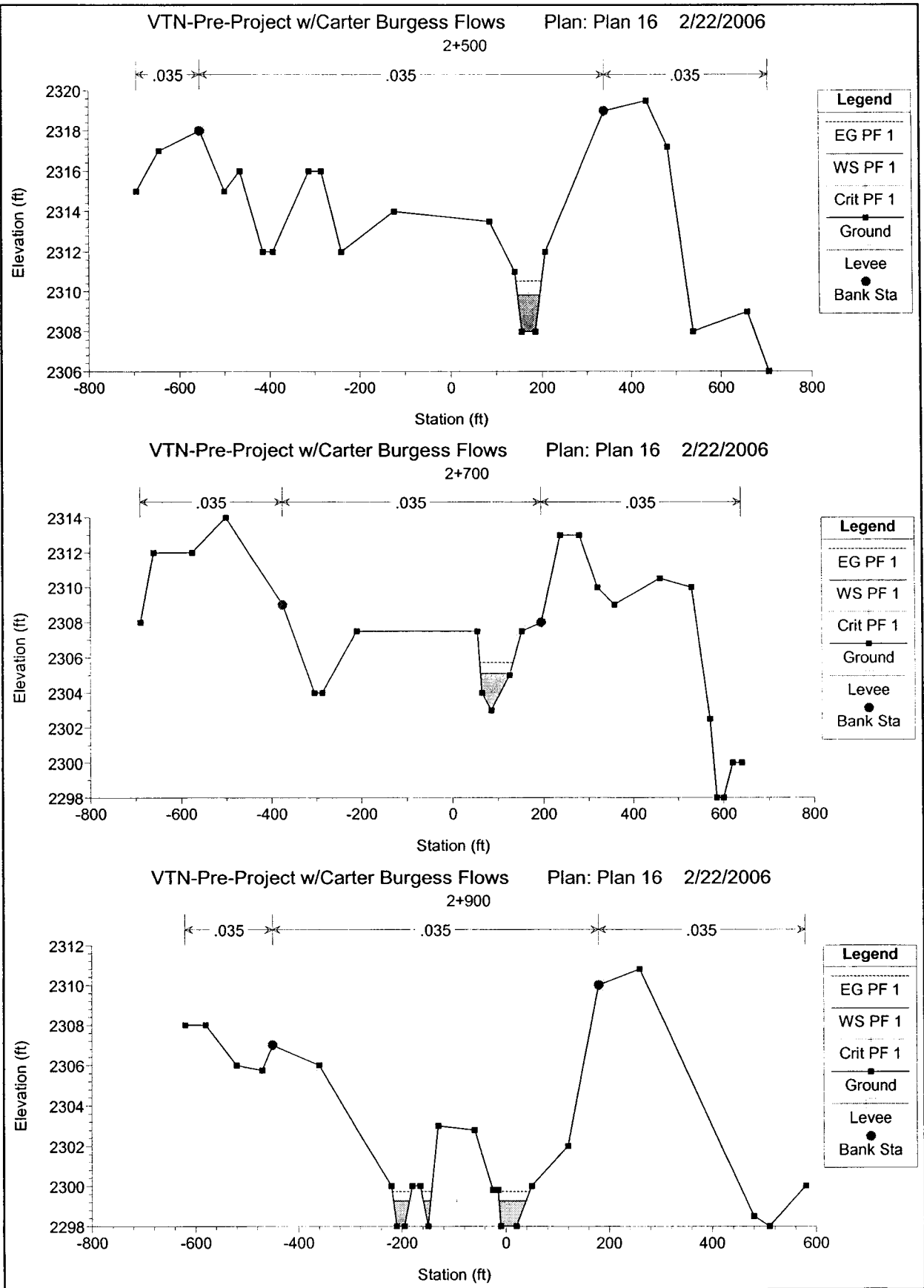


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2+100

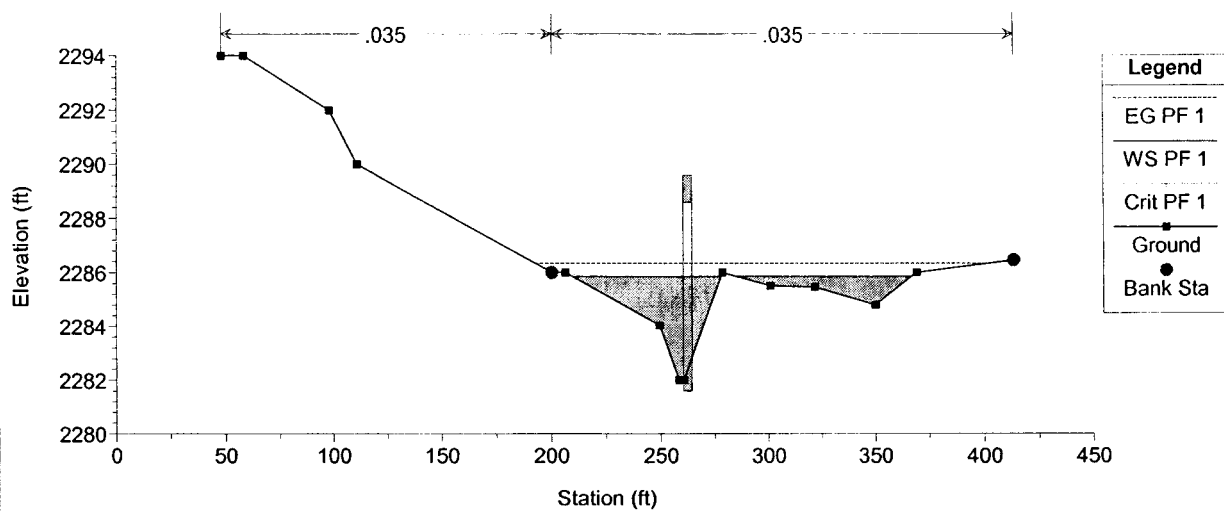


VTN-Pre-Project w/Carter Burgess Flows Plan: Plan 16 2/22/2006
2+300

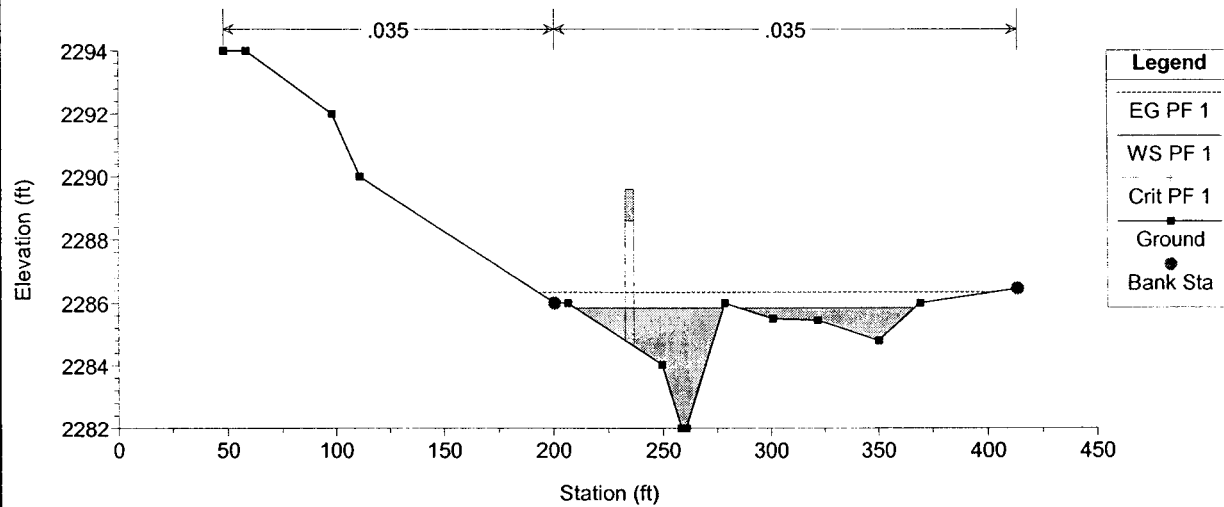




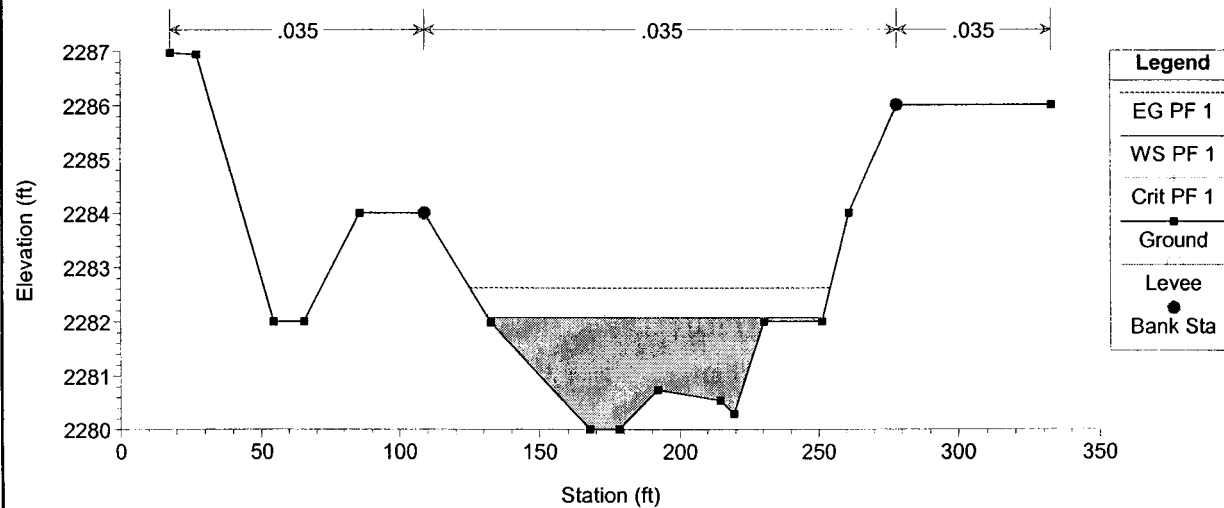
VTN-Pre-Project w/Carter Burgess Flows Plan: Plan 16 2/22/2006

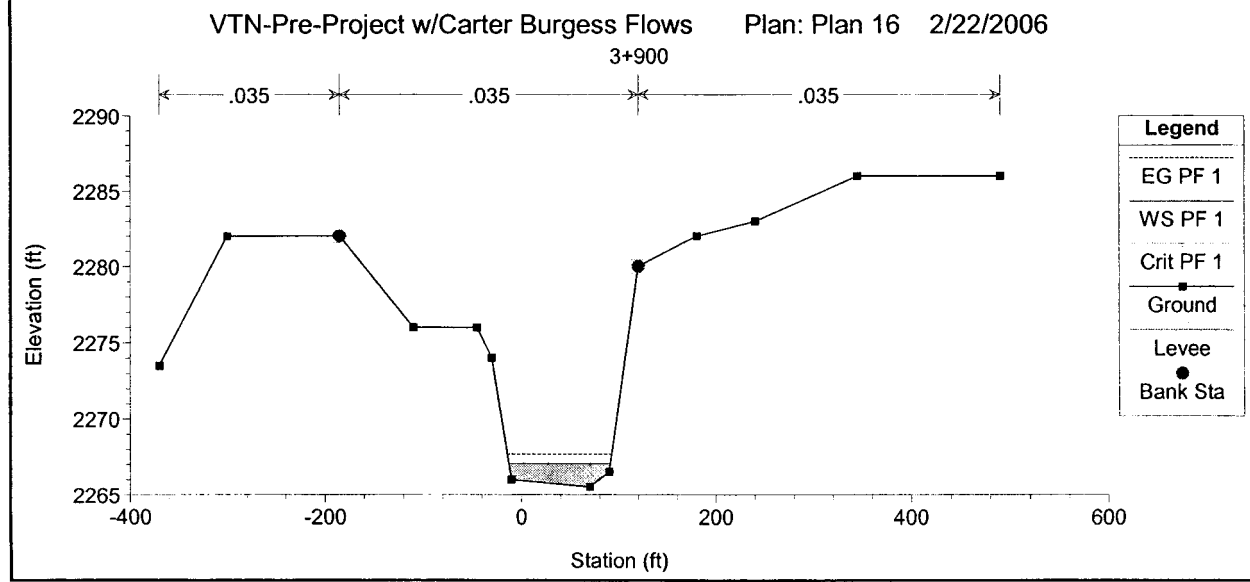
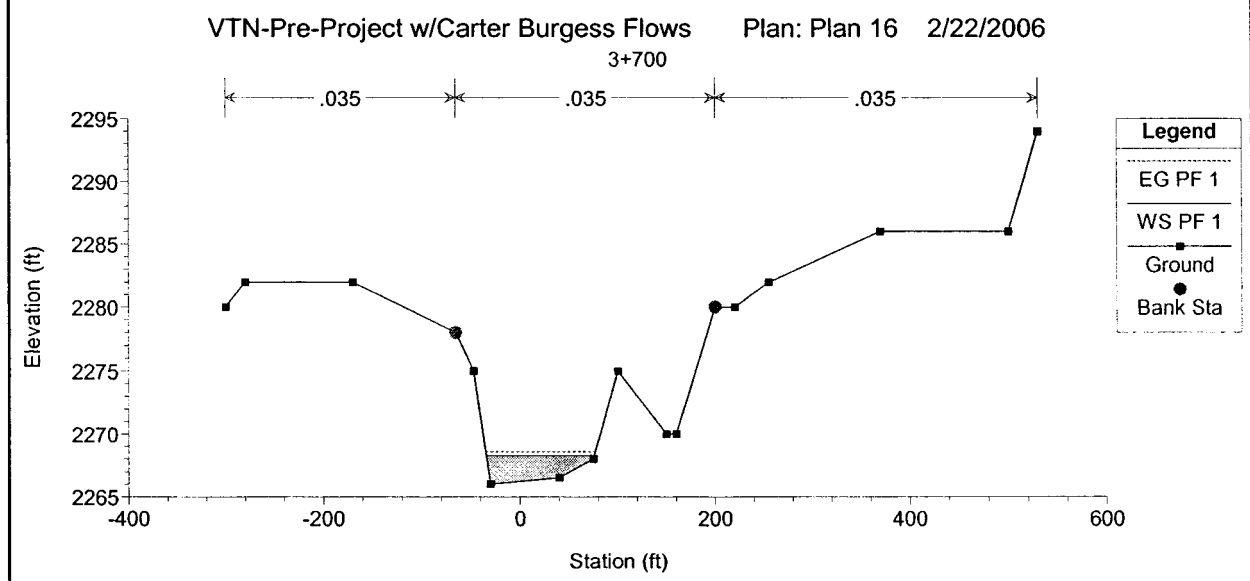
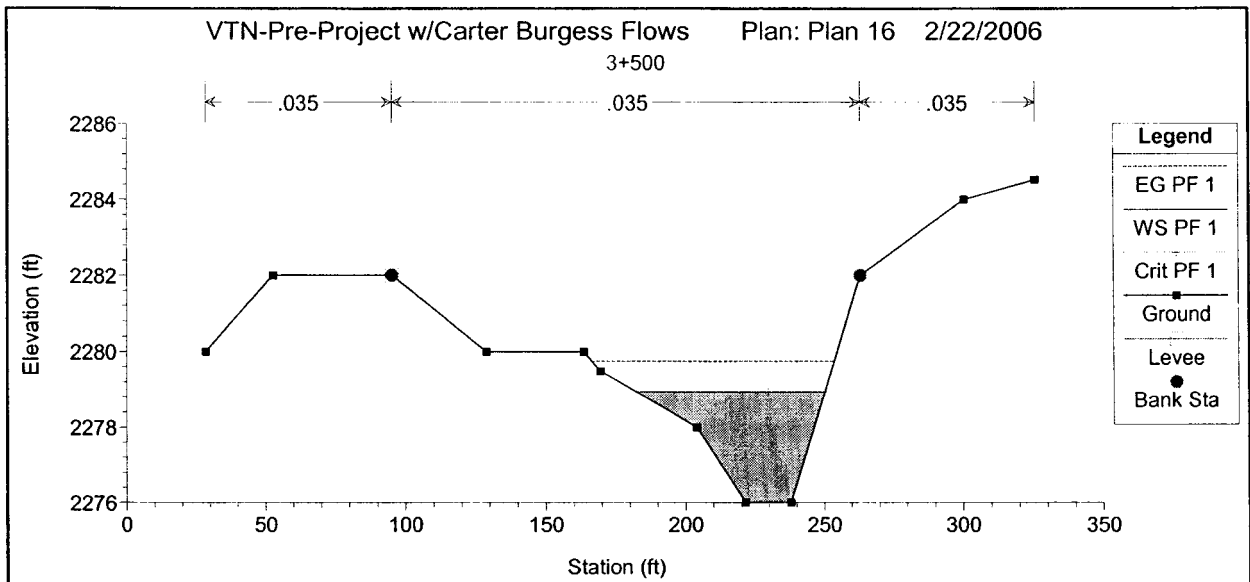


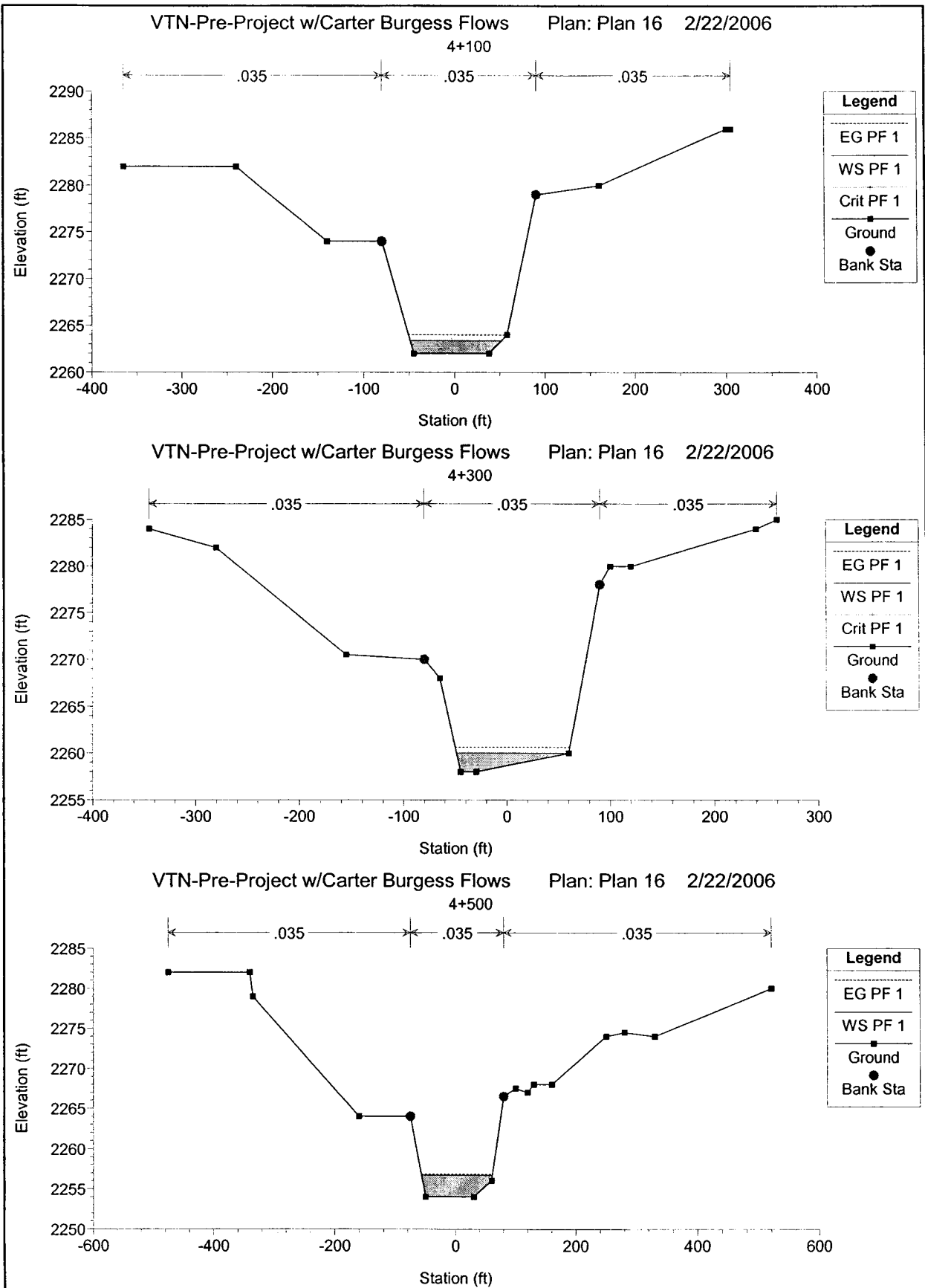
VTN-Pre-Project w/Carter Burgess Flows 3+300 Plan: Plan 16 2/22/2006



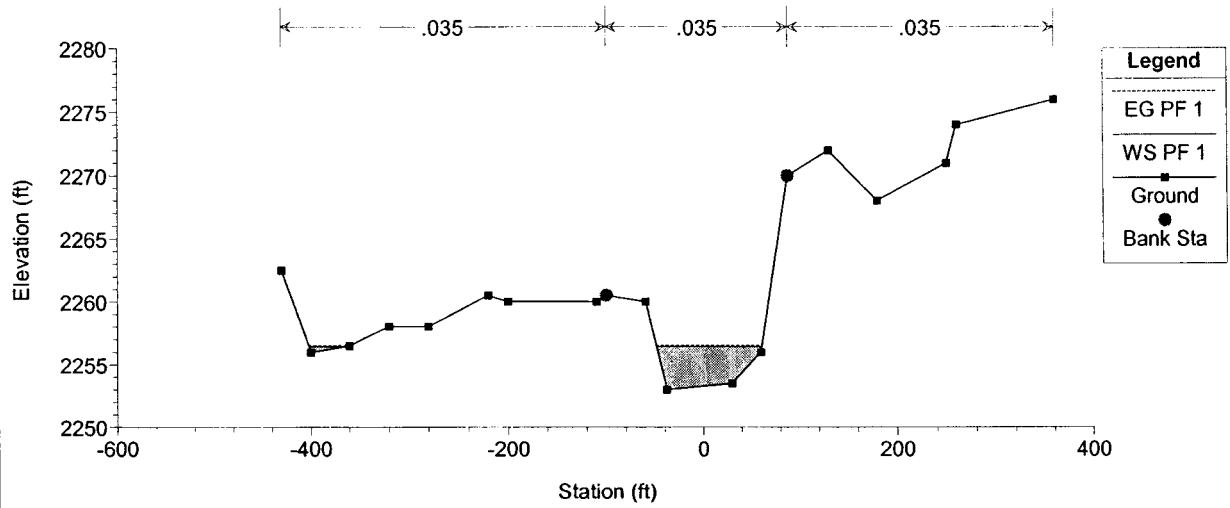
VTN-Pre-Project w/Carter Burgess Flows 3+400 Plan: Plan 16 2/22/2006



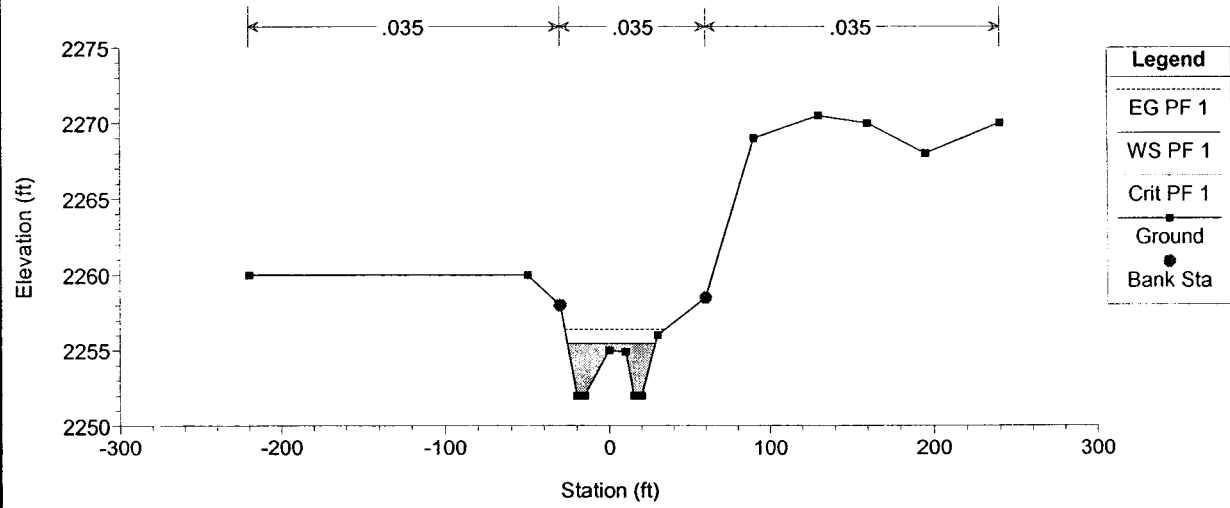




VTN-Pre-Project w/Carter Burgess Flows Plan: Plan 16 2/22/2006
4+700



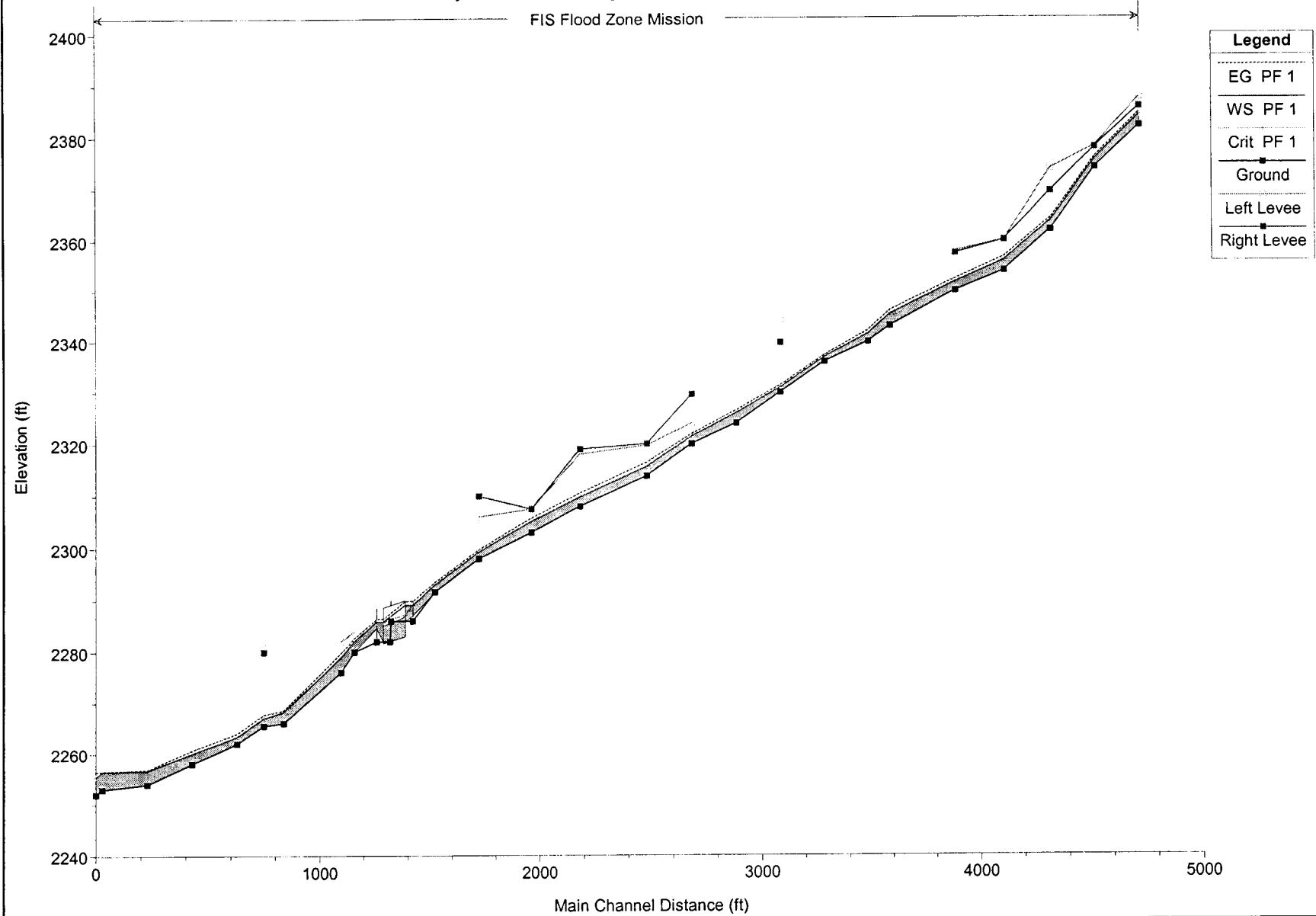
VTN-Pre-Project w/Carter Burgess Flows Plan: Plan 16 2/22/2006
4+729



VTN-Pre-Project w/Carter Burgess Flows

Plan: Plan 16 2/22/2006

FIS Flood Zone Mission



Reach	River Sta	Cross Section Sta.	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #	C Hydr Depth (ft)
Mission	48	0+100	PF 1	286	2382	2384.01	2384.01	2384.56	0.017231	5.95	48.1	43.38	0.99	1.11
Mission	46	0+300	PF 1	286	2374	2375.57	2375.57	2376.04	0.018018	5.5	52.03	54.8	0.99	0.95
Mission	44	0+500	PF 1	286	2362	2363.7	2363.7	2364.22	0.017427	5.76	49.67	47.47	0.99	1.05
Mission	42	0+700	PF 1	286	2354	2356.03	2356.03	2356.68	0.016645	6.48	44.13	33.92	1	1.3
Mission	40	0+900	PF 1	286	2350	2351.75	2351.75	2352.33	0.016829	6.07	47.11	40.34	0.99	1.17
Mission	37	1+200	PF 1	286	2343.07	2345.39	2345.39	2346.12	0.016468	6.85	41.74	28.9	1	1.44
Mission	36	1+300	PF 1	286	2340	2341.5	2341.5	2342.18	0.016839	6.62	43.2	32.14	1.01	1.34
Mission	34	1+500	PF 1	286	2336	2336.91	2336.91	2337.3	0.019602	5.03	56.81	72.54	1	0.78
Mission	32	1+700	PF 1	286	2330	2330.94	2330.94	2331.36	0.019354	5.2	55.01	66.41	1.01	0.83
Mission	30	1+900	PF 1	286	2324	2325.93	2325.93	2326.43	0.018576	5.64	50.67	52.44	1.01	0.97
Mission	28	2+100	PF 1	286	2320	2321.4	2321.4	2321.9	0.017379	5.66	50.54	49.56	0.99	1.02
Mission	26	2+300	PF 1	490	2313.84	2315.63	2315.63	2316.38	0.015633	6.92	70.82	47.12	0.99	1.5
Mission	24	2+500	PF 1	490	2308	2309.82	2309.82	2310.54	0.015585	6.81	71.98	49.11	0.99	1.47
Mission	22	2+700	PF 1	490	2303	2305.1	2305.1	2305.72	0.017022	6.28	77.98	64.26	1.01	1.21
Mission	20	2+900	PF 1	490	2298	2299.27	2299.27	2299.72	0.018289	5.42	90.41	97.87	0.99	0.92
Mission	19	3+000	PF 1	799	2291.63	2292.97	2292.97	2293.46	0.018683	5.59	142.93	150.98	1.01	0.95
Mission	18	3+100	PF 1	799	2287.03	2289.11	2289.11	2289.82	0.016733	6.74	118.63	83.5	0.9	1.42
Mission	17	Culvert		Culvert										
Mission	16	3+300	PF 1	799	2284.62	2285.85	2285.85	2286.34	0.019006	5.6	142.72	149.54	0.92	0.95
Mission	15	3+400	PF 1	799	2280	2282.07	2282.07	2282.61	0.01677	5.93	134.75	120.08	0.99	1.12
Mission	14	3+500	PF 1	799	2276	2278.94	2278.94	2279.75	0.015398	7.24	110.29	67.92	1	1.62
Mission	12	3+700	PF 1	799	2266	2268.24		2268.55	0.005851	4.47	178.76	110.09	0.62	1.62
Mission	10	3+900	PF 1	799	2265.5	2267.03	2267.03	2267.67	0.017824	6.4	124.87	103.76	1.03	1.2
Mission	8	4+100	PF 1	799	2262	2263.39	2263.37	2264	0.016007	6.27	127.52	100.91	0.98	1.26
Mission	6	4+300	PF 1	799	2258	2260.04	2260.04	2260.64	0.01759	6.24	127.99	109.13	1.02	1.17
Mission	4	4+500	PF 1	799	2254	2256.69		2256.82	0.001525	2.9	275.22	118.03	0.34	2.33
Mission	2	4+700	PF 1	799	2253	2256.42		2256.54	0.001225	2.79	292.06	145.36	0.31	2.01
Mission	1	4+729	PF 1	799	2252	2255.43	2255.43	2256.37	0.015443	7.8	102.43	54.29	1	1.89

**CORRECTIVE/EFFECTIVE
CHECK-RAS – (VTN) PRE PROJECT
HYDRAULIC MODEL
(022206.PRJ)**

CHECK-RAS PROGRAM: N1 CHECK
Manning's n Value and Transition Loss Coefficient Review

Project File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.prj
 Plan File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.pl6
 Geometry File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.g12
 Flow File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.f04
 Report File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.nt
 Selected profiles: PF 1
 Date: 3/2/2006
 Time: 10:47:17 AM

SECNO	STRUCTURE	NLOB	NCHL	NROB	CNTR	EXP

FIS Flood Zone,Mission						
48		0.035	0.035	0.035	0.1	0.3
46		0.035	0.035	0.035	0.1	0.3
44		0.035	0.035	0.035	0.1	0.3
42		0.035	0.035	0.035	0.1	0.3
40		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
37		0.035	0.035	0.035	0.1	0.3
36		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
34		0.035	0.035	0.035	0.1	0.3
32		0.035	0.035	0.035	0.1	0.3
30		0.035	0.035	0.035	0.1	0.3
28		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
26		0.035	0.035	0.035	0.1	0.3
24		0.035	0.035	0.035	0.1	0.3
22		0.035	0.035	0.035	0.1	0.3
20		0.035	0.035	0.035	0.1	0.3
19		0.035	0.035	0.035	0.1	0.3
18		0.035	0.035	0.035	0.1	0.3
17	Culvert-Up	0.035	0.035	0.035	0.1	0.3
17	Culvert-Dn	0.035	0.035	0.035	0.1	0.3
16		0.035	0.035	0.035	0.1	0.3
15		0.035	0.035	0.035	0.1	0.3
14		0.035	0.035	0.035	0.1	0.3
12		0.035	0.035	0.035	0.1	0.3
10		0.035	0.035	0.035	0.1	0.3
8		0.035	0.035	0.035	0.1	0.3
6		0.035	0.035	0.035	0.1	0.3
4		0.035	0.035	0.035	0.1	0.3
2		0.035	0.035	0.035	0.1	0.3
1		0.035	0.035	0.035	0.1	0.3

---Summary of Statistics---

	Minimum	Maximum
Left Overbank n Value:	0.035	0.035
Right Overbank n Value:	0.035	0.035
Channel n Value:	0.035	0.035
Contraction Coefficient:	0.1	0.1
Expansion Coefficient:	0.3	0.3

ROUGHNESS COEFFICIENT CHECK

RS: 48

NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
 The overbank n values should be reevaluated.

RS: 46

NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
 The overbank n values should be reevaluated.

RS: 44

NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
 The overbank n values should be reevaluated.

RS: 42

NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
 The overbank n values should be reevaluated.

RS: 37

NT RC 05 The left overbank n value of 0.035 and the right overbank n value

of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 6
NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 4
NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 2
NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

TRANSITION LOSS COEFFICIENT CHECK

RS: 19
NT TL 01 This is section 4
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

RS: 18
NT TL 01 This is section 3
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

RS: 16
NT TL 01 This is section 2
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

ROUGHNESS COEFFICIENT AT STRUCTURES

---END---

Project File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.prj
 Plan File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.pl6
 Geometry File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.g12
 Flow File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.f04
 Report File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.xls
 Selected profiles: PF 1
 Date: 3/2/2006
 Time: 10:47:40 AM

SECNO	Len Lob	Len Chl	Len Rob	TopWdthAct	Q Total	Flow Code

FIS Flood Zone, Mission						
48	200	200	200	43.38	286	C
46	200	200	200	54.8	286	C
44	400	210	200	47.47	286	C
42	220	220	350	33.92	286	C
40	300	300	300	40.34	286	C
37	100	100	100	28.9	286	C
36	200	200	200	32.14	286	C
34	250	200	200	72.54	286	D,C
32	200	200	200	66.41	286	E,C
30	200	200	200	52.44	286	C
28	210	200	200	49.56	286	E,C
26	300	300	330	47.12	490	E,C
24	220	220	270	49.11	490	E,C
22	230	240	240	64.26	490	E,C
20	200	200	200	97.87	490	D,C
19	100	100	100	150.98	799	C
18	165	165	165	83.5	799	C
17	Culvert #1-Up					
17	Culvert #1-Dn					
16	100	100	110	149.54	799	D,C
15	60	60	60	120.08	799	C
14	240	260	390	67.92	799	C
12	140	90	120	110.09	799	
10	110	120	125	103.76	799	C
8	200	200	200	100.91	799	
6	200	200	200	109.13	799	C
4	200	200	200	118.03	799	
2	29	29	29	145.36	799	D
1	0	0	0	54.29	799	C

B=blocked obstruction XS SC 05
 C=critical depth XS SC 03
 D=divided flow XS SC 01
 E=cross section extended XS SC 02
 K=known water-surface XS SC 04

DISTANCE CHECK

SPACING CHECK

INEFFECTIVE FLOW CHECK

RS: 48
 XS IF 01 Left Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 48
 XS IF 01 Right Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 46
 XS IF 01 Left Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 46
 XS IF 01 Right Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 44
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 44
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 42
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 42
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 40
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 40
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 32
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 32
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 28
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 28
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 26
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 26
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 24
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 24
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 22
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 22
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 20
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 20
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 15
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 14
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 10
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 10
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

DISCHARGE CHECK

LOCATION CHECK

RS: 46
XS LC 01 Lenchl Up/TopwdthAct Dn = 4.21
MaxChlDpth Up/MaxChlDpth Dn = 1.20
TopwdthAct Up/TopwdthAct Dn = 1.15
This cross section is located too far upstream from the
critical depth cross section.

RS: 44
XS LC 01 Lenchl Up/TopwdthAct Dn = 6.19
MaxChlDpth Up/MaxChlDpth Dn = 1.17
TopwdthAct Up/TopwdthAct Dn = 1.40
This cross section is located too far upstream from the
critical depth cross section.

RS: 32
XS LC 01 Lenchl Up/TopwdthAct Dn = 3.81
MaxChlDpth Up/MaxChlDpth Dn = 4.71
TopwdthAct Up/TopwdthAct Dn = 1.27
This cross section is located too far upstream from the
critical depth cross section.

BOUNDARY CONDITION CHECK

XS BC 02 The name of the stream is FIS Flood Zone,Mission
Normal S = 0.0229 is specified as the downstream boundary
for profile PF 1

XS BC 02 The name of the stream is FIS Flood Zone,Mission
Critical is specified as the upstream boundary
for profile PF 1

XS BC 03 Maximum number of iterations is 0
It should not be less than 20.

XS FR 01 The profile is computed as supercritical flow regime.

LATERAL WEIRS CHECK

---END---

CHECK-RAS Program: Structure Check

Project File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.prj
 Plan File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.pl6
 Geometry File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.g12
 Flow File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.f04
 Report File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\Carter Burgess FIS Post Flows- VTN Model\022206.br
 Selected profiles: PF 1
 Date: 3/2/2006
 Time: 10:47:51 AM

RS	MaxLoChord	MnTpRd	EGEL	WSEL	MinChEl	Structure
FIS Flood Zone, Mission						
48			2384.56	2384.01	2382	
46			2376.04	2375.57	2374	
44			2364.22	2363.7	2362	
42			2356.68	2356.03	2354	
40			2352.33	2351.75	2350	
37			2346.12	2345.39	2343.07	
36			2342.18	2341.5	2340	
34			2337.3	2336.91	2336	
32			2331.36	2330.94	2330	
30			2326.43	2325.93	2324	
28			2321.9	2321.4	2320	
26			2316.38	2315.63	2313.84	
24			2310.54	2309.82	2308	
22			2305.72	2305.1	2303	
20			2299.72	2299.27	2298	
19			2293.46	2292.97	2291.63	
18			2289.82	2289.11	2287.03	Lid
17	2290	2286	0	2287.21	2283	Culvert #1-Up
17	2288.6	2282	0	2285.08	2281.6	Culvert #1-Dn
16			2286.34	2285.85	2284.62	Lid
15			2282.61	2282.07	2280	
14			2279.75	2278.94	2276	
12			2268.55	2268.24	2266	
10			2267.67	2267.03	2265.5	
8			2264	2263.39	2262	
6			2260.64	2260.04	2258	
4			2256.82	2256.69	2254	
2			2256.54	2256.42	2253	
1			2256.37	2255.43	2252	

RIVER/REACH: FIS Flood Zone, Mission
 RIVER STATION: 17
 TYPE OF STRUCTURE: Culvert

Description:

Distance from Upstream XS: 100
 Deck/Roadway Width: 4
 Weir Coefficient: 2.6
 Maximum allowable submergence for weir flow: 0.95
 Elevation at which weir flow begins: 0
 Weir crest shape: Broad Crested

Sec	River Station	Length Channel	WSEL	Surch.	EGEL	TopWidth Actual
4	19	100.00	2292.97		2293.46	150.98
3	18	165.00	2289.11		2289.82	83.5
	17	100.00	2287.21		0	0
	17	30.00	2285.08		0	0
2	16	100.00	2285.85		2286.34	149.54
1	15	60.00	2282.07		2282.61	120.08

Ineffective Flow, Section 3
 Sta L Sta R Elev

Ineffective Flow, Section 2
 Sta L Sta R Elev

Opening Type StagStaL StagStaR EncStaL EncStaR LIfStaS RIfStaS
 Culvert Group

U
D

CULVERT:

Culvert Name: Culvert #1

Shape: Box Rise: 7 Span: 4 Barrels: 1

FHWA Chart #: # 8 - flared wingwalls

FHWA Scale #: # 1 - Wingwall flared 30 to 75 deg.

Solution Crit: Highest U.S. EG

UpstrmDist: 35 Length: 100 n-Value: 0.014
 EntLossCoef: 0.05 ExtLossCoef: 1 CulvInvElU 2283 CulvInvElD 2281.6
 LCntStaU: 223.03 RCntStaU: 223.03 LCntStaD 262.31 RCntStaD 262.31
 Culvert Depth Blocked: 0

 Culv Area: 28 CulvQ: 196.19 MinTopRd: 2286.01

	LAbutSt	RAbutSt	LMnTpRd	RMnTpRd	MnTpRd	MxLoCd	
Culvert #1	221.03	225.03	2286	2286	2286	2290	U
	260.31	264.31	2282	2282	2282	2288.6	D

Name	Q Total.	Q Struc	Q Weir	Selected Method	Flow Type
Culvert #1		196.19	602.81	Highest U.S. EG	Low and Weir Flow

GEOMETRIC CHECK

RS: 17

ST GD 03 The starting station of 221.03 from upstream road/weir data is greater than the starting station of 41.32 from upstream internal section/ section 3.
 The high chord elevation of 2291 for the starting road/weir station is greater than the ground elevation of 2286 for the same ground station.
 The road/weir profile may need to be extended.

RS: 17

ST GD 03 The end station of 225.03 from upstream road/weir data is less than the end station of 432.4 from upstream internal section/section 3.
 The high chord elevation of 2291 for the end road/weir station is greater than the ground elevation of 2286 for the same ground station.
 The road/weir profile may need to be extended.

RS: 17

ST GD 03 The starting station of 260.31 from downstream road/weir data is greater than the starting station of 48.08 from downstream internal section.
 The high chord elevation of 2289.6 for the starting road/weir station is greater than the ground elevation of 2282 for the same ground station.
 The road/weir profile may need to be extended.

RS: 17

ST GD 03 The end station of 264.31 from downstream road/weir data is less than the end station of 413.53 from downstream internal section.
 The high chord elevation of 2289.6 for the end road/weir station is greater than the ground elevation of 2282.826 for the same ground station.
 The road/weir profile may need to be extended.

RS: 16

ST GD 08 'Cross Section Lid' option is used for this section.
 Cross section lid data must be removed from this section, unless the structure is modeled as culverts in series.

RS: 18

ST GD 08 'Cross Section Lid' option is used for this section.
 Cross section lid data must be removed from this section, unless the structure is modeled as culverts in series.

TYPE OF FLOW CHECK

RS: 17 This is Culvert #1

CV LW 01 Type of flow is low and weir flow because,
 1. EGEL 3 of 2289.82 is greater than MinTopRd of 2286.01.
 2. EGEL 3 of 2289.82 is less than MxLoCdU of 2290.00.

RS: 17 This is Culvert #1

CV LW 01 Type of flow is low and weir flow because,
 1. EGEL 3 of 2289.82 is greater than MinTopRd of 2286.01.

2. CulvWSIn of 2287.21 is less than MxLoCdU of 2290.00.
3. CulvWSOut of 2285.08 is less than MxLoCdD of 2288.60.
4. $Q/AD^{0.5}$ of 2.65 is less than 4.0.

DISTANCE CHECK

CULVERT COEFFICIENT CHECK

RS: 17 This is Culvert #1
CV CF 01 Culvert Chart # is 8 and Scale # is 1
Culvert entrance shape is Wingwall flared 30 to 75 deg.
Culvert entrance loss coefficient is 0.05 It should be equal
to 0.4
Please refer to Table 6.3 on page 6-22 and Tabble 6.4 on page 6-23
of HEC-RAS Hydraulic Reference Manual, September 1998.

CULVERT CRITERIA CHECK

INEFFECTIVE FLOW CHECK

RS: 18 This is section 3
ST GD 05 Weir flow occurs at Culvert Group 1
The velocity head at Section 3 is more than 0.5 foot and more than
the velocity head at Section 4.
Section 3 should be recoded to represent the natural valley
cross section.

---END

POST- PROJECT CONDITIONS (VTN): HEC-RAS OUTPUT
(USED VTN HEC-1 POST-PROJECT
CONDITIONS FOR FLOWS)

HEC-RAS Version 3.1.3 May 2005
U.S. Army Corp of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

```

X   X   XXXXXX   XXXX   XXXX   XX   XXXX
X   X   X   X   X   X   X   X   X   X
X   X   X   X   X   X   X   X   X   X
XXXXXXXX XXXX   X   XXX XXXX XXXXXX XXXX
X   X   X   X   X   X   X   X   X   X
X   X   X   X   X   X   X   X   X   X
X   X   XXXXXX   XXXX   X   X   X   XXXX

```

PROJECT DATA
Project Title: Mission-Post Dev 02-26-06
Project File : 022606.prj
Run Date and Time: 2/26/2006 4:21:33 PM

Project in English units

Project Description:
Mission LOMR Post-Conditions-VTN

PLAN DATA

Plan Title: Post-Project 02-26-06
Plan File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.pl5
Geometry Title: post test 02-08-06
Geometry File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.g11
Flow Title : Post Conditions
Flow File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.f04

Plan Summary Information:
Number of: Cross Sections = 27 Multiple Openings = 0
Culverts = 1 Inline Structures = 0
Bridges = 0 Lateral Structures = 0

Computational Information
Water surface calculation tolerance = 0.01
Critical depth calculation tolerance = 0.01
Maximum number of iterations = 20
Maximum difference tolerance = 0.3
Flow tolerance factor = 0.001

Computation Options
Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: Post Conditions
Flow File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.f04

Flow Data (cfs)

* River Reach RS * PF 1 *
* FIS Flood Zone Mission 48 * 157 *
* FIS Flood Zone Mission 26 * 166 *
* FIS Flood Zone Mission 19 * 204 *
* FIS Flood Zone Mission 12 * 602 *

Boundary Conditions

* River Reach Profile * Upstream Downstream *
* FIS Flood Zone Mission PF 1 * Critical Normal S = 0.0229 *

GEOMETRY DATA

Geometry Title: post test 02-08-06
Geometry File : j:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.g11

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 48

INPUT
Description: 0+100
Station Elevation Data num= 27
Sta Elev Sta Elev Sta Elev Sta Elev

-173.84 2392 -118.84 2391.68 -58.01 2388 -42.83 2387.43 21.55 2382
28.51 2382 38.23 2383.92 97.69 2385.67 123.66 2384.09 145.04 2380
256.2 2378.52 338.85 2376 371.85 2381.52 376.8 2380 389.09 2382
423.32 2374.68 446.53 2376 457.06 2378 484.25 2378 508.7 2372.78
524.94 2376 555.62 2376 567.65 2370 591.28 2370 609.45 2372
628.27 2372 682.75 2401.51

Manning's n Values num= 3
Sta n Val Sta n Val

-173.84 .035 -118.84 .035 97.69 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
-118.84 97.69 200 200
Left Levee Station= -42.83 Elevation= 2387.43
Right Levee Station= 97.69 Elevation= 2385.67

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft) * 2383.94 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.45 * Wt. n-Val. * 0.035 *
* W.S. Elev (ft) * 2383.50 * Reach Len. (ft) * 200.00 * 200.00 * 200.00 *
* Crit W.S. (ft) * 2383.50 * Flow Area (sq ft) * 29.32 *
* E.G. Slope (ft/ft) * 0.018231 * Area (sq ft) * 29.32 *
* Q Total (cfs) * 157.00 * Flow (cfs) * 157.00 *
* Top Width (ft) * 32.26 * Top Width (ft) * 32.26 *


```

022606.rep
* Vel Total (ft/s)      * 5.36 * Avg. Vel. (ft/s)      * 5.36 *
* Max Chl Dpth (ft)    * 13.50 * Hydr. Depth (ft)      * 0.91 *
* Conv. Total (cfs)    * 1162.8 * Conv. (cfs)           * 1162.8 *
* Length Wtd. (ft)     * 200.00 * Wetted Per. (ft)      * 32.47 *
* Min Ch El (ft)       * 2382.00 * Shear (lb/sq ft)      * 1.03 *
* Alpha                * 1.00 * Stream Power (lb/ft s) * 5.50 *
* Frctn Loss (ft)      * 0.21 * Cum Volume (acre-ft)  * 6.31 *
* C & E Loss (ft)      * 0.04 * Cum SA (acres)        * 6.38 *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 46

INPUT

Description: 0+300

Station	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-84.97	2384.63	6.45	2378.12	25.09	2376.04	53.39	2374	64.77	2374
117.96	2377.87	218.54	2376	266.82	2367.72	294.84	2367.11	312.32	2368
366.86	2367.89	383.36	2368.35	447.53	2368	474.66	2367.16	514.95	2379.89
554.18	2380.42	601.91	2379.58	617.76	2376	641.09	2376.13	683.46	2387.18

Manning's n values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-84.97	.035	6.45	.035	117.96	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
Left Levee	6.45	117.96	200	200	200	.1	.3
Right Levee	Station=	6.45	Elevation=	2378.12			
	Station=	117.96	Elevation=	2377.87			

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2375.54	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.37	* Wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2375.17	* Reach Len. (ft)	* 200.00	* 200.00	* 200.00
* Crit W.S. (ft)	* 2375.17	* Flow Area (sq ft)		* 32.34	
* E.G. Slope (ft/ft)	* 0.019624	* Area (sq ft)		* 32.34	
* Q Total (cfs)	* 157.00	* Flow (cfs)		* 157.00	
* Top Width (ft)	* 43.77	* Top width (ft)		* 43.77	
* Vel Total (ft/s)	* 4.85	* Avg. Vel. (ft/s)		* 4.85	
* Max Chl Dpth (ft)	* 8.06	* Hydr. Depth (ft)		* 0.74	
* Conv. Total (cfs)	* 1120.8	* Conv. (cfs)		* 1120.8	
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)		* 43.85	
* Min Ch El (ft)	* 2374.00	* Shear (lb/sq ft)		* 0.90	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 4.39	
* Frctn Loss (ft)	* 0.60	* Cum Volume (acre-ft)		* 6.17	
* C & E Loss (ft)	* 0.03	* Cum SA (acres)		* 6.21	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 44

INPUT

Description: 0+500

Station	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-49.81	2378.58	46.88	2373.73	87.47	2363.08	121.51	2362	160.53	2368
195.41	2369.5	229.76	2368	247.29	2362	299.43	2362	354.98	2366
437.9	2366	457.32	2358.25	476.17	2356.64	598.56	2368.16	646.7	2368
681.22	2382								

Manning's n values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-49.81	.035	46.88	.035	195.41	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
Left Levee	46.88	195.41	400	210	200	.1	.3
Right Levee	Station=	46.88	Elevation=	2373.73			
	Station=	195.41	Elevation=	2369.5			

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2363.69	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.37	* Wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2363.31	* Reach Len. (ft)	* 400.00	* 210.00	* 200.00
* Crit W.S. (ft)	* 2363.31	* Flow Area (sq ft)		* 32.04	
* E.G. Slope (ft/ft)	* 0.020097	* Area (sq ft)		* 32.04	
* Q Total (cfs)	* 157.00	* Flow (cfs)		* 157.00	
* Top Width (ft)	* 43.47	* Top width (ft)		* 43.47	
* Vel Total (ft/s)	* 4.90	* Avg. Vel. (ft/s)		* 4.90	
* Max Chl Dpth (ft)	* 6.67	* Hydr. Depth (ft)		* 0.74	
* Conv. Total (cfs)	* 1107.5	* Conv. (cfs)		* 1107.5	
* Length Wtd. (ft)	* 210.00	* Wetted Per. (ft)		* 43.62	
* Min Ch El (ft)	* 2362.00	* Shear (lb/sq ft)		* 0.92	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 4.52	
* Frctn Loss (ft)	* 1.09	* Cum Volume (acre-ft)		* 6.02	
* C & E Loss (ft)	* 0.04	* Cum SA (acres)		* 6.01	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 42

INPUT

Description: 0+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-3.26	2370.96	20.48	2360	109.52	2357.99	127.31	2354	136.96	2354
166.31	2357.9	208.45	2358.52	227.77	2360	247.65	2360	277.16	2361.97
277.27	2361.97	277.77	2361.97	331.57	2362	383.73	2364	399.01	2364
442.36	2362	462.45	2360	479.15	2352.13	490.21	2352	515.36	2354
540	2352	597	2350	627.49	2362				

Manning's n values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-3.26	.035	20.48	.035	227.77	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 20.48 227.77 220 220 220 220
 Left Levee Station= 20.48 Elevation= 2360
 Right Levee Station= 227.77 Elevation= 2360

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2355.99	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.49	* Wt. n-Val.	* 220.00	* 0.035	* 350.00
* W.S. Elev (ft)	* 2355.50	* Reach Len. (ft)			
* Crit W.S. (ft)	* 2355.50	* Flow Area (sq ft)		* 27.86	
* E.G. Slope (ft/ft)	* 0.017604	* Area (sq ft)		* 27.86	
* Q Total (cfs)	* 157.00	* Flow (cfs)		* 157.00	
* Top Width (ft)	* 27.59	* Top Width (ft)		* 27.59	
* Vel Total (ft/s)	* 5.63	* Avg. Vel. (ft/s)		* 5.63	
* Max Chl Dpth (ft)	* 5.50	* Hydr. Depth (ft)		* 1.01	
* Conv. Total (cfs)	* 1183.3	* Conv. (cfs)		* 1183.3	
* Length Wtd. (ft)	* 220.00	* Wetted Per. (ft)		* 27.85	
* Min Ch El (ft)	* 2354.00	* Shear (lb/sq ft)		* 1.10	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 6.20	
* Frctn Loss (ft)	* 2.44	* Cum Volume (acre-ft)		* 5.87	
* C & E Loss (ft)	* 0.02	* Cum SA (acres)		* 5.84	

Warning: The energy equation could not be balanced within the specified number of iterations. The program selected the water surface that had the least amount of error between computed and assumed values.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 40

INPUT

Description: 0+900

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
40.76	2357.87	138.91	2350	152.31	2350	169.69	2356
265.62	2357.42	382.86	2358	382.96	2358	425.96	2356
524.35	2358	550.64	2348	568.55	2348		

Manning's n values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
40.76	.035	138.91	.035	382.96	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 40.76 382.96 300 300 300 300
 Left Levee Station= 40.76 Elevation= 2357.87
 Right Levee Station= 265.62 Elevation= 2357.42

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2351.71	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.45	* Wt. n-Val.	* 300.00	* 0.035	* 300.00
* W.S. Elev (ft)	* 2351.26	* Reach Len. (ft)			
* Crit W.S. (ft)	* 2351.26	* Flow Area (sq ft)		* 29.21	
* E.G. Slope (ft/ft)	* 0.018922	* Area (sq ft)		* 29.21	
* Q Total (cfs)	* 157.00	* Flow (cfs)		* 157.00	
* Top Width (ft)	* 32.82	* Top Width (ft)		* 32.82	
* Vel Total (ft/s)	* 5.37	* Avg. Vel. (ft/s)		* 5.37	
* Max Chl Dpth (ft)	* 3.26	* Hydr. Depth (ft)		* 0.89	
* Conv. Total (cfs)	* 1141.3	* Conv. (cfs)		* 1141.3	
* Length Wtd. (ft)	* 300.00	* Wetted Per. (ft)		* 33.09	
* Min Ch El (ft)	* 2350.00	* Shear (lb/sq ft)		* 1.04	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 5.61	
* Frctn Loss (ft)	* 5.30	* Cum Volume (acre-ft)		* 5.73	
* C & E Loss (ft)	* 0.01	* Cum SA (acres)		* 5.69	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 37

INPUT

Description: 1+200

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-73.3	2350	-64.13	2348	17.29	2348	31.09	2350.31	43.06	2350.77
67.84	2350	109.53	2349.52	129.54	2348	141.96	2348	160.5	2347.44
203.41	2347.05	213.19	2346.2	231.47	2345.27	237.84	2343.07	254.96	2344
263.97	2348	292.81	2348.8	430.54	2347.99	447.09	2346.43	482.21	2348.76
508.61	2349.28	538.41	2348.38	604.11	2349.14	661.33	2347.98		

Manning's n values num= 3
 Sta n Val Sta n Val Sta n Val
 -73.3 .035 43.06 .035 508.61 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 43.06 508.61 100 100 100 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2345.34 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.55 * Wt. n-Val. * 100.00 * 100.00 * 100.00 *
* W.S. Elev (ft) * 2344.78 * Reach Len. (ft) * * * *
* Crit W.S. (ft) * 2344.78 * Flow Area (sq ft) * * 26.27 * *
* E.G. Slope (ft/ft) * 0.017879 * Area (sq ft) * * 26.27 * *
* Q Total (cfs) * 157.00 * Flow (cfs) * * 157.00 * *
* Top Width (ft) * 23.84 * Top Width (ft) * * 23.84 * *
* Vel Total (ft/s) * 5.98 * Avg. Vel. (ft/s) * * 5.98 * *
* Max Chl Dpth (ft) * 1.71 * Hydr. Depth (ft) * * 1.10 * *
* Conv. Total (cfs) * 1174.2 * Conv. (cfs) * * 1174.2 * *
* Length Wtd. (ft) * 100.00 * Wetted Per. (ft) * * 24.31 * *
* Min Ch El (ft) * 2343.07 * Shear (lb/sq ft) * * 1.21 * *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 7.21 * *
* Frctn Loss (ft) * 1.83 * Cum Volume (acre-ft) * * 5.54 * *
* C & E Loss (ft) * 0.02 * Cum SA (acres) * * 5.49 * *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 36

INPUT

Description: 1+300

Station Elevation Data num= 12
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
 45.57 2347.92 159.01 2344 180.69 2344 189.27 2340 214.78 2340
 230.59 2346.93 271.17 2348 280.07 2346.31 427.63 2344 456.67 2346
 512.55 2346.25 652.62 2345.86

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 45.57 .035 45.57 .035 456.67 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 45.57 456.67 200 200 200 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2341.50 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.47 * Wt. n-Val. * 200.00 * 200.00 * 200.00 *
* W.S. Elev (ft) * 2341.02 * Reach Len. (ft) * * * *
* Crit W.S. (ft) * 2341.02 * Flow Area (sq ft) * * 28.40 * *
* E.G. Slope (ft/ft) * 0.018636 * Area (sq ft) * * 28.40 * *
* Q Total (cfs) * 157.00 * Flow (cfs) * * 157.00 * *
* Top Width (ft) * 30.04 * Top Width (ft) * * 30.04 * *
* Vel Total (ft/s) * 5.53 * Avg. Vel. (ft/s) * * 5.53 * *
* Max Chl Dpth (ft) * 1.02 * Hydr. Depth (ft) * * 0.95 * *
* Conv. Total (cfs) * 1150.1 * Conv. (cfs) * * 1150.1 * *
* Length Wtd. (ft) * 200.00 * Wetted Per. (ft) * * 30.48 * *
* Min Ch El (ft) * 2340.00 * Shear (lb/sq ft) * * 1.08 * *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 5.99 * *
* Frctn Loss (ft) * 4.03 * Cum Volume (acre-ft) * * 5.48 * *
* C & E Loss (ft) * 0.06 * Cum SA (acres) * * 5.43 * *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 34

INPUT

Description: 1+500

Station Elevation Data num= 19
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
 -186.26 2346 -148.74 2345.86 -54.8 2339.88 22.59 2339.59 62.76 2340
 115.82 2340.55 160.63 2340.07 209.66 2338 219.09 2336 254.24 2336
 273.6 2340.11 310.56 2340 331.1 2336 349.75 2336.04 387.82 2342
 448.56 2345.82 490.03 2346.79 514.61 2346.13 602.59 2338

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 -186.26 .035 -148.74 .035 448.56 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -148.74 448.56 250 200 200 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

```

*****
* E.G. Elev (ft) * 2336.90 * Element * Left OB * Channel * Right OB *
* Vel Head (ft) * 0.28 * Wt. n-Val. * 250.00 * 200.00 * 200.00 *
* W.S. Elev (ft) * 2336.62 * Reach Len. (ft) * * * *
* Crit W.S. (ft) * 2336.62 * Flow Area (sq ft) * * 37.07 * *
* E.G. Slope (ft/ft) * 0.021830 * Area (sq ft) * * 37.07 * *
* Q Total (cfs) * 157.00 * Flow (cfs) * * 157.00 * *
* Top Width (ft) * 66.60 * Top Width (ft) * * 66.60 * *
* Vel Total (ft/s) * 4.23 * Avg. Vel. (ft/s) * * 4.23 * *
* Max Chl Dpth (ft) * 0.62 * Hydr. Depth (ft) * * 0.56 * *
* Conv. Total (cfs) * 1062.6 * Conv. (cfs) * * 1062.6 * *
* Length Wtd. (ft) * 200.00 * Wetted Per. (ft) * * 66.84 * *
* Min Ch El (ft) * 2336.00 * Shear (lb/sq ft) * * 0.76 * *
* Alpha * 1.00 * Stream Power (lb/ft s) * * 3.20 * *
* Frctn Loss (ft) * 4.54 * Cum Volume (acre-ft) * * 3.31 * *
* C & E Loss (ft) * 0.00 * Cum SA (acres) * * 2.21 * *
*****

```

Warning: The energy equation could not be balanced within the specified number of iterations. The

Warning: program used critical depth for the water surface and continued on with the calculations.
 Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 32

INPUT

Description: 1+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-284.04	2344	-243.74	2344	-118.46	2337.35	-75.6	2336.84	-46.51	2334
-13.99	2334	27.6	2335.17	168.04	2334.99	253.22	2333.67	295.68	2330
348.33	2330.04	360.87	2334	437.29	2338	497.79	2339.78	616.37	2334
631.42	2333.89	653.39	2332.06	689.8	2321.85				

Sta	n Val	Sta	n Val	Sta	n Val
-284.04	.035	-243.74	.035	497.79	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
Left Levee	-243.74	497.79	200	200	200	.1	.3	
Right Levee	Station=	-243.74	Elevation=	2344				
	Station=	497.79	Elevation=	2339.78				

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2330.94	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.31	* Wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2330.63	* Reach Len. (ft)	* 200.00	* 200.00	* 200.00
* Crit W.S. (ft)	* 2330.63	* Flow Area (sq ft)		* 35.11	
* E.G. Slope (ft/ft)	* 0.023667	* Area (sq ft)		* 35.11	
* Q Total (cfs)	* 157.00	* Flow (cfs)		* 157.00	
* Top Width (ft)	* 61.84	* Top Width (ft)		* 61.84	
* Vel Total (ft/s)	* 4.47	* Avg. Vel. (ft/s)		* 4.47	
* Max Chl Dpth (ft)	* 8.78	* Hydr. Depth (ft)		* 0.57	
* Conv. Total (cfs)	* 1020.5	* Conv. (cfs)		* 1020.5	
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)		* 61.96	
* Min Ch El (ft)	* 2330.00	* Shear (lb/sq ft)		* 0.84	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 3.74	
* Frctn Loss (ft)	* 0.22	* Cum Volume (acre-ft)		* 5.16	
* C & E Loss (ft)	* 0.04	* Cum SA (acres)		* 4.91	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 30

INPUT

Description: 1+900

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-250.32	2336.65	-126.77	2324	-102.3	2328	-79.42	2326.47	-53.84	2328
15.58	2329.84	173.54	2329.68	248.4	2330	274.21	2326	307.47	2324
329.12	2326.06	356.58	2326	431.57	2334.48	494.85	2334.48	604.27	2328
621.53	2328.89	638.68	2328.1						

Sta	n Val	Sta	n Val	Sta	n Val
-250.32	.035	-126.77	.035	431.57	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
Left Levee	-126.77	431.57	200	200	200	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2325.91	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft) <td>* 0.39 <td>* Wt. n-Val. <td>* 0.035</td> <td></td> <td></td> </td></td>	* 0.39 <td>* Wt. n-Val. <td>* 0.035</td> <td></td> <td></td> </td>	* Wt. n-Val. <td>* 0.035</td> <td></td> <td></td>	* 0.035		
* W.S. Elev (ft) <td>* 2325.52 <td>* Reach Len. (ft) <td>* 200.00</td> <td>* 200.00</td> <td>* 200.00</td> </td></td>	* 2325.52 <td>* Reach Len. (ft) <td>* 200.00</td> <td>* 200.00</td> <td>* 200.00</td> </td>	* Reach Len. (ft) <td>* 200.00</td> <td>* 200.00</td> <td>* 200.00</td>	* 200.00	* 200.00	* 200.00
* Crit W.S. (ft) <td>* 2325.52 <td>* Flow Area (sq ft) <td></td> <td>* 31.34</td> <td></td> </td></td>	* 2325.52 <td>* Flow Area (sq ft) <td></td> <td>* 31.34</td> <td></td> </td>	* Flow Area (sq ft) <td></td> <td>* 31.34</td> <td></td>		* 31.34	
* E.G. Slope (ft/ft) <td>* 0.020153 <td>* Area (sq ft) <td></td> <td>* 31.34</td> <td></td> </td></td>	* 0.020153 <td>* Area (sq ft) <td></td> <td>* 31.34</td> <td></td> </td>	* Area (sq ft) <td></td> <td>* 31.34</td> <td></td>		* 31.34	
* Q Total (cfs) <td>* 157.00 <td>* Flow (cfs) <td></td> <td>* 157.00</td> <td></td> </td></td>	* 157.00 <td>* Flow (cfs) <td></td> <td>* 157.00</td> <td></td> </td>	* Flow (cfs) <td></td> <td>* 157.00</td> <td></td>		* 157.00	
* Top Width (ft) <td>* 41.25 <td>* Top Width (ft) <td></td> <td>* 41.25</td> <td></td> </td></td>	* 41.25 <td>* Top Width (ft) <td></td> <td>* 41.25</td> <td></td> </td>	* Top Width (ft) <td></td> <td>* 41.25</td> <td></td>		* 41.25	
* Vel Total (ft/s) <td>* 5.01 <td>* Avg. Vel. (ft/s) <td></td> <td>* 5.01</td> <td></td> </td></td>	* 5.01 <td>* Avg. Vel. (ft/s) <td></td> <td>* 5.01</td> <td></td> </td>	* Avg. Vel. (ft/s) <td></td> <td>* 5.01</td> <td></td>		* 5.01	
* Max Chl Dpth (ft) <td>* 1.52 <td>* Hydr. Depth (ft) <td></td> <td>* 0.76</td> <td></td> </td></td>	* 1.52 <td>* Hydr. Depth (ft) <td></td> <td>* 0.76</td> <td></td> </td>	* Hydr. Depth (ft) <td></td> <td>* 0.76</td> <td></td>		* 0.76	
* Conv. Total (cfs) <td>* 1105.9 <td>* Conv. (cfs) <td></td> <td>* 1105.9</td> <td></td> </td></td>	* 1105.9 <td>* Conv. (cfs) <td></td> <td>* 1105.9</td> <td></td> </td>	* Conv. (cfs) <td></td> <td>* 1105.9</td> <td></td>		* 1105.9	
* Length Wtd. (ft) <td>* 200.00 <td>* Wetted Per. (ft) <td></td> <td>* 41.36</td> <td></td> </td></td>	* 200.00 <td>* Wetted Per. (ft) <td></td> <td>* 41.36</td> <td></td> </td>	* Wetted Per. (ft) <td></td> <td>* 41.36</td> <td></td>		* 41.36	
* Min Ch El (ft) <td>* 2324.00 <td>* Shear (lb/sq ft) <td></td> <td>* 0.95</td> <td></td> </td></td>	* 2324.00 <td>* Shear (lb/sq ft) <td></td> <td>* 0.95</td> <td></td> </td>	* Shear (lb/sq ft) <td></td> <td>* 0.95</td> <td></td>		* 0.95	
* Alpha <td>* 1.00 <td>* Stream Power (lb/ft s) <td></td> <td>* 4.78</td> <td></td> </td></td>	* 1.00 <td>* Stream Power (lb/ft s) <td></td> <td>* 4.78</td> <td></td> </td>	* Stream Power (lb/ft s) <td></td> <td>* 4.78</td> <td></td>		* 4.78	
* Frctn Loss (ft) <td>* 4.00 <td>* Cum Volume (acre-ft) <td></td> <td>* 5.01</td> <td></td> </td></td>	* 4.00 <td>* Cum Volume (acre-ft) <td></td> <td>* 5.01</td> <td></td> </td>	* Cum Volume (acre-ft) <td></td> <td>* 5.01</td> <td></td>		* 5.01	
* C & E Loss (ft) <td>* 0.00 <td>* Cum SA (acres) <td></td> <td>* 4.67</td> <td></td> </td></td>	* 0.00 <td>* Cum SA (acres) <td></td> <td>* 4.67</td> <td></td> </td>	* Cum SA (acres) <td></td> <td>* 4.67</td> <td></td>		* 4.67	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 28

INPUT

Description: 2+100

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-233.84	2330.42	-84.24	2324	-66.89	2324	-53.02	2320	-18.78	2321.74
3.04	2324	16.5	2322	25.01	2324	63.16	2323.8	91.57	2322.33
170.95	2323.22	247.57	2324	273.66	2320	296.16	2320	360	2325
420.77	2329.64	473.24	2330.78	579.4	2322	646.84	2321.94	675.91	2312.1

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val

 -233.84 .035 -233.84 .035 420.77 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -233.84 420.77 210 200
 Left Levee Station= 247.57 Elevation= 2324
 Right Levee Station= 420.77 Elevation= 2329.64

CROSS SECTION OUTPUT Profile #PF 1

 * E.G. Elev (ft) * 2321.37 * Element * Left OB * Channel * Right OB *
 * Vel Head (ft) * 0.38 * Wt. n-Val. * 210.00 * 0.035 *
 * W.S. Elev (ft) * 2320.99 * Reach Len. (ft) * 200.00 * 200.00 *
 * Crit W.S. (ft) * 2320.99 * Flow Area (sq ft) * 31.60 *
 * E.G. Slope (ft/ft) * 0.019800 * Area (sq ft) * 31.60 *
 * Q Total (cfs) * 157.00 * Flow (cfs) * 157.00 *
 * Top Width (ft) * 41.54 * Top Width (ft) * 41.54 *
 * Vel Total (ft/s) * 4.97 * Avg. Vel. (ft/s) * 4.97 *
 * Max chl Dpth (ft) * 8.89 * Hydr. Depth (ft) * 0.76 *
 * Conv. Total (cfs) * 1115.8 * Conv. (cfs) * 1115.8 *
 * Length Wtd. (ft) * 200.00 * Wetted Per. (ft) * 41.65 *
 * Min Ch El (ft) * 2320.00 * Shear (lb/sq ft) * 0.94 *
 * Alpha * 1.00 * Stream Power (lb/ft s) * 4.66 *
 * Frctn Loss (ft) * 0.44 * Cum Volume (acre-ft) * 4.86 *
 * C & E Loss (ft) * 0.04 * Cum SA (acres) * 4.48 *

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 26

INPUT
 Description: 2+300
 Station Elevation Data num= 26
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev

 -332.09 2322.62 -266.12 2322.02 -239 2320.3 -195.8 2319.85 -171.96 2317.86
 -341.05 2318 -89.33 2319.39 8.82 2319.2 50.01 2318 62.61 2314
 89.81 2314 132.42 2317.69 158.02 2316 168.26 2315.97 200.86 2319.7
 272.99 2316.02 284.41 2313.88 317.24 2313.84 334.2 2320 386.09 2326
 465.37 2326 491.34 2322.53 509.9 2321.9 558.51 2316 606.32 2315.97
 632.67 2312.82

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val

 -332.09 .035 8.82 .035 386.09 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -332.09 386.09 300 300
 Left Levee Station= 200.86 Elevation= 2319.7
 Right Levee Station= 334.2 Elevation= 2320

CROSS SECTION OUTPUT Profile #PF 1

 * E.G. Elev (ft) * 2315.16 * Element * Left OB * Channel * Right OB *
 * Vel Head (ft) * 0.40 * Wt. n-Val. * 300.00 * 0.035 *
 * W.S. Elev (ft) * 2314.76 * Reach Len. (ft) * 300.00 * 330.00 *
 * Crit W.S. (ft) * 2314.76 * Flow Area (sq ft) * 32.71 *
 * E.G. Slope (ft/ft) * 0.018864 * Area (sq ft) * 32.71 *
 * Q Total (cfs) * 166.00 * Flow (cfs) * 166.00 *
 * Top Width (ft) * 40.05 * Top Width (ft) * 40.05 *
 * Vel Total (ft/s) * 5.07 * Avg. Vel. (ft/s) * 5.07 *
 * Max chl Dpth (ft) * 1.94 * Hydr. Depth (ft) * 0.82 *
 * Conv. Total (cfs) * 1208.6 * Conv. (cfs) * 1208.6 *
 * Length Wtd. (ft) * 300.00 * Wetted Per. (ft) * 40.29 *
 * Min Ch El (ft) * 2313.84 * Shear (lb/sq ft) * 0.96 *
 * Alpha * 1.00 * Stream Power (lb/ft s) * 4.85 *
 * Frctn Loss (ft) * 5.66 * Cum Volume (acre-ft) * 4.71 *
 * C & E Loss (ft) * 0.00 * Cum SA (acres) * 4.30 *

Warning: The energy equation could not be balanced within the specified number of iterations. The program selected the water surface that had the least amount of error between computed and assumed values.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 24

INPUT
 Description: 2+500
 Station Elevation Data num= 22
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev

 -695 2315 -645 2317 -555 2318 -500 2315 -466 2316
 -415 2312 -393 2312 -313 2316 -285 2316 -240 2312
 -123 2314 85 2313.5 140 2311 155 2308 185 2308
 207 2312 340 2319 435 2319.5 482 2317.2 538 2308
 658 2309 705 2306

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val

 -695 .035 -555 .035 340 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -555 340 220 220
 Left Levee Station= -555 Elevation= 2318
 Right Levee Station= 340 Elevation= 2319

CROSS SECTION OUTPUT Profile #PF 1

 * E.G. Elev (ft) * 2309.34 * Element * Left OB * Channel * Right OB *
 * Vel Head (ft) * 0.40 * Wt. n-Val. * 300.00 * 0.035 *

```

022606.rep
* W.S. Elev (ft)      * 2308.93 * Reach Len. (ft)    * 220.00 * 220.00 * 270.00 *
* Crit W.S. (ft)      * 2308.93 * Flow Area (sq ft)  *         * 32.60 *         *
* E.G. Slope (ft/ft)  * 0.01881 * Area (sq ft)       *         * 32.60 *         *
* Q Total (cfs)        * 166.00 * Flow (cfs)         *         * 166.00 *         *
* Top Width (ft)       * 39.81 * Top Width (ft)      *         * 39.81 *         *
* Vel Total (ft/s)     * 5.09 * Avg. Vel. (ft/s)    *         * 5.09 *         *
* Max Chl Dpth (ft)    * 2.93 * Hydr. Depth (ft)    *         * 0.82 *         *
* Conv. Total (cfs)    * 1208.1 * Conv. (cfs)         *         * 1208.1 *         *
* Length Wtd. (ft)     * 220.00 * Wetted Per. (ft)    *         * 39.98 *         *
* Min Ch El (ft)       * 2308.00 * Shear (lb/sq ft)    *         * 0.96 *         *
* Alpha                * 1.00 * Stream Power (lb/ft s) *         * 4.89 *         *
* Frctn Loss (ft)      * 3.34 * Cum Volume (acre-ft) *         * 4.49 *         *
* C & E Loss (ft)      * 0.01 * Cum SA (acres)      *         * 4.02 *         *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 22

INPUT

Description: 2+700

Station Elevation Data		num=	25						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-690	2308	-660	2312	-575	2312	-500	2314	-375	2309
-305	2304	-287	2304	-210	2307.5	55	2307.5	65	2304
85	2303	125	2305	152	2307.5	195	2308	237	2313
280	2313	320	2310	358	2309	460	2310.5	530	2310
570	2302.5	585	2298	600	2298	620	2300	640	2300

Manning's n Values		num=	3
Sta	n Val	Sta	n Val
-690	.035	-375	.035
195		195	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
-375	195	230	240	240		.1	.3	
Left Levee	Station=	55	Elevation=	2307.5				
Right Levee	Station=	152	Elevation=	2307.5				

CROSS SECTION OUTPUT Profile #PF 1

```

* E.G. Elev (ft)      * 2304.69 * Element            * Left OB * Channel * Right OB *
* Vel Head (ft)       * 0.35 * Wt. n-Val.         *         * 0.035 *         *
* W.S. Elev (ft)       * 2304.34 * Reach Len. (ft)    * 230.00 * 240.00 * 240.00 *
* Crit W.S. (ft)       * 2304.34 * Flow Area (sq ft)  *         * 34.73 *         *
* E.G. Slope (ft/ft)  * 0.019407 * Area (sq ft)       *         * 34.73 *         *
* Q Total (cfs)        * 166.00 * Flow (cfs)         *         * 166.00 *         *
* Top Width (ft)       * 47.68 * Top Width (ft)      *         * 47.68 *         *
* Vel Total (ft/s)     * 4.78 * Avg. Vel. (ft/s)    *         * 4.78 *         *
* Max Chl Dpth (ft)    * 6.34 * Hydr. Depth (ft)    *         * 0.73 *         *
* Conv. Total (cfs)    * 1191.6 * Conv. (cfs)         *         * 1191.6 *         *
* Length Wtd. (ft)     * 240.00 * Wetted Per. (ft)    *         * 47.79 *         *
* Min Ch El (ft)       * 2303.00 * Shear (lb/sq ft)    *         * 0.88 *         *
* Alpha                * 1.00 * Stream Power (lb/ft s) *         * 4.21 *         *
* Frctn Loss (ft)      * 1.52 * Cum Volume (acre-ft) *         * 4.32 *         *
* C & E Loss (ft)      * 0.02 * Cum SA (acres)      *         * 3.80 *         *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 20

INPUT

Description: 2+900

Station Elevation Data		num=	25						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-620	2308	-580	2308	-520	2306	-470	2305.75	-450	2307
-360	2306	-220	2300	-210	2298	-195	2298	-180	2300
-165	2300	-150	2298	-130	2303	-60	2302.8	-25	2299.8
-15	2299.8	-10	2298	20	2298	50	2300	120	2302
180	2310	260	2310.8	480	2298.5	510	2298	580	2300

Manning's n Values		num=	3
Sta	n Val	Sta	n Val
-620	.035	-450	.035
180		180	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
-450	180	200	200	200		.1	.3	
Left Levee	Station=	-360	Elevation=	2306				
Right Levee	Station=	180	Elevation=	2310				

CROSS SECTION OUTPUT Profile #PF 1

```

* E.G. Elev (ft)      * 2298.94 * Element            * Left OB * Channel * Right OB *
* Vel Head (ft)       * 0.27 * Wt. n-Val.         *         * 0.035 *         *
* W.S. Elev (ft)       * 2298.67 * Reach Len. (ft)    * 200.00 * 200.00 * 200.00 *
* Crit W.S. (ft)       * 2298.67 * Flow Area (sq ft)  *         * 39.63 *         *
* E.G. Slope (ft/ft)  * 0.022156 * Area (sq ft)       *         * 39.63 *         *
* Q Total (cfs)        * 166.00 * Flow (cfs)         *         * 166.00 *         *
* Top Width (ft)       * 73.05 * Top Width (ft)      *         * 73.05 *         *
* Vel Total (ft/s)     * 4.19 * Avg. Vel. (ft/s)    *         * 4.19 *         *
* Max Chl Dpth (ft)    * 0.67 * Hydr. Depth (ft)    *         * 0.54 *         *
* Conv. Total (cfs)    * 1115.2 * Conv. (cfs)         *         * 1115.2 *         *
* Length Wtd. (ft)     * 200.00 * Wetted Per. (ft)    *         * 73.43 *         *
* Min Ch El (ft)       * 2298.00 * Shear (lb/sq ft)    *         * 0.75 *         *
* Alpha                * 1.00 * Stream Power (lb/ft s) *         * 3.13 *         *
* Frctn Loss (ft)      * 4.65 * Cum Volume (acre-ft) *         * 4.11 *         *
* C & E Loss (ft)      * 0.02 * Cum SA (acres)      *         * 3.47 *         *

```

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m), between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 19

INPUT

Description: 3+000

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
52.74	2299.74	81.63	2298.73	100.84	2296	152.59	2295.81	199	2294
210.08	2292	247.52	2292	252.8	2291.63	258.56	2292	349.01	2292
362.72	2294	420.28	2295.25						

Sta	n Val	Sta	n Val
52.74	.035	199	.035
362.72	.035		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	199	362.72		100	100		.1	.3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2292.59	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.20	* Wt. n-Val.	* 100.00	* 0.035	* 100.00
* W.S. Elev (ft)	* 2292.39	* Reach Len. (ft)			
* Crit W.S. (ft)	* 2292.39	* Flow Area (sq ft)		* 57.15	
* E.G. Slope (ft/ft)	* 0.024201	* Area (sq ft)		* 57.15	
* Q Total (cfs)	* 204.00	* Flow (cfs)		* 204.00	
* Top width (ft)	* 143.76	* Top width (ft)		* 143.76	
* Vel Total (ft/s)	* 3.57	* Avg. Vel. (ft/s)		* 3.57	
* Max Chl Dpth (ft)	* 0.76	* Hydr. Depth (ft)		* 0.40	
* Conv. Total (cfs)	* 1311.3	* Conv. (cfs)		* 1311.3	
* Length Wtd. (ft)	* 100.00	* Wetted Per. (ft)		* 143.85	
* Min Ch El (ft)	* 2291.63	* Shear (lb/sq ft)		* 0.60	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 2.14	
* Frctn Loss (ft)	* 2.07	* Cum Volume (acre-ft)		* 3.89	
* C & E Loss (ft)	* 0.03	* Cum SA (acres)		* 2.97	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m), between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 18

INPUT

Description: 3+100

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
41.32	2296	62.28	2296	80.22	2293.9	112.9	2292.5	168.47	2292
214.86	2286	227.03	2286	237.92	2288	303.24	2290	322.54	2290
347.5	2291	369.05	2290.98	404.01	2290	432.4	2290		

Sta	n Val	Sta	n Val
41.32	.035	168.47	.035
347.5	.035		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	168.47	347.5		165	165		.1	.3

Cross Section Lid

Sta	Hi	Cord	Lo	Cord	Sta	Hi	Cord	Lo	Cord
232.61	2291	2290	236.61	2291	2290				

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2288.09	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.53 <td>* Wt. n-Val.</td> <td>* 165.00</td> <td>* 0.035</td> <td>* 165.00</td>	* Wt. n-Val.	* 165.00	* 0.035	* 165.00
* W.S. Elev (ft)	* 2287.56 <td>* Reach Len. (ft)</td> <td></td> <td></td> <td></td>	* Reach Len. (ft)			
* Crit W.S. (ft)	* 2287.56 <td>* Flow Area (sq ft)</td> <td></td> <td>* 34.96</td> <td></td>	* Flow Area (sq ft)		* 34.96	
* E.G. Slope (ft/ft)	* 0.017836 <td>* Area (sq ft)</td> <td></td> <td>* 34.96</td> <td></td>	* Area (sq ft)		* 34.96	
* Q Total (cfs)	* 204.00 <td>* Flow (cfs)</td> <td></td> <td>* 204.00</td> <td></td>	* Flow (cfs)		* 204.00	
* Top width (ft)	* 32.70 <td>* Top width (ft)</td> <td></td> <td>* 32.70</td> <td></td>	* Top width (ft)		* 32.70	
* Vel Total (ft/s)	* 5.84 <td>* Avg. Vel. (ft/s)</td> <td></td> <td>* 5.84</td> <td></td>	* Avg. Vel. (ft/s)		* 5.84	
* Max Chl Dpth (ft)	* 0.53 <td>* Hydr. Depth (ft)</td> <td></td> <td>* 1.07</td> <td></td>	* Hydr. Depth (ft)		* 1.07	
* Conv. Total (cfs)	* 1527.5	* Conv. (cfs)		* 1527.5	
* Length Wtd. (ft)	* 165.00 <td>* Wetted Per. (ft)</td> <td></td> <td>* 33.47</td> <td></td>	* Wetted Per. (ft)		* 33.47	
* Min Ch El (ft)	* 2287.03 <td>* Shear (lb/sq ft)</td> <td></td> <td>* 1.16</td> <td></td>	* Shear (lb/sq ft)		* 1.16	
* Alpha	* 1.00 <td>* Stream Power (lb/ft s)</td> <td></td> <td>* 6.79</td> <td></td>	* Stream Power (lb/ft s)		* 6.79	
* Frctn Loss (ft)	*	* Cum Volume (acre-ft)		* 3.79	
* C & E Loss (ft)	*	* Cum SA (acres)		* 2.77	

Warning: During subcritical analysis, the water surface upstream of culvert went to critical depth.

CULVERT

RIVER: FIS Flood Zone
 REACH: Mission RS: 17

INPUT

Distance From Upstream XS = 100
 Deck/Roadway Width = 4
 Weir Coefficient = 2.6
 Upstream Deck/Roadway Coordinates

Sta	Hi	Cord	Lo	Cord	Sta	Hi	Cord	Lo	Cord
221.03	2291	2290	225.03	2291	2290				

Upstream Bridge Cross Section Data

Sta	Elev	Sta	Elev	Sta	Elev
221.03	2291	2290	225.03	2291	2290

022606.rep
41.32 2296 62.28 2296 80.22 2293.9 112.9 2292.5 168.47 2292
214.86 2286 227.03 2286 237.92 2288 303.24 2290 322.54 2290
347.5 2291 369.05 2290.98 404.01 2290 432.4 2290

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val

41.32 .035 168.47 .035 347.5 .035

Bank Sta: Left Right Coeff Contr. Expan.
168.47 347.5 .1 .3

Downstream Deck/Roadway Coordinates
num= 2
Sta Hi Cord Lo Cord Sta Hi Cord Lo Cord

260.31 2289.6 2288.6 264.31 2289.6 2288.6

Downstream Bridge Cross Section Data
Station Elevation Data num= 15
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev

48.08 2294 58.34 2294 98.13 2292 111.08 2290 200.49 2286
206.56 2286 249.41 2284.03 258.31 2282 260.61 2282 278.52 2286
301 2285.51 321.73 2285.46 350.14 2284.8 369.37 2286 413.53 2286.45

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val

48.08 .035 200.49 .035 413.53 .035

Bank Sta: Left Right Coeff Contr. Expan.
200.49 413.53 .1 .3

Upstream Embankment side slope = 0 horiz. to 1.0 vertical
Downstream Embankment side slope = 0 horiz. to 1.0 vertical
Maximum allowable submergence for weir flow = .95
Elevation at which weir flow begins =
Energy head used in spillway design =
Spillway height used in design =
Weir crest shape = Broad Crested

Number of Culverts = 1

Culvert Name Shape Rise Span
Culvert #1 Box 7 4
FHWA Chart # 8 - flared wingwalls
FHWA scale # 1 - Wingwall flared 30 to 75 deg.
Solution Criteria = Highest U.S. E
Culvert Upstrm Dist Length Top n Bottom n Depth Blocked Entrance Loss Coef Exit Loss Coef
35 100 .014 .014 0 .05 1
Upstream Elevation = 2283
Centerline Station = 223.03
Downstream Elevation = 2281.6
Centerline Station = 262.31

CULVERT OUTPUT Profile #PF 1 Culv Group: Culvert #1

* Q Culv Group (cfs) * 115.47 * Culv Full Len (ft) *
* # Barrels (cfs) * 1 * Culv Vel US (ft/s) * 9.76 *
* Q Barrel (cfs) * 115.47 * Culv Vel DS (ft/s) * 12.51 *
* E.G. US. (ft) * 2287.67 * Culv Inv El Up (ft) * 2283.00 *
* W.S. US. (ft) * 2287.56 * Culv Inv El Dn (ft) * 2281.60 *
* E.G. DS (ft) * 2285.04 * Culv Frctn Ls (ft) * 1.10 *
* W.S. DS (ft) * 2284.64 * Culv Exit Loss (ft) * 1.30 *
* Delta EG (ft) * 2.63 * Culv Entr Loss (ft) * 0.23 *
* Delta WS (ft) * 2.92 * Q Weir (cfs) * 88.53 *
* E.G. IC (ft) * 2287.67 * Weir Sta Lft (ft) * 202.02 *
* E.G. OC (ft) * 2287.51 * Weir Sta Rgt (ft) * 236.07 *
* Culvert Control * Inlet * Weir Submerg * 0.00 *
* Culv WS Inlet (ft) * 2285.96 * Weir Max Depth (ft) * 1.66 *
* Culv WS Outlet (ft) * 2283.91 * Weir Avg Depth (ft) * 1.06 *
* Culv Nml Depth (ft) * 2.22 * Weir Flow Area (sq ft) * 31.74 *
* Culv CRT Depth (ft) * 2.96 * Min El Weir Flow (ft) * 2286.01 *

Warning: During subcritical analysis, the water surface upstream of culvert went to critical depth.
Note: The flow in the culvert is entirely supercritical.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 16

INPUT
Description: 3+300
Station Elevation Data num= 15
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev

48.08 2294 58.34 2294 98.13 2292 111.08 2290 200.49 2286
206.56 2286 249.41 2284.03 258.31 2282 260.61 2282 278.52 2286
301 2285.51 321.73 2285.46 350.14 2284.8 369.37 2286 413.53 2286.45

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val

48.08 .035 200.49 .035 413.53 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
200.49 413.53 100 100 .1 .3

Cross Section Lid
num= 2
Sta Hi Cord Lo Cord Sta Hi Cord Lo Cord

232.61 2289.6 2288.6 236.61 2289.6 2288.6

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft) * 2285.04 * Element * Left 08 * Channel * Right 08 *
* Vel Head (ft) * 0.40 * W.C. n-Val. * 0.035 *
* W.S. Elev (ft) * 2284.64 * Reach Len. (ft) * 100.00 * 100.00 * 110.00 *
* Crit W.S. (ft) * 2284.64 * Flow Area (sq ft) * 40.18 *
* E.G. Slope (ft/ft) * 0.012747 * Area (sq ft) * 40.18 *
* Q Total (cfs) * 204.00 * Flow (cfs) * 204.00 *
* Top width (ft) * 36.29 * Top width (ft) * 36.29 *
* Vel Total (ft/s) * 5.08 * Avg. Vel. (ft/s) * 5.08 *
* Max Chl Dpth (ft) * 0.02 * Hydr. Depth (ft) * 1.11 *
* Conv. Total (cfs) * 1806.9 * Conv. (cfs) * 1806.9 *
* Length Wtd. (ft) * 100.00 * Wetted Per. (ft) * 36.85 *
* Min Ch El (ft) * 2284.62 * Shear (lb/sq ft) * 0.87 *
* Alpha * 1.00 * Stream Power (lb/ft s) * 4.41 *
* Frctn Loss (ft) * 1.61 * Cum Volume (acre-ft) * 3.64 *
* C & E Loss (ft) * 0.03 * Cum SA (acres) * 2.64 *

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross

section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 15

INPUT

Description: 3+400

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
17.71	2286.97	26.99	2286.94	54.39	2282	65.42	2282	85.7	2284
108.83	2284	132.46	2281.98	167.75	2280	178.3	2280	192.04	2280.74
214.38	2280.54	219.45	2280.29	230.34	2282	251.22	2282	260.86	2284
278.16	2286	332.59	2286						

Sta	n Val	Sta	n Val	Sta	n Val
17.71	.035	108.83	.035	278.16	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
108.83	278.16	60	60	2284	.1	.3	
Left Levee	Station=	108.83	Elevation=	2284			

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2281.38	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.30	* Wt. n-Val.	* 60.00	* 0.035	* 60.00
* W.S. Elev (ft)	* 2281.07	* Reach Len. (ft)	* 60.00	* 46.27	* 46.27
* Crit W.S. (ft)	* 2281.07	* Flow Area (sq ft)	* 46.27	* 46.27	* 46.27
* E.G. Slope (ft/ft)	* 0.020877	* Area (sq ft)	* 204.00	* 204.00	* 204.00
* Q Total (cfs)	* 204.00	* Flow (cfs)	* 75.83	* 75.83	* 75.83
* Top Width (ft)	* 75.83	* Top Width (ft)	* 4.41	* 4.41	* 4.41
* Vel Total (ft/s)	* 4.41	* Avg. Vel. (ft/s)	* 0.61	* 0.61	* 0.61
* Max Chl Dpth (ft)	* 1.07	* Hydr. Depth (ft)	* 1411.9	* 1411.9	* 1411.9
* Conv. Total (cfs)	* 1411.9	* Conv. (cfs)	* 75.95	* 75.95	* 75.95
* Length Wtd. (ft)	* 60.00	* Wetted Per. (ft)	* 0.79	* 0.79	* 0.79
* Min Ch El (ft)	* 2280.00	* Shear (lb/sq ft)	* 3.50	* 3.50	* 3.50
* Alpha	* 1.00	* Stream Power (lb/ft s)	* 3.55	* 3.55	* 3.55
* Frctn Loss (ft)	* 1.16	* Cum Volume (acre-ft)	* 2.51	* 2.51	* 2.51
* C & E Loss (ft)	* 0.02	* Cum SA (acres)			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 14

INPUT

Description: 3+500

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
28.41	2280	52.78	2282	95.32	2282	128.99	2280	163.46	2280
169.48	2279.49	204.01	2278	221.5	2276	237.94	2276	263.15	2282
300.4	2284	325.65	2284.53						

Sta	n Val	Sta	n Val	Sta	n Val
28.41	.035	95.32	.035	263.15	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
95.32	263.15	240	240	2282	.1	.3	
Left Levee	Station=	95.32	Elevation=	2282			

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2277.91	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.52	* Wt. n-Val.	* 240.00	* 0.035	* 390.00
* W.S. Elev (ft)	* 2277.39	* Reach Len. (ft)	* 240.00	* 35.35	* 35.35
* Crit W.S. (ft)	* 2277.39	* Flow Area (sq ft)	* 35.35	* 35.35	* 35.35
* E.G. Slope (ft/ft)	* 0.018013	* Area (sq ft)	* 204.00	* 204.00	* 204.00
* Q Total (cfs)	* 204.00	* Flow (cfs)	* 34.43	* 34.43	* 34.43
* Top Width (ft)	* 34.43	* Top Width (ft)	* 5.77	* 5.77	* 5.77
* Vel Total (ft/s)	* 5.77	* Avg. Vel. (ft/s)	* 1.03	* 1.03	* 1.03
* Max Chl Dpth (ft)	* 1.39	* Hydr. Depth (ft)	* 1520.0	* 1520.0	* 1520.0
* Conv. Total (cfs)	* 1520.0	* Conv. (cfs)	* 34.67	* 34.67	* 34.67
* Length Wtd. (ft)	* 260.00	* Wetted Per. (ft)	* 1.15	* 1.15	* 1.15
* Min Ch El (ft)	* 2276.00	* Shear (lb/sq ft)	* 6.62	* 6.62	* 6.62
* Alpha	* 1.00	* Stream Power (lb/ft s)	* 3.49	* 3.49	* 3.49
* Frctn Loss (ft)	* 1.93	* Cum Volume (acre-ft)	* 2.43	* 2.43	* 2.43
* C & E Loss (ft)	* 0.08	* Cum SA (acres)			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 12

INPUT

Description: 3+700

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-300	2280	-280	2282	-170	2282	-65	2278	-47	2275
30	2266	40	2266.5	75	2268	100	2275	150	2270
160	2270	200	2280	220	2280	255	2282	370	2286
500	2286	530	2294						

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val

 -300 .035 -65 .035 200 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -65 200 140 90 120 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2268.22	* Element	* Left OB	* Channel	* Right OB	*
* Vel Head (ft)	* 0.25	* Wt. n-Val.	* 0.035			*
* W.S. Elev (ft)	* 2267.97	* Reach Len. (ft)	* 140.00	* 90.00	* 120.00	*
* Crit W.S. (ft)		* Flow Area (sq ft)		* 149.25		*
* E.G. Slope (ft/ft)	* 0.005903	* Area (sq ft)		* 149.25		*
* Q Total (cfs)	* 602.00	* Flow (cfs)		* 602.00		*
* Top Width (ft)	* 108.01	* Top Width (ft)		* 108.01		*
* Vel Total (ft/s)	* 4.03	* Avg. Vel. (ft/s)		* 4.03		*
* Max Chl Dpth (ft)	* 1.97	* Hydr. Depth (ft)		* 1.38		*
* Conv. Total (cfs)	* 7835.2	* Conv. (cfs)		* 7835.2		*
* Length Wtd. (ft)	* 90.00	* Wetted Per. (ft)		* 108.54		*
* Min Ch El (ft)	* 2266.00	* Shear (lb/sq ft)		* 0.51		*
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 2.04		*
* Frctn Loss (ft)	* 0.85	* Cum Volume (acre-ft)		* 2.94		*
* C & E Loss (ft)	* 0.03	* Cum SA (acres)		* 2.01		*

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 10

INPUT
 Description: 3+900
 Station Elevation Data num= 14
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev

 -370 2273.5 -300 2282 -185 2282 -110 2276 -45 2276
 -30 2274 -10 2265.5 70 2266.5 90 2266.5 120 2280
 180 2282 240 2283 345 2286 490 2286

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val

 -370 .035 -185 .035 120 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -185 120 110 120 125 .1 .3
 Left Levee Station= -185 Elevation= 2282
 Right Levee Station= 120 Elevation= 2280

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2267.35	* Element	* Left OB	* Channel	* Right OB	*
* Vel Head (ft)	* 0.50	* Wt. n-Val.	* 0.035			*
* W.S. Elev (ft)	* 2266.85	* Reach Len. (ft)	* 110.00	* 120.00	* 125.00	*
* Crit W.S. (ft)	* 2266.85	* Flow Area (sq ft)		* 105.57		*
* E.G. Slope (ft/ft)	* 0.017489	* Area (sq ft)		* 105.57		*
* Q Total (cfs)	* 602.00	* Flow (cfs)		* 602.00		*
* Top Width (ft)	* 102.88	* Top Width (ft)		* 102.88		*
* Vel Total (ft/s)	* 5.70	* Avg. Vel. (ft/s)		* 5.70		*
* Max Chl Dpth (ft)	* 1.35	* Hydr. Depth (ft)		* 1.03		*
* Conv. Total (cfs)	* 4552.1	* Conv. (cfs)		* 4552.1		*
* Length Wtd. (ft)	* 120.00	* Wetted Per. (ft)		* 103.14		*
* Min Ch El (ft)	* 2265.50	* Shear (lb/sq ft)		* 1.12		*
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 6.37		*
* Frctn Loss (ft)	* 1.97	* Cum Volume (acre-ft)		* 2.67		*
* C & E Loss (ft)	* 0.01	* Cum SA (acres)		* 1.79		*

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 08

INPUT
 Description: 4+100
 Station Elevation Data num= 11
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev

 -365 2282 -240 2282 -140 2274 -80 2274 -45 2262
 38 2262 58 2264 90 2279 160 2280 300 2286
 305 2286

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val

 -365 .035 -80 .035 90 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 -80 90 200 200 200 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2263.67	* Element	* Left OB	* Channel	* Right OB	*
* Vel Head (ft)	* 0.48	* Wt. n-Val.	* 0.035			*
* W.S. Elev (ft)	* 2263.19	* Reach Len. (ft)	* 200.00	* 200.00	* 200.00	*
* Crit W.S. (ft)	* 2263.14	* Flow Area (sq ft)		* 107.79		*
* E.G. Slope (ft/ft)	* 0.015369	* Area (sq ft)		* 107.79		*
* Q Total (cfs)	* 602.00	* Flow (cfs)		* 602.00		*
* Top Width (ft)	* 98.35	* Top Width (ft)		* 98.35		*
* Vel Total (ft/s)	* 5.58	* Avg. Vel. (ft/s)		* 5.58		*
* Max Chl Dpth (ft)	* 1.19	* Hydr. Depth (ft)		* 1.10		*
* Conv. Total (cfs)	* 4855.9	* Conv. (cfs)		* 4855.9		*
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)		* 98.61		*
* Min Ch El (ft)	* 2262.00	* Shear (lb/sq ft)		* 1.05		*
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 5.86		*
* Frctn Loss (ft)	* 3.34	* Cum Volume (acre-ft)		* 2.38		*
* C & E Loss (ft)	* 0.00	* Cum SA (acres)		* 1.51		*

Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 06

INPUT

Description: 4+300

Station Elevation Data		num= 13		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-345	2284	-280	2282	-155	2270.5	-80	2270	-65	2268
-45	2258	-30	2258	60	2260	90	2278	100	2280
120	2280	240	2284	260	2285				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-345	.035	-80	.035	90	.035

Bank Sta: Left -80 Right 90 Lengths: Left Channel 200 Right 200 Coeff Contr. .1 Expan. .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)		* Element		* Left OB		* Channel		* Right OB	
* Vel Head (ft)	* 0.53	* Wt. n-Val.	* 0.035	* 200.00	* 200.00	* 200.00	* 200.00		
* W.S. Elev (ft)	* 2259.80	* Reach Len. (ft)							
* Crit W.S. (ft)	* 2259.80	* Flow Area (sq ft)							
* E.G. Slope (ft/ft)	* 0.018215	* Area (sq ft)							
* Q Total (cfs)	* 602.00	* Flow (cfs)							
* Top Width (ft)	* 99.53	* Top Width (ft)							
* Vel Total (ft/s)	* 5.84	* Avg. Vel. (ft/s)							
* Max Chl Dpth (ft)	* 1.80	* Hydr. Depth (ft)							
* Conv. Total (cfs)	* 4460.5	* Conv. (cfs)							
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)							
* Min Ch El (ft)	* 2258.00	* Shear (lb/sq ft)							
* Alpha	* 1.00	* Stream Power (lb/ft s)							
* Frctn Loss (ft)	* 0.80	* Cum Volume (acre-ft)							
* C & E Loss (ft)	* 0.13	* Cum SA (acres)							

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 04

INPUT

Description: 4+500

Station Elevation Data		num= 17		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-475	2282	-340	2282	-335	2279	-160	2264	-75	2264
50	2254	30	2254	60	2256	80	2266.5	100	2267.5
120	2267	130	2268	160	2268	250	2274	280	2274.5
330	2274	520	2280						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-475	.035	-75	.035	80	.035

Bank Sta: Left -75 Right 80 Lengths: Left Channel 200 Right 200 Coeff Contr. .1 Expan. .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)		* Element		* Left OB		* Channel		* Right OB	
* Vel Head (ft)	* 0.11	* Wt. n-Val.	* 0.035	* 200.00	* 200.00	* 200.00	* 200.00		
* W.S. Elev (ft)	* 2256.24	* Reach Len. (ft)							
* Crit W.S. (ft)	* 2256.24	* Flow Area (sq ft)							
* E.G. Slope (ft/ft)	* 0.001717	* Area (sq ft)							
* Q Total (cfs)	* 602.00	* Flow (cfs)							
* Top Width (ft)	* 116.05	* Top Width (ft)							
* Vel Total (ft/s)	* 2.71	* Avg. Vel. (ft/s)							
* Max Chl Dpth (ft)	* 2.24	* Hydr. Depth (ft)							
* Conv. Total (cfs)	* 14529.2	* Conv. (cfs)							
* Length Wtd. (ft)	* 200.00	* Wetted Per. (ft)							
* Min Ch El (ft)	* 2254.00	* Shear (lb/sq ft)							
* Alpha	* 1.00	* Stream Power (lb/ft s)							
* Frctn Loss (ft)	* 0.30	* Cum Volume (acre-ft)							
* C & E Loss (ft)	* 0.00	* Cum SA (acres)							

CROSS SECTION

RIVER: FIS Flood Zone
 REACH: Mission RS: 02

INPUT

Description: 4+700

Station Elevation Data		num= 19		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-430	2262.5	-400	2256	-360	2256.5	-320	2258	-280	2258
-220	2260.5	-200	2260	-110	2260	-100	2260.5	-60	2260
-38	2253	30	2253.5	60	2256	88	2270	130	2272
180	2268	250	2271	260	2274	360	2276		

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-430	.035	-100	.035	88	.035

Bank Sta: Left -100 Right 88 Lengths: Left Channel 29 Right 29 Coeff Contr. .1 Expan. .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)		* Element		* Left OB		* Channel		* Right OB	
* Vel Head (ft)	* 0.10	* Wt. n-Val.	* 0.035	* 29.00	* 29.00	* 29.00	* 29.00		
* W.S. Elev (ft)	* 2255.94	* Reach Len. (ft)							
* Crit W.S. (ft)	* 2255.94	* Flow Area (sq ft)							
* E.G. Slope (ft/ft)	* 0.001322	* Area (sq ft)							
* Q Total (cfs)	* 602.00	* Flow (cfs)							
* Top Width (ft)	* 106.57	* Top Width (ft)							

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022606.rep
* Vel Total (ft/s)      * 2.59 * Avg. Vel. (ft/s)      *      * 2.59 *
* Max Chl Dpth (ft)    * 2.94 * Hydr. Depth (ft)     *      * 2.18 *
* Conv. Total (cfs)    * 16558.3 * Conv. (cfs)         *      * 16558.3 *
* Length Wtd. (ft)     * 29.00 * Wetted Per. (ft)     *      * 107.14 *
* Min Ch El (ft)       * 2253.00 * Shear (lb/sq ft)     *      * 0.18 *
* Alpha                * 1.00 * Stream Power (lb/ft s) *      * 0.46 *
* Frctn Loss (ft)      * 0.09 * Cum Volume (acre-ft) *      * 0.11 *
* C & E Loss (ft)      * 0.07 * Cum SA (acres)       *      * 0.05 *

```

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: FIS Flood Zone
REACH: Mission RS: 01

INPUT

Description: 4+729

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-220	2260	-50	2260	-30	2258	-20	2252	-15	2252
0	2255	10	2254.9	15	2252	20	2252	30	2256
60	2258.5	90	2269	130	2270.5	160	2270	195	2268
240	2270								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-220	.035	-30	.035	60	.035

Bank Sta: Left Right Coeff Contr. Expan.
-30 60 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

* E.G. Elev (ft)	* 2255.88	* Element	* Left OB	* Channel	* Right OB
* Vel Head (ft)	* 0.81	* Wt. n-Val.	* 0.035		
* W.S. Elev (ft)	* 2255.07	* Reach Len. (ft)			
* Crit W.S. (ft)	* 2255.07	* Flow Area (sq ft)		* 83.25	
* E.G. Slope (ft/ft)	* 0.016819	* Area (sq ft)		* 83.25	
* Q Total (cfs)	* 602.00	* Flow (cfs)		* 602.00	
* Top Width (ft)	* 52.80	* Top Width (ft)		* 52.80	
* Vel Total (ft/s)	* 7.23	* Avg. Vel. (ft/s)		* 7.23	
* Max Chl Dpth (ft)	* 3.07	* Hydr. Depth (ft)		* 1.58	
* Conv. Total (cfs)	* 4641.9	* Conv. (cfs)		* 4641.9	
* Length Wtd. (ft)		* Wetted Per. (ft)		* 55.32	
* Min Ch El (ft)	* 2252.00	* Shear (lb/sq ft)		* 1.58	
* Alpha	* 1.00	* Stream Power (lb/ft s)		* 11.43	
* Frctn Loss (ft)		* Cum Volume (acre-ft)			
* C & E Loss (ft)		* Cum SA (acres)			

Warning: Slope too steep for slope area to converge during supercritical flow calculations (normal depth is below critical depth). Water surface set to critical depth.

SUMMARY OF MANNING'S N VALUES

River: FIS Flood Zone

* Reach	* River Sta.	* n1	* n2	* n3
*Mission	* 48	* .035*	* .035*	* .035*
*Mission	* 46	* .035*	* .035*	* .035*
*Mission	* 44	* .035*	* .035*	* .035*
*Mission	* 42	* .035*	* .035*	* .035*
*Mission	* 40	* .035*	* .035*	* .035*
*Mission	* 37	* .035*	* .035*	* .035*
*Mission	* 36	* .035*	* .035*	* .035*
*Mission	* 34	* .035*	* .035*	* .035*
*Mission	* 32	* .035*	* .035*	* .035*
*Mission	* 30	* .035*	* .035*	* .035*
*Mission	* 28	* .035*	* .035*	* .035*
*Mission	* 26	* .035*	* .035*	* .035*
*Mission	* 24	* .035*	* .035*	* .035*
*Mission	* 22	* .035*	* .035*	* .035*
*Mission	* 20	* .035*	* .035*	* .035*
*Mission	* 19	* .035*	* .035*	* .035*
*Mission	* 18	* .035*	* .035*	* .035*
*Mission	* 17	* Culvert	*	*
*Mission	* 16	* .035*	* .035*	* .035*
*Mission	* 15	* .035*	* .035*	* .035*
*Mission	* 14	* .035*	* .035*	* .035*
*Mission	* 12	* .035*	* .035*	* .035*
*Mission	* 10	* .035*	* .035*	* .035*
*Mission	* 08	* .035*	* .035*	* .035*
*Mission	* 06	* .035*	* .035*	* .035*
*Mission	* 04	* .035*	* .035*	* .035*
*Mission	* 02	* .035*	* .035*	* .035*
*Mission	* 01	* .035*	* .035*	* .035*

SUMMARY OF REACH LENGTHS

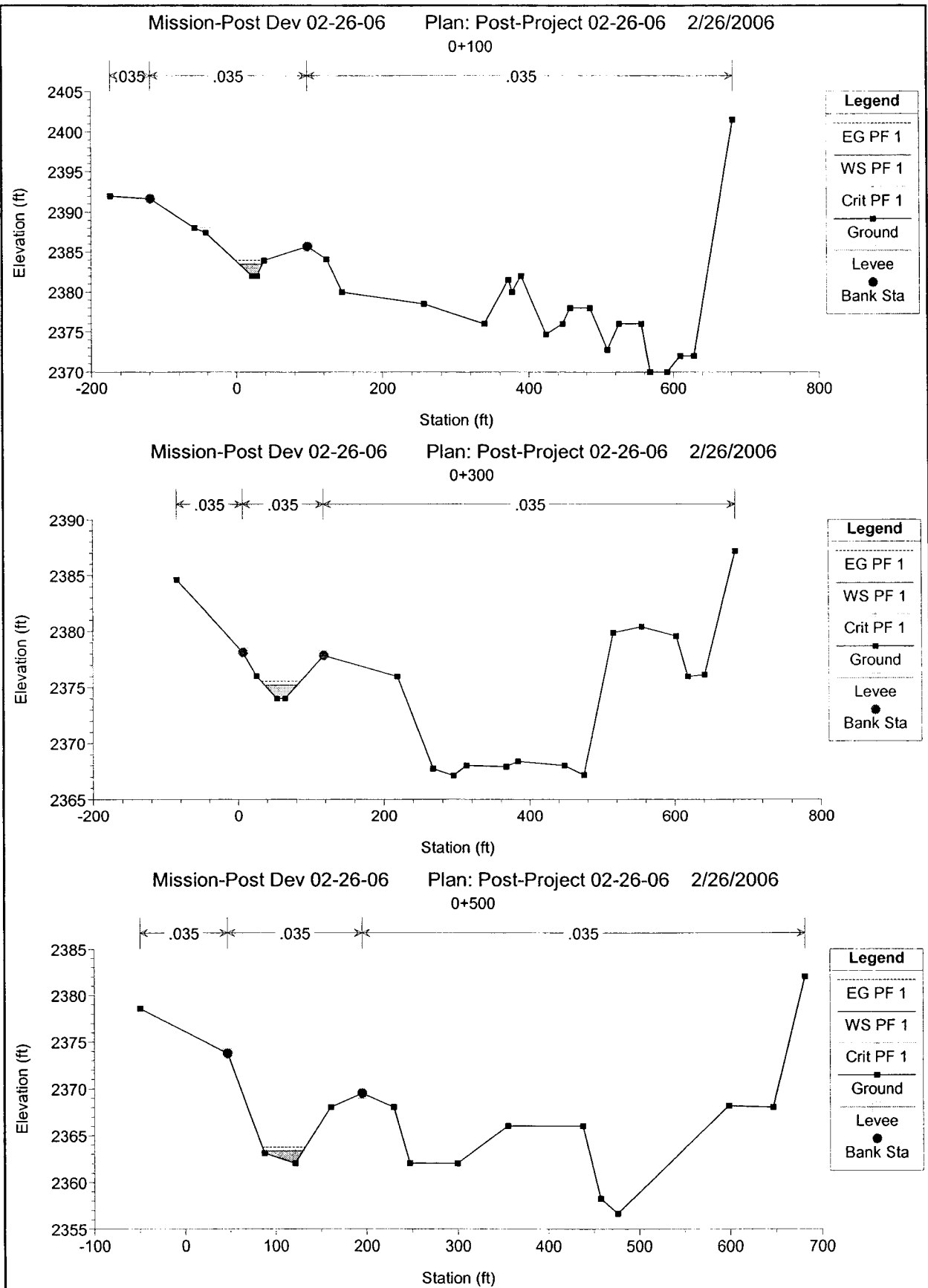
River: FIS Flood Zone

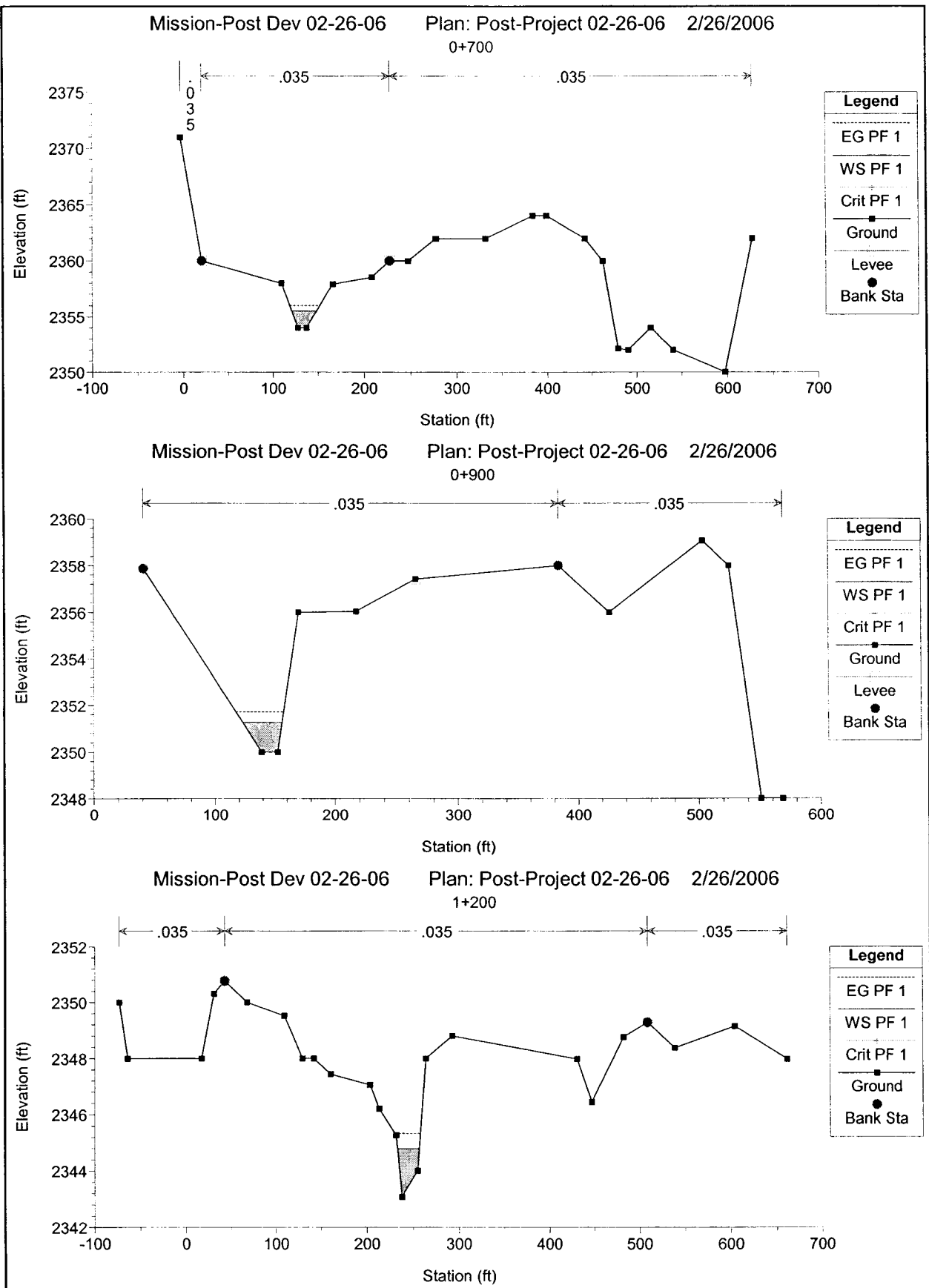
* Reach	* River Sta.	* Left	* Channel	* Right
*Mission	* 48	* 200*	* 200*	* 200*
*Mission	* 46	* 200*	* 200*	* 200*
*Mission	* 44	* 400*	* 210*	* 200*
*Mission	* 42	* 220*	* 220*	* 350*
*Mission	* 40	* 300*	* 300*	* 300*
*Mission	* 37	* 100*	* 100*	* 100*
*Mission	* 36	* 200*	* 200*	* 200*
*Mission	* 34	* 250*	* 200*	* 200*
*Mission	* 32	* 200*	* 200*	* 200*
*Mission	* 30	* 200*	* 200*	* 200*
*Mission	* 28	* 210*	* 200*	* 200*
*Mission	* 26	* 300*	* 300*	* 330*
*Mission	* 24	* 220*	* 220*	* 270*
*Mission	* 22	* 230*	* 240*	* 240*
*Mission	* 20	* 200*	* 200*	* 200*
*Mission	* 19	* 100*	* 100*	* 100*
*Mission	* 18	* 165*	* 165*	* 165*
*Mission	* 17	* Culvert	*	*
*Mission	* 16	* 100*	* 100*	* 110*
*Mission	* 15	* 60*	* 60*	* 60*
*Mission	* 14	* 240*	* 260*	* 390*
*Mission	* 12	* 140*	* 90*	* 120*

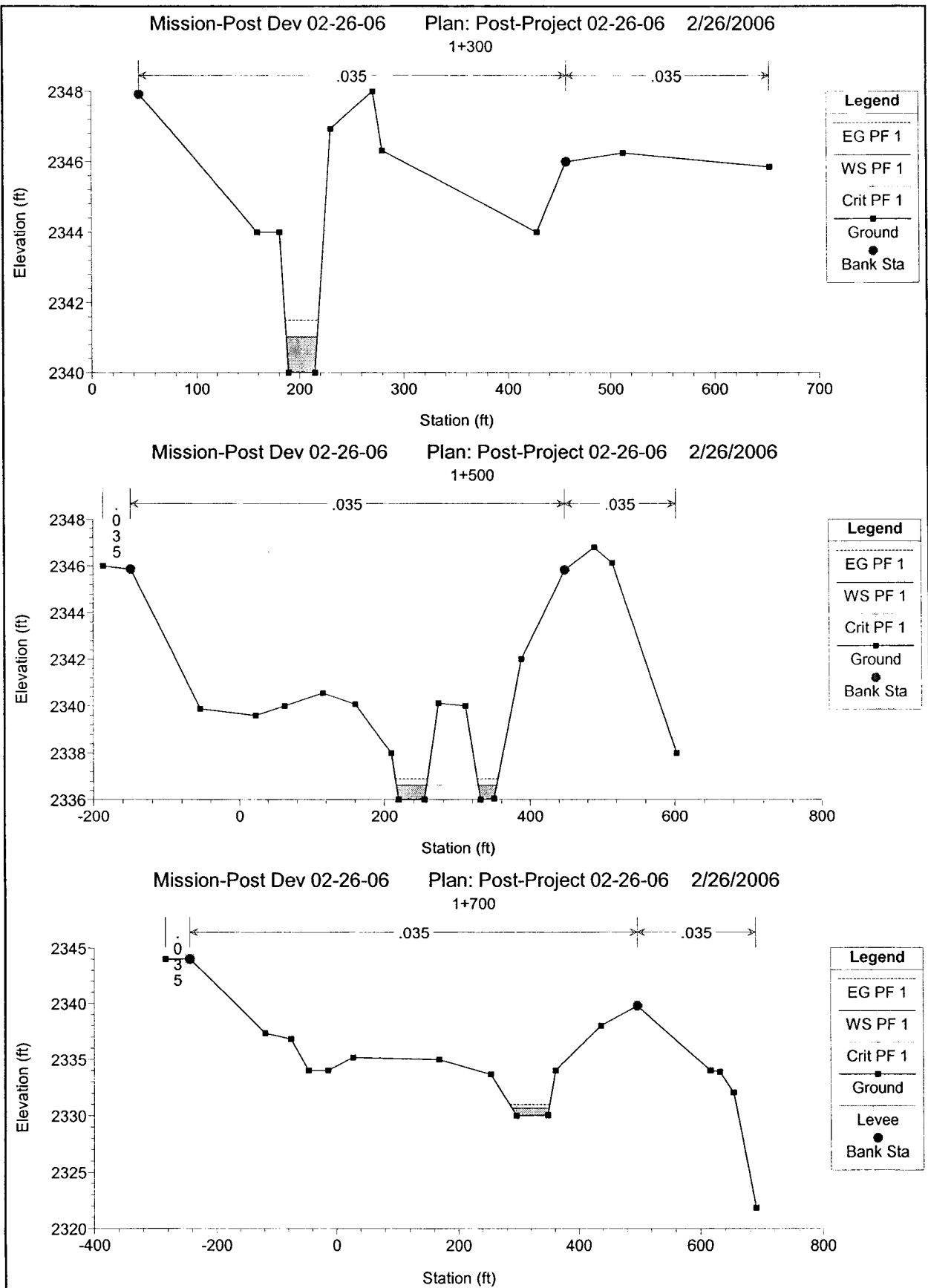
*Mission	*	10	*	110*	120*	125*
*Mission	*	08	*	200*	200*	200*
*Mission	*	06	*	200*	200*	200*
*Mission	*	04	*	200*	200*	200*
*Mission	*	02	*	29*	29*	29*
*Mission	*	01	*	*	*	*

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS River: FIS Flood Zone

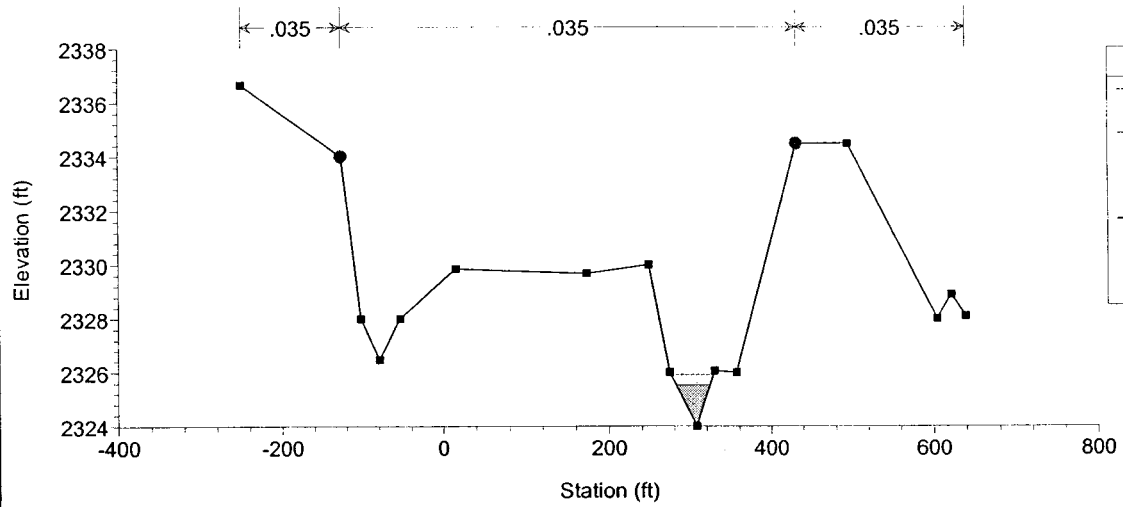
* Reach	* River Sta.	* Contr.	* Expan.
*Mission	* 48	* .1*	* .3*
*Mission	* 46	* .1*	* .3*
*Mission	* 44	* .1*	* .3*
*Mission	* 42	* .1*	* .3*
*Mission	* 40	* .1*	* .3*
*Mission	* 37	* .1*	* .3*
*Mission	* 36	* .1*	* .3*
*Mission	* 34	* .1*	* .3*
*Mission	* 32	* .1*	* .3*
*Mission	* 30	* .1*	* .3*
*Mission	* 28	* .1*	* .3*
*Mission	* 26	* .1*	* .3*
*Mission	* 24	* .1*	* .3*
*Mission	* 22	* .1*	* .3*
*Mission	* 20	* .1*	* .3*
*Mission	* 19	* .1*	* .3*
*Mission	* 18	* .1*	* .3*
*Mission	* 17	* culvert	* *
*Mission	* 16	* .1*	* .3*
*Mission	* 15	* .1*	* .3*
*Mission	* 14	* .1*	* .3*
*Mission	* 12	* .1*	* .3*
*Mission	* 10	* .1*	* .3*
*Mission	* 08	* .1*	* .3*
*Mission	* 06	* .1*	* .3*
*Mission	* 04	* .1*	* .3*
*Mission	* 02	* .1*	* .3*
*Mission	* 01	* .1*	* .3*



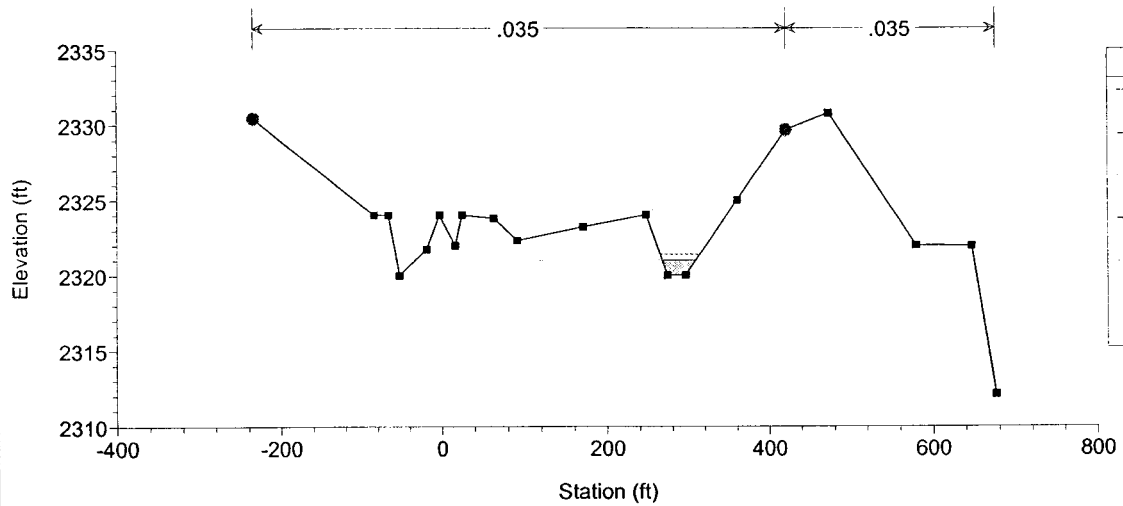




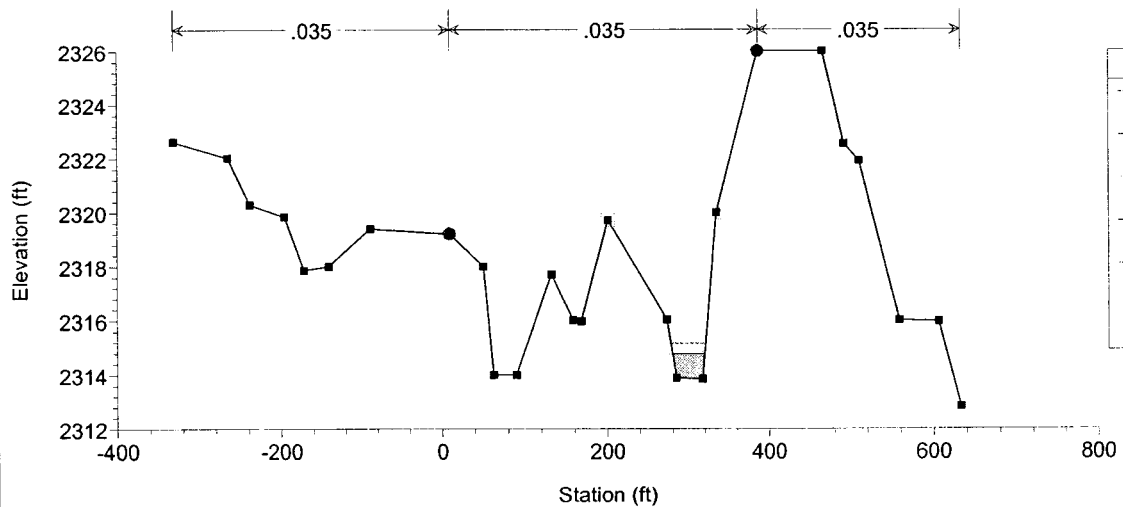
Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006
1+900

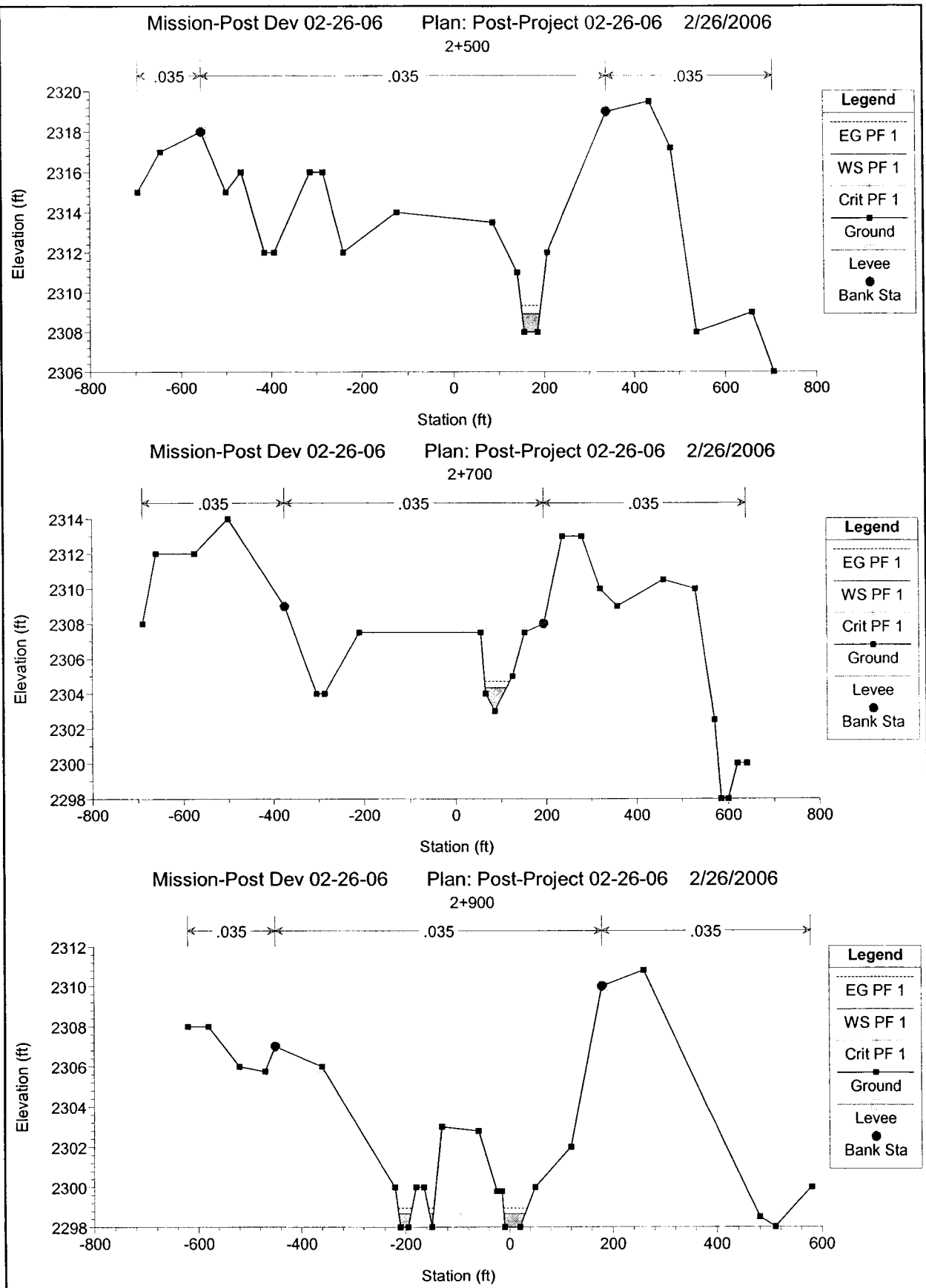


Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006
2+100

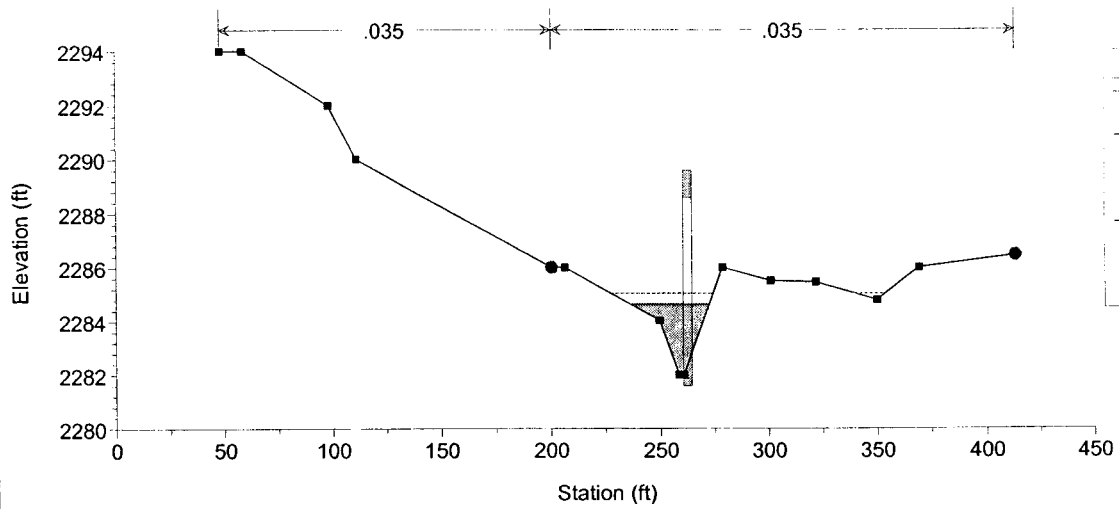


Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006
2+300

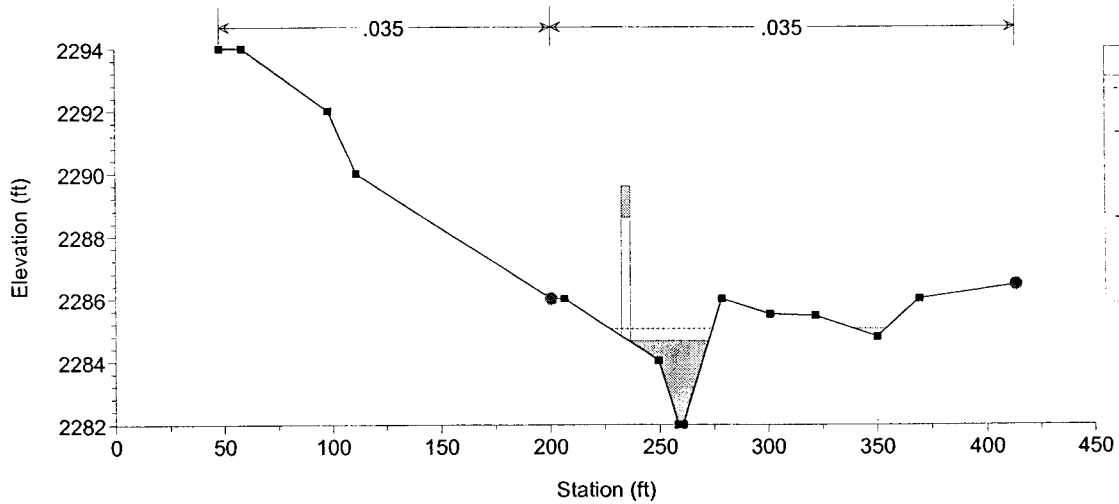




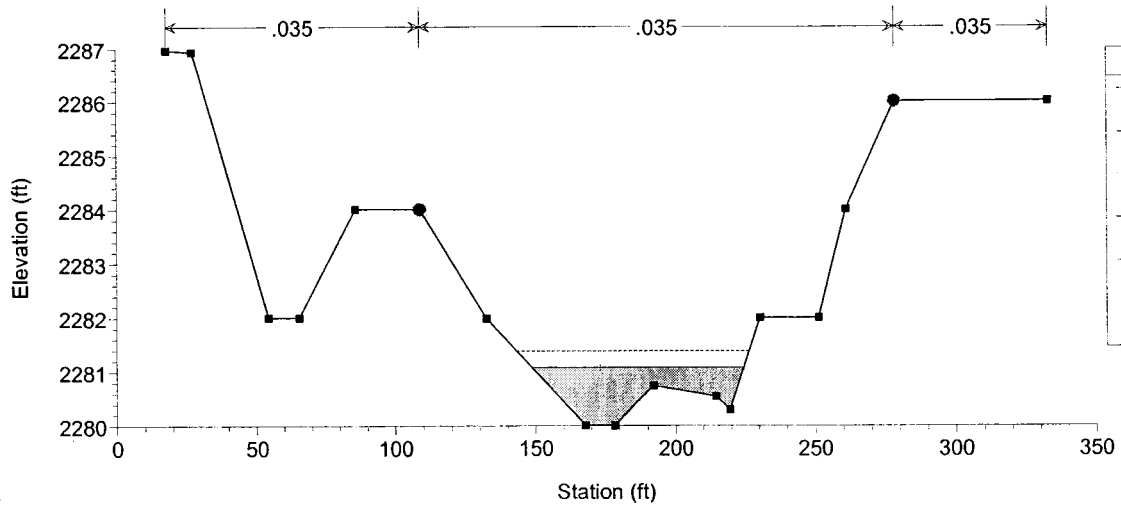
Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006

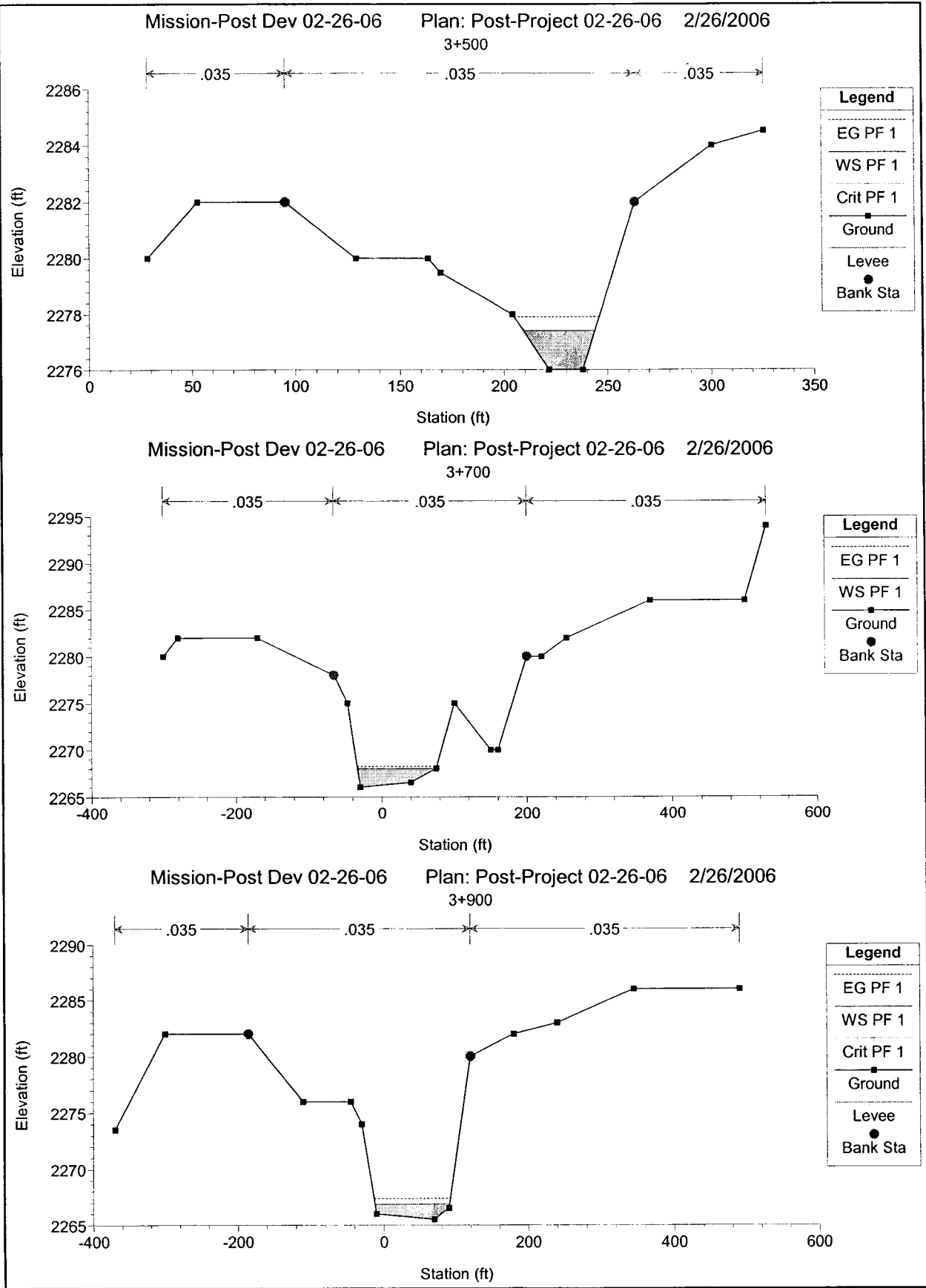


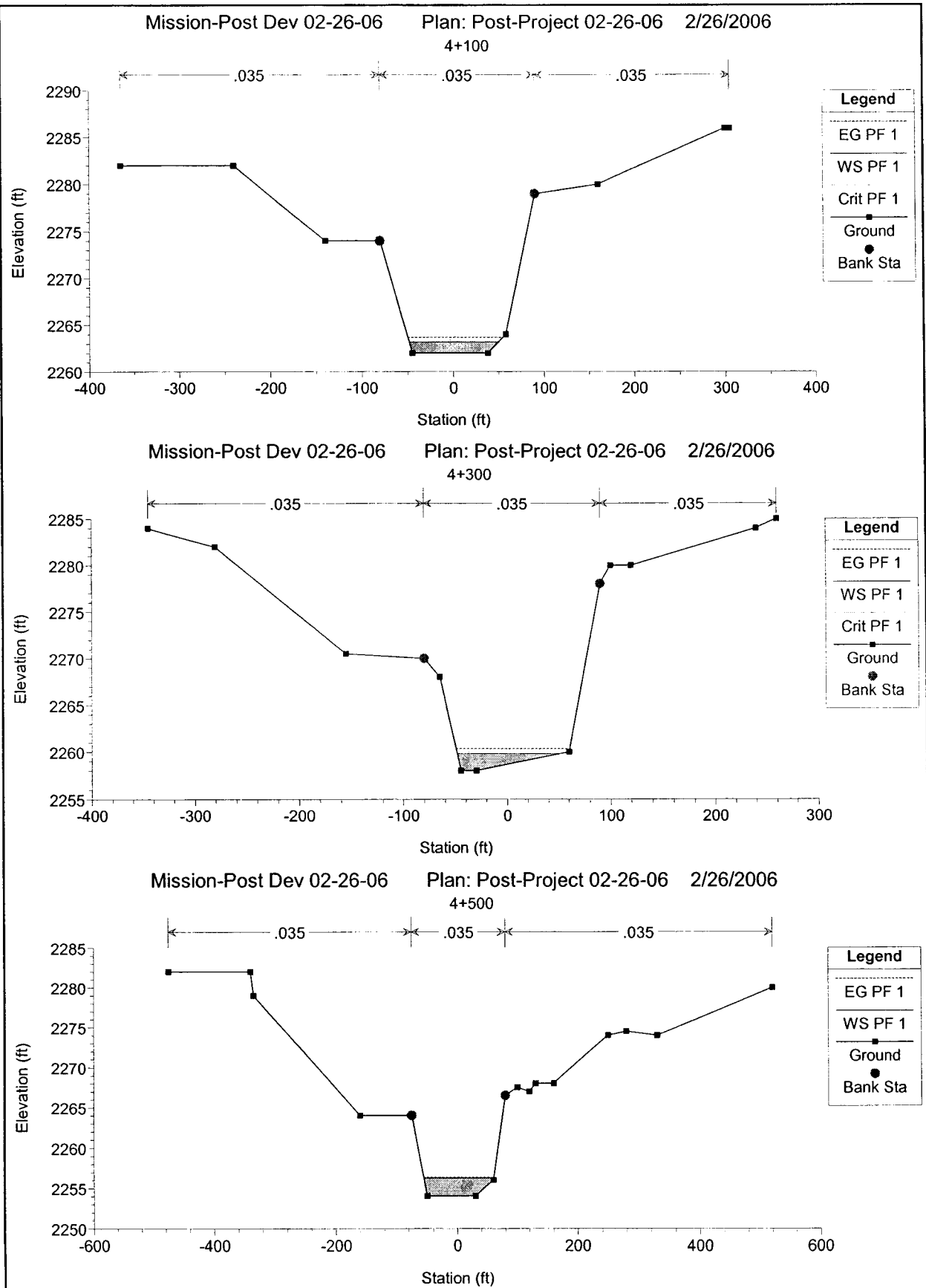
Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006
3+300



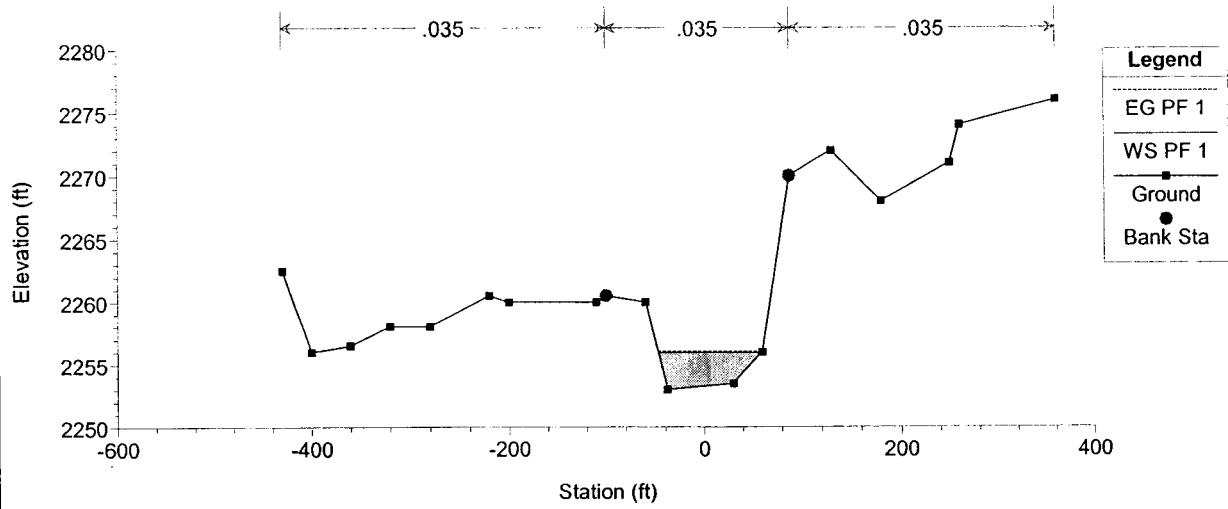
Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006
3+400



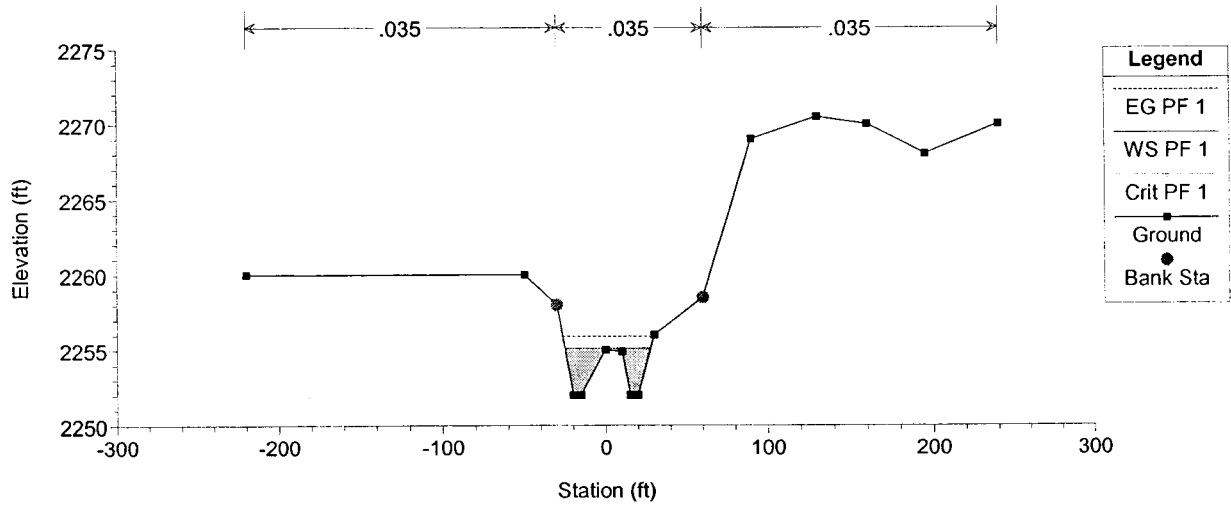




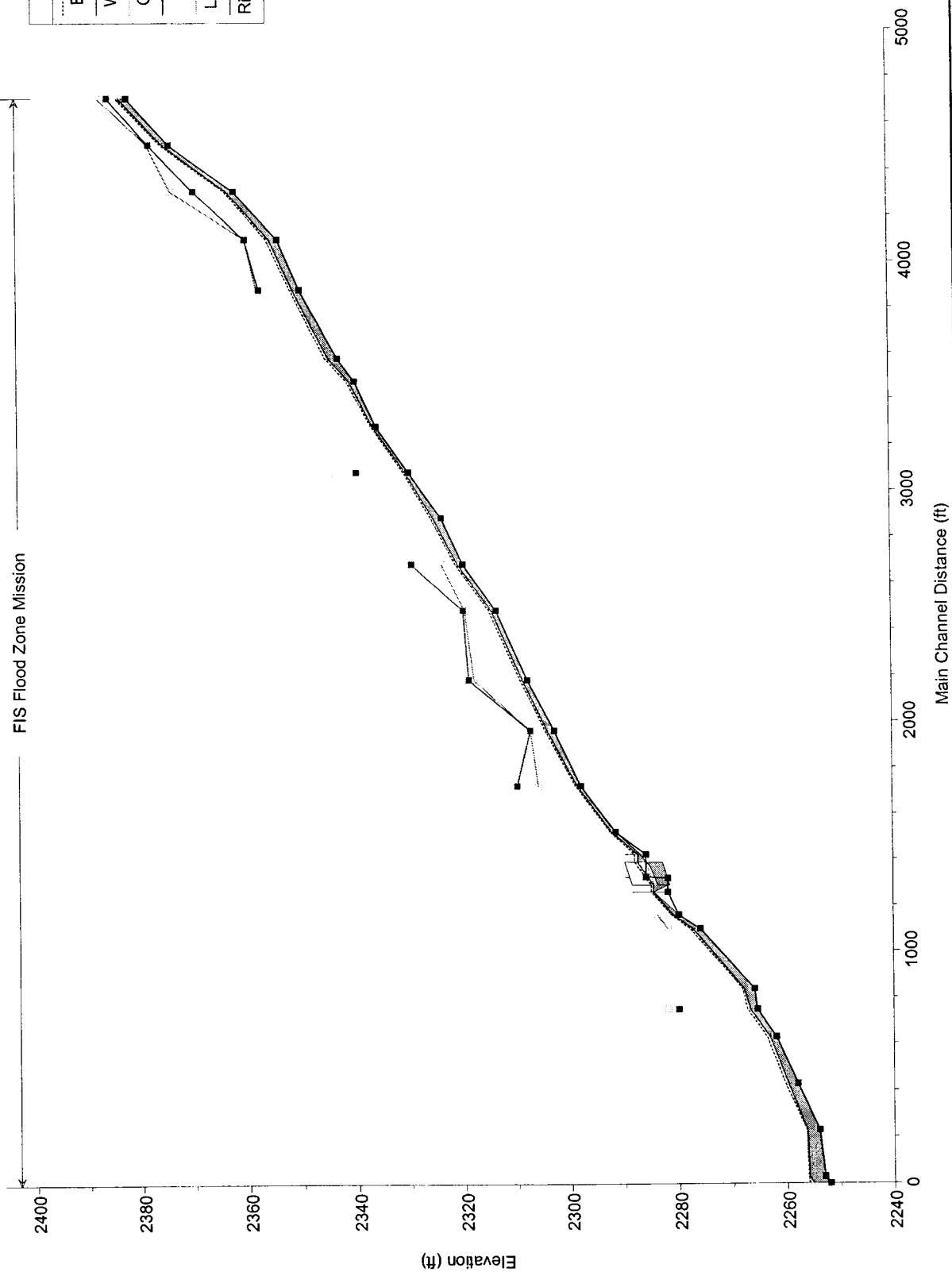
Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006
4+700



Mission-Post Dev 02-26-06 Plan: Post-Project 02-26-06 2/26/2006
4+729



FIS Flood Zone Mission



HEC-RAS Plan: 022606 River: FIS Flood Zone Reach: Mission Profile: PF 1

Reach	River Sta	Cross Section	Sta.	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #	C Hydr Depth (ft)
Mission	48	0+100		PF 1	157	2382	2383.5	2383.5	2383.94	0.018231	5.36	29.32	32.26	0.99	0.91
Mission	46	0+300		PF 1	157	2374	2375.17	2375.17	2375.54	0.019624	4.85	32.34	43.77	1	0.74
Mission	44	0+500		PF 1	157	2362	2363.31	2363.31	2363.69	0.020097	4.9	32.04	43.47	1.01	0.74
Mission	42	0+700		PF 1	157	2354	2355.5	2355.5	2355.99	0.017604	5.63	27.86	27.59	0.99	1.01
Mission	40	0+900		PF 1	157	2350	2351.26	2351.26	2351.71	0.018922	5.37	29.21	32.82	1	0.89
Mission	37	1+200		PF 1	157	2343.07	2344.78	2344.78	2345.34	0.017879	5.98	26.27	23.84	1	1.1
Mission	36	1+300		PF 1	157	2340	2341.02	2341.02	2341.5	0.018636	5.53	28.4	30.04	1	0.95
Mission	34	1+500		PF 1	157	2336	2336.62	2336.62	2336.9	0.02183	4.23	37.07	66.6	1	0.56
Mission	32	1+700		PF 1	157	2330	2330.63	2330.63	2330.94	0.023667	4.47	35.11	61.84	1.05	0.57
Mission	30	1+900		PF 1	157	2324	2325.52	2325.52	2325.91	0.020153	5.01	31.34	41.25	1.01	0.76
Mission	28	2+100		PF 1	157	2320	2320.99	2320.99	2321.37	0.0198	4.97	31.6	41.54	1	0.76
Mission	26	2+300		PF 1	166	2313.84	2314.76	2314.76	2315.16	0.018864	5.07	32.71	40.05	0.99	0.82
Mission	24	2+500		PF 1	166	2308	2308.93	2308.93	2309.34	0.018881	5.09	32.6	39.81	0.99	0.82
Mission	22	2+700		PF 1	166	2303	2304.34	2304.34	2304.69	0.019407	4.78	34.73	47.68	0.99	0.73
Mission	20	2+900		PF 1	166	2298	2298.67	2298.67	2298.94	0.022156	4.19	39.63	73.05	1	0.54
Mission	19	3+000		PF 1	204	2291.63	2292.39	2292.39	2292.59	0.024201	3.57	57.15	143.76	1	0.4
Mission	18	3+100		PF 1	204	2287.03	2287.56	2287.56	2288.09	0.017836	5.84	34.96	32.7	0.99	1.07
Mission	17	Culvert			Culvert										
Mission	16	3+300		PF 1	204	2284.62	2284.64	2284.64	2285.04	0.012747	5.08	40.18	36.29	6.07	1.11
Mission	15	3+400		PF 1	204	2280	2281.07	2281.07	2281.38	0.020877	4.41	46.27	75.83	0.99	0.61
Mission	14	3+500		PF 1	204	2276	2277.39	2277.39	2277.91	0.018013	5.77	35.35	34.43	1	1.03
Mission	12	3+700		PF 1	602	2266	2267.97		2268.22	0.005903	4.03	149.25	108.01	0.6	1.38
Mission	10	3+900		PF 1	602	2265.5	2266.85	2266.85	2267.35	0.017489	5.7	105.57	102.88	0.99	1.03
Mission	8	4+100		PF 1	602	2262	2263.19	2263.14	2263.67	0.015369	5.58	107.79	98.35	0.94	1.1
Mission	6	4+300		PF 1	602	2258	2259.8	2259.8	2260.33	0.018215	5.84	103	99.53	1.01	1.03
Mission	4	4+500		PF 1	602	2254	2256.24		2256.35	0.001717	2.71	222.47	116.05	0.34	1.92
Mission	2	4+700		PF 1	602	2253	2255.94		2256.05	0.001322	2.59	232.61	106.57	0.31	2.18
Mission	1	4+729		PF 1	602	2252	2255.07	2255.07	2255.88	0.016819	7.23	83.25	52.8	1.01	1.58

**CHECK-RAS – (VTN) POST PROJECT
HYDRAULIC MODEL
(022606.PRJ)**

CHECK-RAS Program: NT Check
Manning's n Value and Transition Loss Coefficient Review

Project File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.prj
Plan File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.pl5
Geometry File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.g11
Flow File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.f04
Report File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.nt
Selected profiles: PF 1
Date: 2/27/2006
Time: 11:46:54 AM

SECNO	STRUCTURE	NLOB	NCHL	NROB	CNTR	EXP

FIS	Flood Zone, Mission					
48		0.035	0.035	0.035	0.1	0.3
46		0.035	0.035	0.035	0.1	0.3
44		0.035	0.035	0.035	0.1	0.3
42		0.035	0.035	0.035	0.1	0.3
40		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
37		0.035	0.035	0.035	0.1	0.3
36		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
34		0.035	0.035	0.035	0.1	0.3
32		0.035	0.035	0.035	0.1	0.3
30		0.035	0.035	0.035	0.1	0.3
28		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
26		0.035	0.035	0.035	0.1	0.3
24		0.035	0.035	0.035	0.1	0.3
22		0.035	0.035	0.035	0.1	0.3
20		0.035	0.035	0.035	0.1	0.3
19		0.035	0.035	0.035	0.1	0.3
18		0.035	0.035	0.035	0.1	0.3
17	Culvert-Up	0.035	0.035	0.035	0.1	0.3
17	Culvert-Dn	0.035	0.035	0.035	0.1	0.3
16		0.035	0.035	0.035	0.1	0.3
15		0.035	0.035	0.035	0.1	0.3
14		0.035	0.035	0.035	0.1	0.3
12		0.035	0.035	0.035	0.1	0.3
10		0.035	0.035	0.035	0.1	0.3
8		0.035	0.035	0.035	0.1	0.3
6		0.035	0.035	0.035	0.1	0.3
4		0.035	0.035	0.035	0.1	0.3
2		0.035	0.035	0.035	0.1	0.3
1		0.035	0.035	0.035	0.1	0.3

---Summary of Statistics---

	Minimum	Maximum
Left Overbank n Value:	0.035	0.035
Right Overbank n Value:	0.035	0.035
Channel n Value:	0.035	0.035
Contraction Coefficient:	0.1	0.1
Expansion Coefficient:	0.3	0.3

ROUGHNESS COEFFICIENT CHECK

RS: 48
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 46
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 44
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 42
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 37
NT RC 05 The left overbank n value of 0.035 and the right overbank n value

[illegible]

of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 6

NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 4

NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 2

NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

TRANSITION LOSS COEFFICIENT CHECK

RS: 19

NT TL 01 This is section 4
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

RS: 18

NT TL 01 This is section 3
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

RS: 16

NT TL 01 This is section 2
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

ROUGHNESS COEFFICIENT AT STRUCTURES

---END---

CHECK-RAS Program: NT Check
Manning's n Value and Transition Loss Coefficient Review

Project File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.prj
Plan File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.p15
Geometry File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.g11
Flow File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.f04
Report File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.nt
Selected profiles: PF 1
Date: 2/27/2006
Time: 11:52:31 AM

SECNO	STRUCTURE	NLOB	NCHL	NROB	CNTR	EXP

FIS	Flood Zone,Mission					
48		0.035	0.035	0.035	0.1	0.3
46		0.035	0.035	0.035	0.1	0.3
44		0.035	0.035	0.035	0.1	0.3
42		0.035	0.035	0.035	0.1	0.3
40		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
37		0.035	0.035	0.035	0.1	0.3
36		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
34		0.035	0.035	0.035	0.1	0.3
32		0.035	0.035	0.035	0.1	0.3
30		0.035	0.035	0.035	0.1	0.3
28		-----	0.035	0.035	0.1	0.3
		-----	0.035	-----		
26		0.035	0.035	0.035	0.1	0.3
24		0.035	0.035	0.035	0.1	0.3
22		0.035	0.035	0.035	0.1	0.3
20		0.035	0.035	0.035	0.1	0.3
19		0.035	0.035	0.035	0.1	0.3
18		0.035	0.035	0.035	0.1	0.3
17	Culvert-Up	0.035	0.035	0.035	0.1	0.3
17	Culvert-Dn	0.035	0.035	0.035	0.1	0.3
16		0.035	0.035	0.035	0.1	0.3
15		0.035	0.035	0.035	0.1	0.3
14		0.035	0.035	0.035	0.1	0.3
12		0.035	0.035	0.035	0.1	0.3
10		0.035	0.035	0.035	0.1	0.3
8		0.035	0.035	0.035	0.1	0.3
6		0.035	0.035	0.035	0.1	0.3
4		0.035	0.035	0.035	0.1	0.3
2		0.035	0.035	0.035	0.1	0.3
1		0.035	0.035	0.035	0.1	0.3

---Summary of Statistics---

	Minimum	Maximum
Left Overbank n Value:	0.035	0.035
Right Overbank n Value:	0.035	0.035
Channel n Value:	0.035	0.035
Contraction Coefficient:	0.1	0.1
Expansion Coefficient:	0.3	0.3

ROUGHNESS COEFFICIENT CHECK

RS: 48
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 46
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 44
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 42
NT RC 05 The left overbank n value of 0.035 and the right overbank n value of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 37
NT RC 05 The left overbank n value of 0.035 and the right overbank n value

[illegible]

of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 6

NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 4

NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

RS: 2

NT RC 05 The left overbank n value of 0.035 and the right overbank n value
of 0.035 are less than or equal to the channel n value of 0.035
The overbank n values should be reevaluated.

TRANSITION LOSS COEFFICIENT CHECK

RS: 19

NT TL 01 This is section 4
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

RS: 18

NT TL 01 This is section 3
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

RS: 16

NT TL 01 This is section 2
Contraction and expansion loss coefficients are 0.1 and 0.3
They should be equal to 0.3 and 0.5 respectively.

ROUGHNESS COEFFICIENT AT STRUCTURES

---END---

CHECK-RAS Program, XS Check
Cross Section Location and Alignment Review

Project File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.prj
 Plan File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.p15
 Geometry File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.g11
 Flow File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.f04
 Report File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.xs
 Selected profiles: PF 1
 Date: 2/27/2006
 Time: 11:52:43 AM

SECNO	Len Lob	Len Chl	Len Rob	TopWdthAct	Q Total	Flow Code

FIS Flood Zone, Mission						
48	200	200	200	32.26	157	C
46	200	200	200	43.77	157	C
44	400	210	200	43.47	157	C
42	220	220	350	27.59	157	C
40	300	300	300	32.82	157	E,C
37	100	100	100	23.84	157	C
36	200	200	200	30.04	157	C
34	250	200	200	66.6	157	D,C
32	200	200	200	61.84	157	E,C
30	200	200	200	41.25	157	C
28	210	200	200	41.54	157	E,C
26	300	300	330	40.05	166	E,C
24	220	220	270	39.81	166	E,C
22	230	240	240	47.68	166	E,C
20	200	200	200	73.05	166	D,C
19	100	100	100	143.76	204	C
18	165	165	165	32.7	204	C
17	Culvert #1-Up					
17	Culvert #1-Dn					
16	100	100	110	36.29	204	C
15	60	60	60	75.83	204	C
14	240	260	390	34.43	204	C
12	140	90	120	108.01	602	
10	110	120	125	102.88	602	C
8	200	200	200	98.35	602	
6	200	200	200	99.53	602	C
4	200	200	200	116.05	602	
2	29	29	29	106.57	602	
1	0	0	0	52.8	602	C

B=blocked obstruction			XS SC 05			
C=critical depth			XS SC 03			
D=divided flow			XS SC 01			
E=cross section extended			XS SC 02			
K=known water-surface			XS SC 04			

DISTANCE CHECK

SPACING CHECK

INEFFECTIVE FLOW CHECK

RS: 48
 XS IF 01 Left Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 48
 XS IF 01 Right Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 46
 XS IF 01 Left Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 46
 XS IF 01 Right Levee option is used at this river station
 Please investigate whether the NFIP requirements
 for levees are met.

RS: 44
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 44
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 42
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 42
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 40
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 40
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 32
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 32
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 28
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 28
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 26
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 26
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 24
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 24
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 22
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 22
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 20
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 20
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 15
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 14
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 10
XS IF 01 Left Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

RS: 10
XS IF 01 Right Levee option is used at this river station
Please investigate whether the NFIP requirements
for levees are met.

DISCHARGE CHECK

LOCATION CHECK

RS: 44
XS LC 01 Lenchl Up/TopwdthAct Dn = 7.61
MaxChlDpth Up/MaxChlDpth Dn = 1.21
TopwdthAct Up/TopwdthAct Dn = 1.58
This cross section is located too far upstream from the
critical depth cross section.

RS: 40
XS LC 01 Lenchl Up/TopwdthAct Dn = 12.58
MaxChlDpth Up/MaxChlDpth Dn = 1.91
TopwdthAct Up/TopwdthAct Dn = 1.38
This cross section is located too far upstream from the
critical depth cross section.

RS: 32
XS LC 01 Lenchl Up/TopwdthAct Dn = 4.85
MaxChlDpth Up/MaxChlDpth Dn = 5.78
TopwdthAct Up/TopwdthAct Dn = 1.50
This cross section is located too far upstream from the
critical depth cross section.

RS: 19
XS LC 01 Lenchl Up/TopwdthAct Dn = 3.06
MaxChlDpth Up/MaxChlDpth Dn = 1.43
TopwdthAct Up/TopwdthAct Dn = 4.40
This cross section is located too far upstream from the
critical depth cross section.

BOUNDARY CONDITION CHECK

XS BC 02 The name of the stream is FIS Flood Zone,Mission
Normal S = 0.0229 is specified as the downstream boundary
for profile PF 1

XS BC 02 The name of the stream is FIS Flood Zone,Mission
Critical is specified as the upstream boundary
for profile PF 1

XS BC 03 Maximum number of iterations is 0
It should not be less than 20.

LATERAL WEIRS CHECK

---END---

Project File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.prj
 Plan File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.p15
 Geometry File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.g11
 Flow File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.f04
 Report File: J:\JOBS\6139-CLOMR\MISSION LOMR\HEC-RAS\VTN Model - Post Project\022606.br
 Selected profiles: PF 1
 Date: 2/27/2006
 Time: 11:52:50 AM

RS	MaxLoChord	MnTpRd	EGEL	WSEL	MinChEl	Structure
FIS Flood Zone, Mission						
48			2383.94	2383.5	2382	
46			2375.54	2375.17	2374	
44			2363.69	2363.31	2362	
42			2355.99	2355.5	2354	
40			2351.71	2351.26	2350	
37			2345.34	2344.78	2343.07	
36			2341.5	2341.02	2340	
34			2336.9	2336.62	2336	
32			2330.94	2330.63	2330	
30			2325.91	2325.52	2324	
28			2321.37	2320.99	2320	
26			2315.16	2314.76	2313.84	
24			2309.34	2308.93	2308	
22			2304.69	2304.34	2303	
20			2298.94	2298.67	2298	
19			2292.59	2292.39	2291.63	
18			2288.09	2287.56	2287.03	Lid
17	2290	2286	0	2285.96	2283	Culvert #1-Up
17	2288.6	2282	0	2283.91	2281.6	Culvert #1-Dn
16			2285.04	2284.64	2284.62	Lid
15			2281.38	2281.07	2280	
14			2277.91	2277.39	2276	
12			2268.22	2267.97	2266	
10			2267.35	2266.85	2265.5	
8			2263.67	2263.19	2262	
6			2260.33	2259.8	2258	
4			2256.35	2256.24	2254	
2			2256.05	2255.94	2253	
1			2255.88	2255.07	2252	

RIVER/REACH: FIS Flood Zone, Mission
 RIVER STATION: 17
 TYPE OF STRUCTURE: Culvert

Description:
 Distance from Upstream XS: 100
 Deck/Roadway Width: 4
 Weir Coefficient: 2.6
 Maximum allowable submergence for weir flow: 0.95
 Elevation at which weir flow begins: 0
 Weir crest shape: Broad Crested

Sec	River Station	Length Channel	WSEL	Surch.	EGEL	TopWidth Actual	
4	19	100.00	2292.39		2292.59	143.76	
3	18	165.00	2287.56		2288.09	32.7	
	17	100.00	2285.96		0	0	Culvert #1-Up
	17	30.00	2283.91		0	0	Culvert #1-Dn
2	16	100.00	2284.64		2285.04	36.29	
1	15	60.00	2281.07		2281.38	75.83	

Ineffective Flow, Section 3
 Sta L Sta R Elev

Ineffective Flow, Section 2
 Sta L Sta R Elev

Opening Type StagStaL StagStaR EncStaL EncStaR LifStaS RifStaS
 Culvert Group

CULVERT:

Culvert Name: Culvert #1

Shape: Box Rise: 7 Span: 4 Barrels: 1

FHWA Chart #: # 8 - flared wingwalls

FHWA Scale #: # 1 - Wingwall flared 30 to 75 deg.

Solution Crit: Highest U.S. EG

UpstrmDist:	35	Length:	100	n-Value:	0.014		
EntLossCoef:	0.05	ExtLossCoef:	1	CulvInvElU	2283	CulvInvElD	2281.6
LCntStaU:	223.03	RCntStaU:	223.03	LCntStaD	262.31	RCntStaD	262.31
Culvert Depth Blocked:	0						

Culv Area:	28	CulvQ:	115.47	MinTopRd:	2286.01
------------	----	--------	--------	-----------	---------

	LAbutSt	RAbutSt	LMnTpRd	RMnTpRd	MnTpRd	MxLoCd	
Culvert #1	221.03	225.03	2286	2286	2286	2290	U
	260.31	264.31	2282	2282	2282	2288.6	D

Name	Q Total.	Q Struc	Q Weir	Selected Method	Flow Type
Culvert #1		115.47	88.53	Highest U.S. EG	Low and Weir Flow

GEOMETRIC CHECK

RS: 17
ST GD 03 The starting station of 221.03 from upstream road/weir data is greater than the starting station of 41.32 from upstream internal section/ section 3.
The high chord elevation of 2291 for the starting road/weir station is greater than the ground elevation of 2286 for the same ground station.
The road/weir profile may need to be extended.

RS: 17
ST GD 03 The end station of 225.03 from upstream road/weir data is less than the end station of 432.4 from upstream internal section/section 3.
The high chord elevation of 2291 for the end road/weir station is greater than the ground elevation of 2286 for the same ground station.
The road/weir profile may need to be extended.

RS: 17
ST GD 03 The starting station of 260.31 from downstream road/weir data is greater than the starting station of 48.08 from downstream internal section.
The high chord elevation of 2289.6 for the starting road/weir station is greater than the ground elevation of 2282 for the same ground station.
The road/weir profile may need to be extended.

RS: 17
ST GD 03 The end station of 264.31 from downstream road/weir data is less than the end station of 413.53 from downstream internal section.
The high chord elevation of 2289.6 for the end road/weir station is greater than the ground elevation of 2282.826 for the same ground station.
The road/weir profile may need to be extended.

RS: 16
ST GD 08 'Cross Section Lid' option is used for this section.
Cross section lid data must be removed from this section, unless the structure is modeled as culverts in series.

RS: 18
ST GD 08 'Cross Section Lid' option is used for this section.
Cross section lid data must be removed from this section, unless the structure is modeled as culverts in series.

TYPE OF FLOW CHECK

RS: 17 This is Culvert #1
CV LW 01 Type of flow is low and weir flow because,
1. EGEL 3 of 2288.09 is greater than MinTopRd of 2286.01.
2. EGEL 3 of 2288.09 is less than MxLoCdU of 2290.00.

RS: 17 This is Culvert #1
CV LW 01 Type of flow is low and weir flow because,
1. EGEL 3 of 2288.09 is greater than MinTopRd of 2286.01.

2. CulvWSIn of 2285.96 is less than MxLoCdU of 2290.00.
3. CulvWSOut of 2283.91 is less than MxLoCdD of 2288.60.
4. $Q/AD^{0.5}$ of 1.56 is less than 4.0.

DISTANCE CHECK

CULVERT COEFFICIENT CHECK

RS: 17 This is Culvert #1
CV CF 01 Culvert Chart # is 8 and Scale # is 1
Culvert entrance shape is Wingwall flared 30 to 75 deg.
Culvert entrance loss coefficient is 0.05 It should be equal
to 0.4
Please refer to Table 6.3 on page 6-22 and Tabble 6.4 on page 6-23
of HEC-RAS Hydraulic Reference Manual, September 1998.

CULVERT CRITERIA CHECK

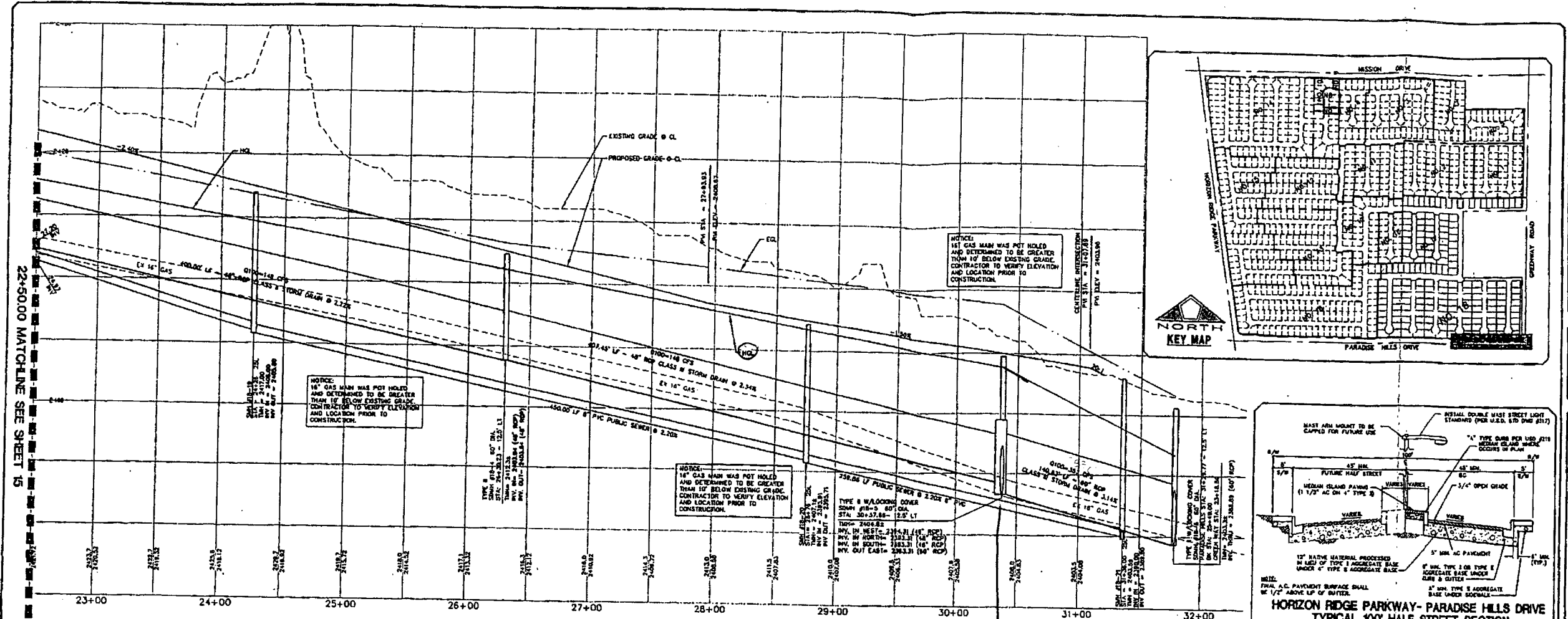
INEFFECTIVE FLOW CHECK

RS: 18 This is section 3
ST GD 05 Weir flow occurs at Culvert Group 1
The velocity head at Section 3 is more than 0.5 foot and more than
the velocity head at Section 4.
Section 3 should be recoded to represent the natural valley
cross section.

---END

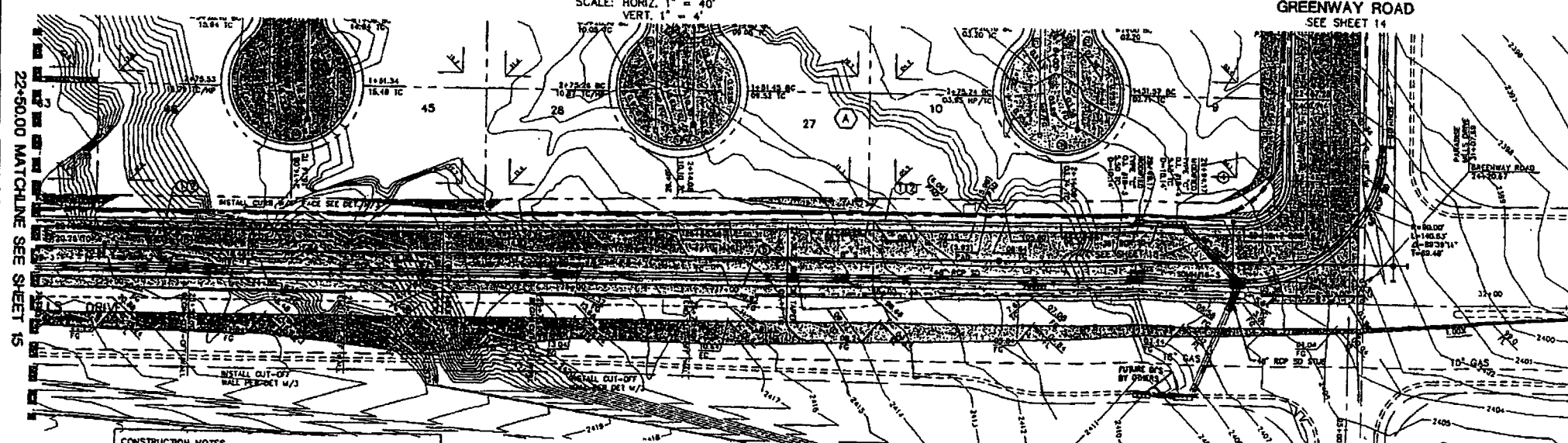
APPENDIX E

REFERENCE MATERIAL



PARADISE HILLS DRIVE
PROFILE

SCALE: HORIZ. 1" = 40'
VERT. 1" = 4'



PARADISE HILLS DRIVE



- CONSTRUCTION NOTES**
- 1. CONSTRUCT SIDEWALK PER USD No. 234
 - 2. CONSTRUCT TYPE "L" CURB & GUTTER PER USD No. 216
 - 3. CONSTRUCT VALLEY GUTTER PER STANDARD DWG No. 228
 - 4. CONSTRUCT HANDICAP RAMP PER STANDARD DWG No. 235 CASE II - SEE SW RAMP TRANSITION TABLE
 - 5. CONSTRUCT MEDIAN ISLAND PER STANDARD DWG No. 218

BENCHMARK

CITY OF HENDERSON SHIP NO. 1, BRASS CAP IN THE TOP OF CURB ON THE NORTHEAST CORNER OF GREENWAY ROAD AND HEADERS STREET.

ELEVATION = 2272.55 FEET NAVD 83 (DATA USED)

PROJECT DATUM = ELEVATION 693.418 METERS NAVD 83

ADD 2.44' TO NAVD 83 DATUM = NAVD 88

Call before you Dig.
1-800-227-2600

SIDEWALK RAMP TRANSITION TABLE

RAMP NO.	GRADE (H) "B" TO "A"	"A" (FT) MIN.	"B" (FT) MIN.
H1	-8.10 - -5.01	4.5	21.5
H2	-5.10 - -4.01	4.5	15.0
H3	-4.10 - -3.01	4.5	12.0
H4	-3.10 - -2.01	4.5	8.5
H5	-2.10 - -1.01	8.0	8.0
H6	1.01 TO 3	9.5	4.5
H7	3.01 TO 4	12.0	4.5
H8	4.01 TO 5	15.0	4.5
H9	5.01 TO 8	21.5	4.5

SEE CLARK COUNTY AREA STANDARD DRAWING NO. 235

CITY APPROVAL OF THE IMPROVEMENT PLANS IS GRANTED FOR ONE (1) YEAR ONLY. PLANS MUST BE RESUBMITTED FOR REVIEW & APPROVAL TO THE DEPARTMENT OF PUBLIC WORKS, CITY OF HENDERSON IF WORK IS NOT COMPLETED BY: 20.

APPROVED BY: _____

REV. Y. KOSHINO, P.E.,
NEW DEVELOPMENT ENGINEER, C.O.H.

DATE: _____

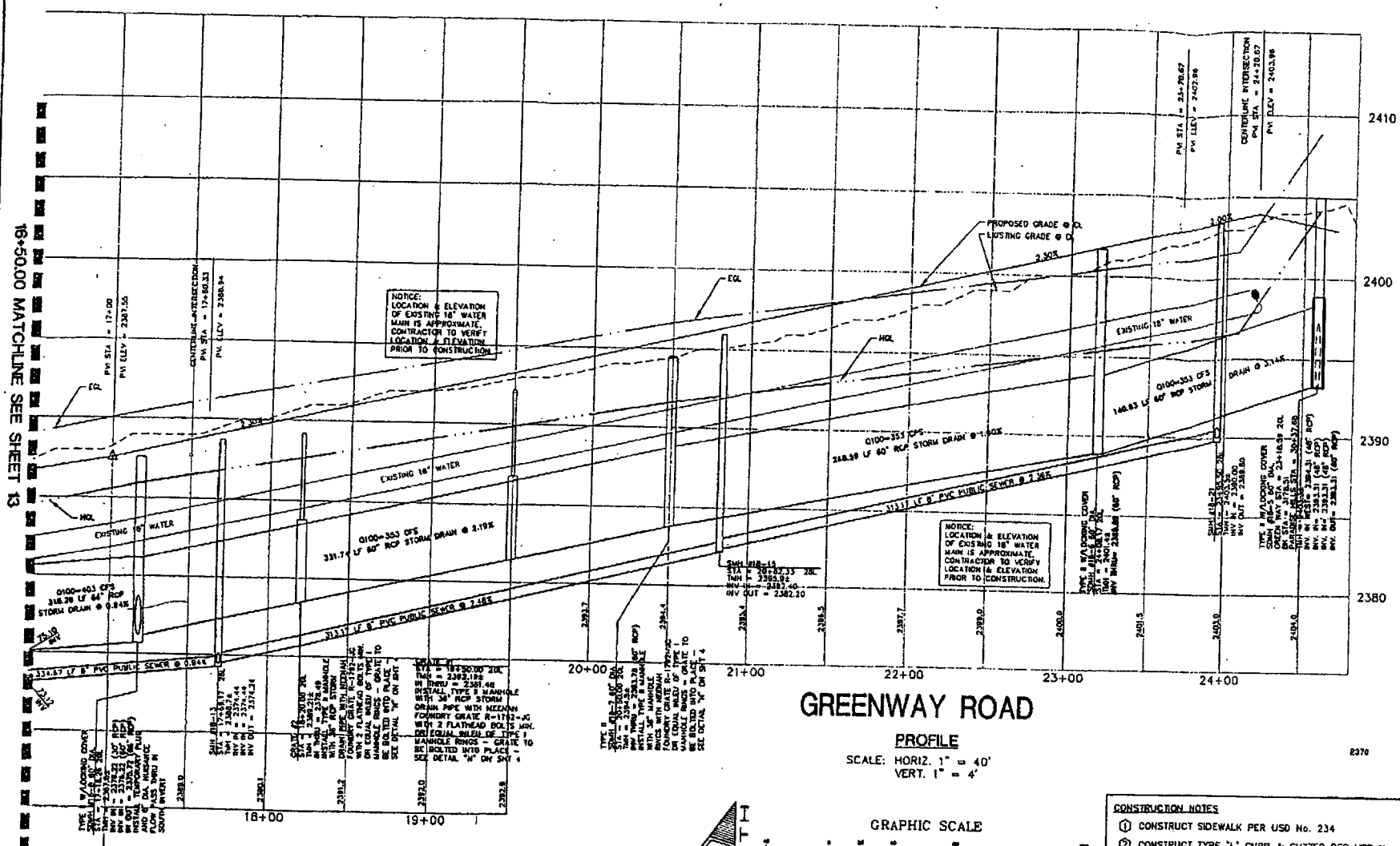
PENTACORE
CIVIL ENGINEERING - LAND SURVEYING - PLANNING
CONSTRUCTION MANAGEMENT - ADA CONSULTING
1783 WEST CHARLESTON BOULEVARD
LAS VEGAS, NEVADA 89146 (702) 268-0115

UPTMAN AND BROAD OF NEVADA, INC.
PARADISE HILLS NO. 18
PARADISE HILLS DRIVE
PLAN & PROFILE
STA: 22+50.00 TO 31+07.69

16
OF 21

16+50.00 MATCHLINE SEE SHEET 13

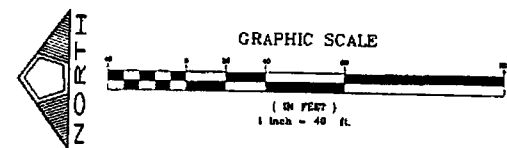
16+50.00 MATCHLINE SEE SHEET 13



GREENWAY ROAD

PROFILE

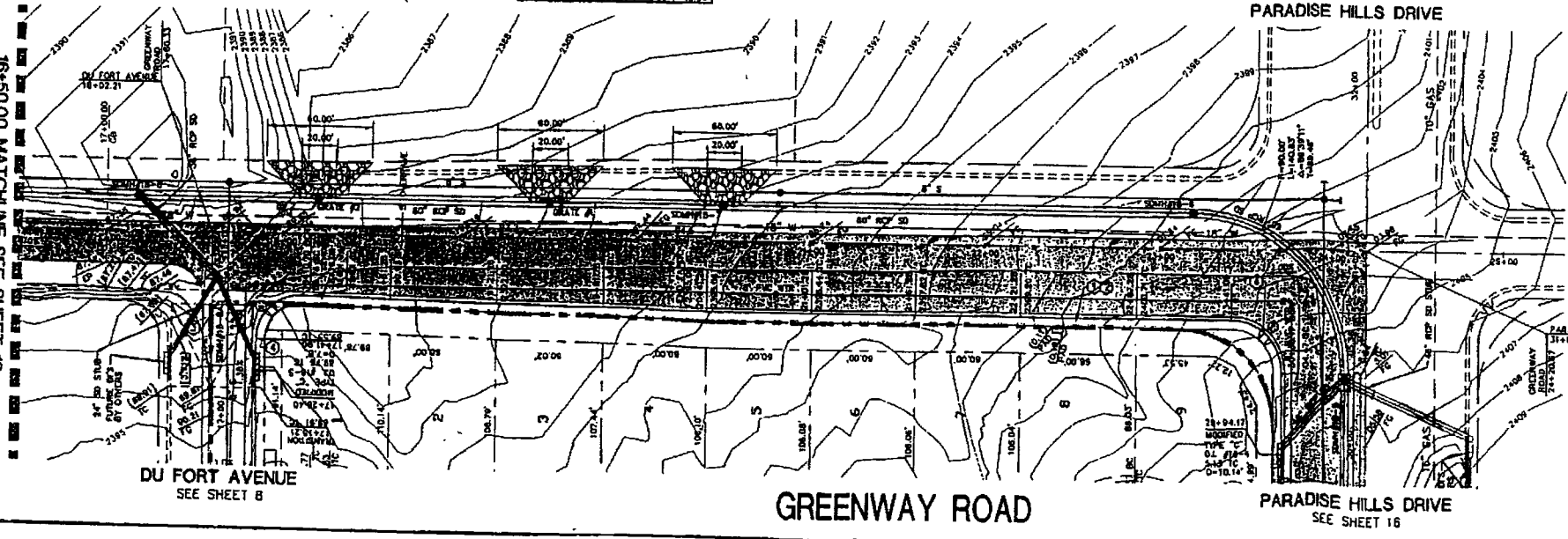
SCALE: HORIZ. 1" = 40'
VERT. 1" = 4'



- CONSTRUCTION NOTES**
- 1. CONSTRUCT SIDEWALK PER STD. NO. 234
 - 2. CONSTRUCT TYPE 'A' CURB & GUTTER PER STD. NO. 216
 - 3. CONSTRUCT VALLEY GUTTER PER STANDARD DWG. NO. 228
 - 4. CONSTRUCT HANDICAP RAMP PER STANDARD DWG. NO. 235 CASE III - SEE SW RAMP TRANSITION TABLE
 - 5. CONSTRUCT MEDIAN ISLAND PER STANDARD DWG. NO. 218

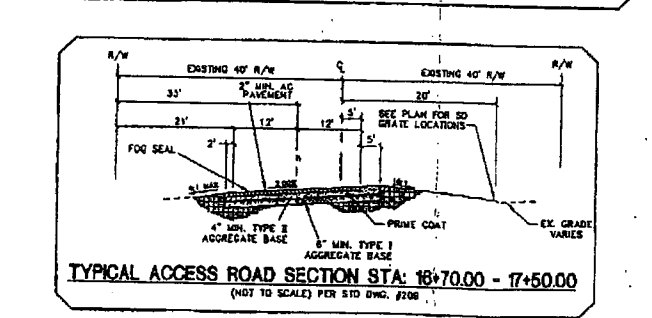
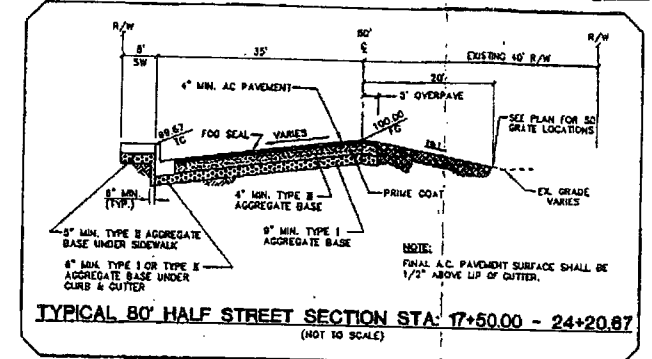
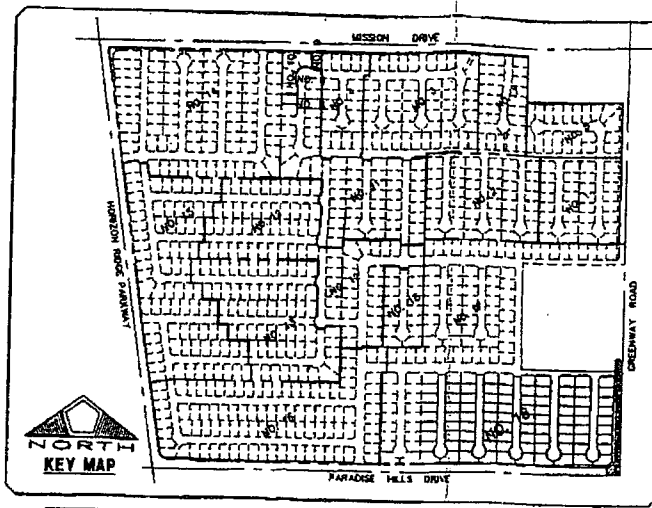
Unit 18 Curve Data

Sta.	Length	Radius	Chord	Offset
18+00	100.00	1000.00	100.00	1.56
18+50	100.00	1000.00	100.00	1.56
19+00	100.00	1000.00	100.00	1.56
19+50	100.00	1000.00	100.00	1.56
20+00	100.00	1000.00	100.00	1.56
20+50	100.00	1000.00	100.00	1.56
21+00	100.00	1000.00	100.00	1.56
21+50	100.00	1000.00	100.00	1.56
22+00	100.00	1000.00	100.00	1.56
22+50	100.00	1000.00	100.00	1.56
23+00	100.00	1000.00	100.00	1.56
23+50	100.00	1000.00	100.00	1.56
24+00	100.00	1000.00	100.00	1.56



GREENWAY ROAD

PARADISE HILLS DRIVE
SEE SHEET 16



SIDEWALK RAMP TRANSITION TABLE

RAMP NO.	GRADE (X)	"A" (FT) MIN.	"B" (FT) MIN.
H1	-8 TO -5.01	4.5	21.5
H2	-5 TO -4.01	4.5	18.0
H3	-4 TO -3.01	4.5	12.0
H4	-3 TO -2.01	4.5	9.5
H5	-2 TO 2	8.0	8.0
H6	2.01 TO 3	8.5	4.5
H7	3.01 TO 4	12.0	4.5
H8	4.01 TO 5	15.0	4.5
H9	5.01 TO 6	21.5	4.5

SEE CLARK COUNTY AREA STANDARD DRAWING NO. 235

BENCHMARK

CITY OF HENDERSON B.M. 101, BRASS CAP IN THE TOP OF CURB ON THE NORTHEAST CORNER OF GREENWAY ROAD AND HEATHER STREET.

ELEVATION = 2272.55 FEET NGVD 29 (DATA USED)

PROJECT DATUM = ELEVATION 823.418 METERS NAVD 83

ADD 1.44' TO NGVD 29 DATUM = NAVD 83

CITY APPROVAL OF THE IMPROVEMENT PLANS IS GRANTED FOR ONE (1) YEAR ONLY. PLANS MUST BE RESUBMITTED FOR REVIEW & APPROVAL TO THE DEPARTMENT OF PUBLIC WORKS, CITY OF HENDERSON IF WORK IS NOT COMPLETED BY: 20

APPROVED BY: _____

REN Y. KOSHINO, P.E.,
NEW DEVELOPMENT ENGINEER, C.O.E.

DATE: _____

Call before you Dig.
1-800-227-2600

Call before you do Overhead
1-702-593-6111

PENTACORE

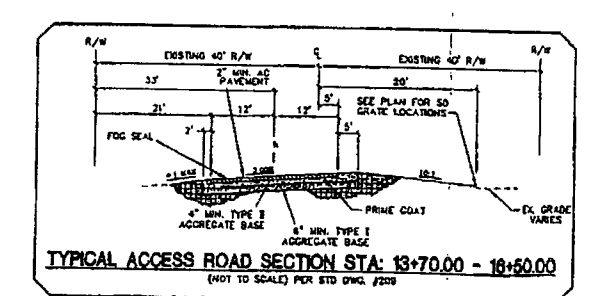
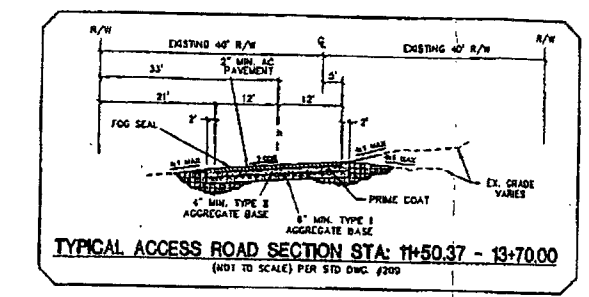
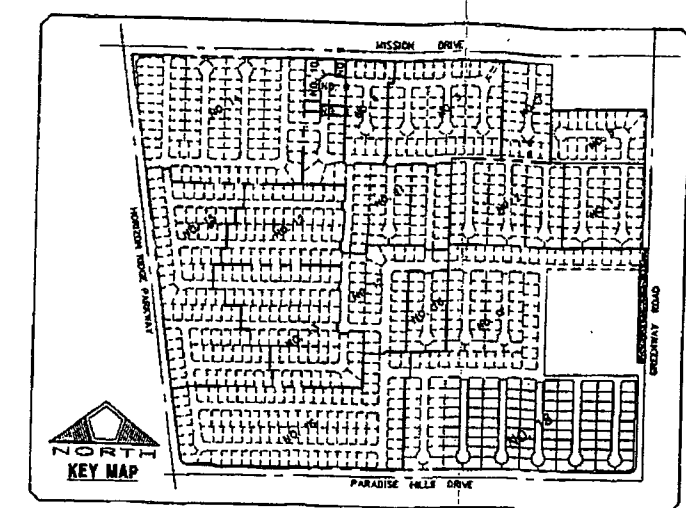
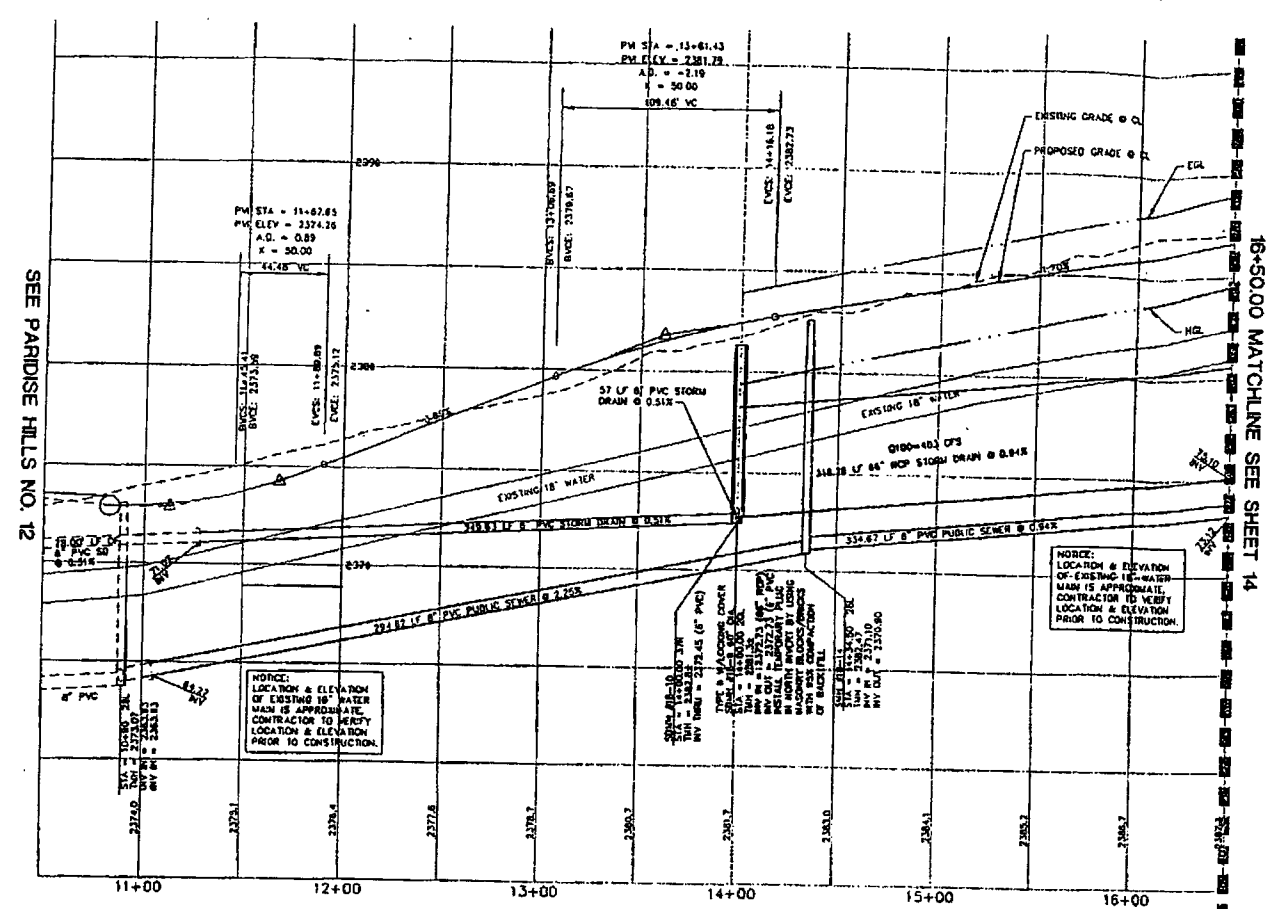
CIVIL ENGINEERING - LAND SURVEYING - PLANNING
CONSTRUCTION MANAGEMENT - AEA CONSULTING
4783 WEST CHARLESTON BOULEVARD
LAS VEGAS, NEVADA 89146 (702) 236-0115

DATE: _____
DRAWN BY: _____
DESIGNED BY: _____
CHECKED BY: _____
JOB NO.: 00000000
SCALE: 1" = 40'

UPMAN AND BROAD OF NEVADA, INC.
PARADISE HILLS NO. 18
GREENWAY ROAD
PLAN & PROFILE II
STA: 16+50.00 TO 24+20.67

PROFESSIONAL ENGINEER - STATE OF NEVADA
SANDY ALWAYNEK
10302

SHEET 14 OF 24



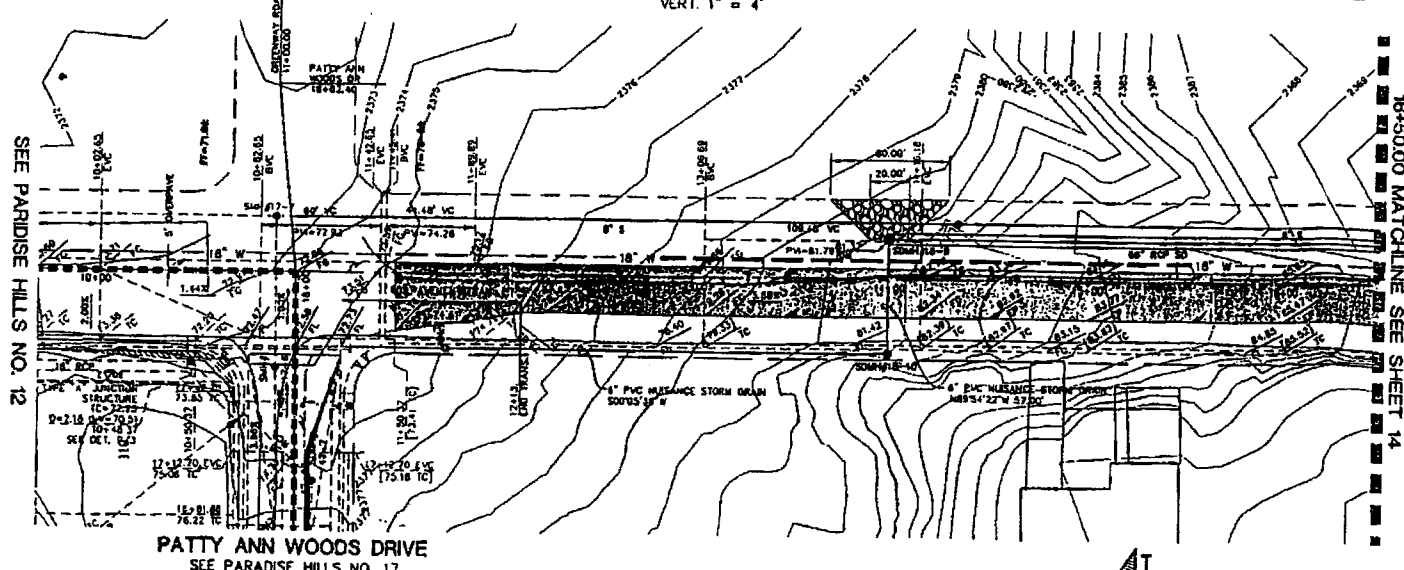
SIDEWALK RAMP TRANSITION TABLE

RAMP NO.	GRADE (X) "B" TO "A"	"A" (FT) MIN.	"B" (FT) MIN.
H1	-4 TO -3.01	4.5	21.5
H2	-3 TO -2.01	4.5	15.0
H3	-2 TO -1.01	4.5	12.0
H4	-1 TO 0	4.5	9.5
H5	0 TO 1	8.0	8.0
H6	1 TO 2	9.5	4.5
H7	2 TO 3	12.0	4.5
H8	3 TO 4	15.0	4.5
H9	4 TO 5	21.5	4.5

SEE CLARK COUNTY AREA STANDARD DRAWING NO. 235

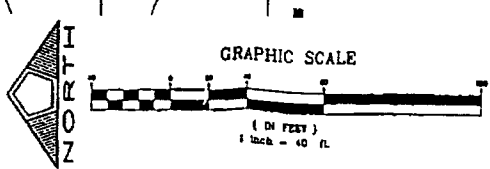
GREENWAY ROAD
PROFILE

SCALE: HORIZ. 1" = 40'
VERT. 1" = 4'



PATTY ANN WOODS DRIVE
SEE PARADISE HILLS NO. 17

GREENWAY ROAD



- CONSTRUCTION NOTES**
1. CONSTRUCT SIDEWALK PER USD NO. 234
 2. CONSTRUCT TYPE "L" CURB & GUTTER PER USD NO. 216
 3. CONSTRUCT VALLEY GUTTER PER STANDARD DWG NO. 226
 4. CONSTRUCT HANDICAP RAMP PER STANDARD DWG NO. 235 CASE III - SEE SW RAMP TRANSITION TABLE
 5. CONSTRUCT MEDIAN ISLAND PER STANDARD DWG NO. 218

Call before you Dig.
1-800-227-2600

Call before you do Overhead
1-702-593-6111

BENCHMARK

CITY OF HENDERSON B.M. 101 BRASS CAP IN THE TOP OF CURB ON THE NORTHEAST CORNER OF GREENWAY ROAD AND HEATHER STREET.

ELEVATION = 2273.55 FEET NAVD 83
(DATA USED)

PROJECT DATUM =
ELEVATION 892.46 METERS NAVD 83
ADD 2.44' TO NAVD 83 DATUM = NAVD 83

CITY APPROVAL OF THE IMPROVEMENT PLANS IS GRANTED FOR ONE (1) YEAR ONLY. PLANS MUST BE RESUBMITTED FOR REVIEW & APPROVAL TO THE DEPARTMENT OF PUBLIC WORKS, CITY OF HENDERSON IF WORK IS NOT COMPLETED BY: 20

APPROVED BY: _____

REN Y. KOSHIRO, P.E.,
NEW DEVELOPMENT ENGINEER, C.O.H.

DATE: _____

PENTACORE
CIVIL ENGINEERING - LAND SURVEYING - PLANNING
6763 WEST CHARLESTON BOULEVARD
LAS VEGAS, NEVADA 89146 (702) 258-0115

MAN AND BROAD OF NEVADA, INC.

PARADISE HILLS NO. 18
GREENWAY ROAD
PLAN & PROFILE I
STA: 11+50.37 TO 16+50.00

PROFESSIONAL ENGINEER - STATE OF NEVADA
SAMIR ALHAYAT
CIVIL
10502

SHEET
13
OF 26

APPENDIX F

DATA CD

Addendum to the Mission Drive Conveyance System LOMR

Case No.: 06-09-B663P
(Mission Drive)
Clark County, Nevada

MAY 2006



2727 S. Rainbow Boulevard, Las Vegas, Nevada 89146

Addendum to the
Mission Drive Conveyance System LOMR
Case No.: 06-09-B663P (Mission Drive)
Clark County, Nevada

Prepared for:

CITY OF HENDERSON
240 Water Street
Henderson, Nevada 89009

Prepared by:

VTN Nevada
2727 S. Rainbow Boulevard
Las Vegas, Nevada 89146
(702) 247-4020



May 2006



NATIONAL FLOOD INSURANCE PROGRAM

FEMA NATIONAL SERVICE PROVIDER

April 14, 2006

Mr. Jeremy Leavitt, P.E.
VTN Nevada
2727 South Rainbow Boulevard
Las Vegas, NV 89146

IN REPLY REFER TO:
Case No.: 06-09-B663P
Community: City of Henderson, NV
Community No.: 320005

316-AD

Dear Mr. Leavitt:

This responds to your request dated March 3, 2006, that the Department of Homeland Security's Federal Emergency Management Agency (FEMA) issue a revision to the Flood Insurance Rate Map (FIRM) for Clark County, Nevada and Incorporated Areas. Pertinent information about the request is listed below.

Identifier:	Mission Drive
Flooding Source:	C-1 Channel
FIRM Panel(s) Affected:	32003C2955 E

The data required to complete our review, which must be submitted within 90 days of the date of this letter, are listed on the enclosed summary.

If we do not receive the required data within 90 days, we will suspend our processing of your request. Any data submitted after 90 days will be treated as an original submittal and will be subject to all submittal/payment procedures, including the flat review and processing fee for requests of this type established by the current fee schedule. A copy of the notice summarizing the current fee schedule, which was published in the *Federal Register*, is enclosed for your information.

FEMA receives a very large volume of requests and cannot maintain inactive requests for an indefinite period of time. In addition, as a result of the aftermath of recent hurricanes, many FEMA employees have been deployed to assist in disaster relief efforts. Therefore, we are unable to grant extensions for the submission of required data/fee for revision requests. If a requester is informed by letter that additional data are required to complete our review of a request, the data/fee **must** be submitted within 90 days of the date of the letter. Any fees already paid will be forfeited for any request for which the requested data are not received within 90 days.

We will continue to work expeditiously to review all submittals in accordance with National Flood Insurance Program (NFIP) regulations, and will aim to meet the regulatory timeframe for the review of all requests. However, requesters should be aware that delays may occur in the review process because of the current emergency situation. We appreciate the patience and cooperation of all requesters as FEMA assists in hurricane relief efforts.

If you have general questions about your request, FEMA policy, or the NFIP, please call the FEMA Map Assistance Center, toll free, at 1-877-FEMA MAP (1-877-336-2627). If you have specific questions concerning your request, please call the Revisions Coordinator for your State, Mr. Sacha Tohme, CFM, who may be reached at (703) 960-8800, ext. 3028.

Sincerely,

A handwritten signature in black ink, appearing to read 'Sheila M. Norlin', with a stylized flourish at the end.

Sheila M. Norlin, CFM
National LOMC Manager
Michael Baker Jr., Inc.

Enclosures

cc: Mr. Curt Chandler, P.E., CFM
Land Development Manager
Department of Public Works
City of Henderson

Mr. Joseph Damiani, P.E.
Project Manager
City of Henderson

Mr. Kevin Eubanks, P.E., CFM
Assistant General Manager
Clark County Regional Flood Control District



NATIONAL FLOOD INSURANCE PROGRAM

FEMA NATIONAL SERVICE PROVIDER

Summary of Additional Data Required to Support a Letter of Map Revision (LOMR)

Case No.: 06-09-B633P

Requester: Mr. Jeremy Leavitt, P.E.

Community: City of Henderson, NV

Community No.: 320005

The issues listed below must be addressed before we can continue the review of your request.

1. The submitted plans entitled "Storm Drain Plan and Profile," prepared by your firm, dated September 9, 2004, are not certified as representing as-built conditions. Please submit "as-built" plans or a letter stating that the submitted plans represent as-built conditions. The plans or letter must be certified by a registered professional engineer or licensed land surveyor.
2. Our preliminary review revealed that "as-built" plans for the culvert upstream of Patti Ann Woods Drive were not submitted in the report entitled "LOMR Mission Drive Conveyance System," prepared by your firm, dated March 3, 2006. Please submit "as-built" plans for the culvert upstream of Patti Ann Woods Drive, certified by a registered professional engineer or licensed land surveyor.
3. Our preliminary review revealed that the submitted undated topographic work maps entitled "Mission-Greenway Work Map," prepared by your firm, were not certified by a registered professional engineer. Please submit topographic work maps with the proposed conditions floodplain boundary delineated, certified by a registered professional engineer or licensed land surveyor.
4. Our preliminary review revealed that the submitted report entitled "LOMR Mission Drive Conveyance System," prepared by your firm, dated March 3, 2006, did not include a work map for the submitted WSPG hydraulic analysis model for the culvert and channel along Greenway Road and Mission Drive. Please submit a work map showing the locations and alignments of all cross sections used in the WSPG hydraulic analysis. The scale of the map must be sufficient to provide reasonable accuracy and it must be certified by a registered professional engineer.
5. Please submit a digital copy of the input and output files for the WSPG model entitled "VTN3.dat" and the HEC-1 models entitled "SDN3.dat" and "missiond.dat." Digital copies of these files were omitted from the original submittal.

Please send the required data directly to us at the address shown at the bottom of this page. For identification purposes, please include the case number referenced above on all correspondence.



Federal Emergency Management Agency

Washington, D.C. 20472

FEE SCHEDULE FOR PROCESSING REQUESTS FOR MAP CHANGES

This notice contains the fee schedule for processing certain types of requests for changes to National Flood Insurance Program (NFIP) maps. The fee schedule allows FEMA to further reduce the expenses to the NFIP by more fully recovering the costs associated with processing conditional and final map change requests. The fee schedule for map changes is effective for all requests dated October 30, 2005, or later and supersedes the fee schedule that was established on September 1, 2002.

To develop the fee schedule for conditional and final map change requests, FEMA evaluated the actual costs of reviewing and processing requests for Conditional Letters of Map Amendment (CLOMAs), Conditional Letters of Map Revision – Based on Fill (CLOMR-Fs), Conditional Letters of Map Revision (CLOMRs), Letters of Map Revision – Based on Fill (LOMR-Fs), Letters of Map Revision (LOMRs), and Physical Map Revisions (PMRs).

Based on our review of actual cost data for Fiscal Years 2004 and 2005, FEMA has established the following review and processing fees, which are to be submitted with all requests that are not otherwise exempted under 44 CFR 72.5.

Fee Schedule for Requests for CLOMAs, CLOMR-Fs, and LOMR-Fs

Request for single-lot/single-structure CLOMA and CLOMR-F	\$500
Request for single-lot/single structure LOMR-F	\$425
Request for single-lot/single-structure LOMR-F based on as-built information (CLOMR-F previously issued by us)	\$325
Request for multiple-lot/multiple-structure CLOMA	\$700
Request for multiple-lot/multiple-structure CLOMR-F and LOMR-F	\$800
Request for multiple-lot/multiple-structure LOMR-F based on as-built information (CLOMR-F previously issued)	\$700

Fee Schedule for Requests for CLOMRs

Request based on new hydrology, bridge, culvert, channel, or combination of any of these	\$4,000
Request based on levee, berm, or other structural measure	\$5,000

Fee Schedule for Requests for LOMRs and PMRs

Requesters must submit the review and processing fees shown below with requests for LOMRs and PMRs that are not based on structural measures or alluvial fans.

Request based on bridge, culvert, channel, or combination thereof	\$4,400
Request based on levee, berm, or other structural measure	\$6,000
Request based on as-built information submitted as follow-up to CLOMR	\$4,000

Fees for CLOMRs, LOMRs, and PMRs Based on Structural Measures on Alluvial Fans

FEMA has revised the initial fee for requests for CLOMRs and LOMRs based on structural measures on alluvial fans to \$5,600. FEMA will also continue to recover the remainder of the review and processing costs by invoicing the requester before issuing a determination letter, consistent with current practice. The prevailing private-sector labor rate charged to FEMA (\$60 per hour) will be used to calculate the total reimbursable fees.

Payment Submission Requirements

Requesters must make fee payments for non-exempt requests before we render services. This payment must be in the form of a check or money order or by credit card payment. Please make all checks and money orders in U.S. funds payable to the *National Flood Insurance Program*. We will deposit all fees collected to the National Flood Insurance Fund, which is the source of funding for providing this service.



CONSULTING ENGINEERS • PLANNERS • SURVEYORS

PROVIDING QUALITY PROFESSIONAL
SERVICES SINCE 1960

May 10, 2005
File: 6139-LOMR

Sheila M. Norlin, CFM
National LOMC Manager
Michael Baker Jr., Inc.

Federal Emergency Management Agency
3601 Eisenhower Avenue
Alexandria, VA 22304-6425

Reference: Case No.: 06-09-B663P (Mission Drive)
Community: City of Henderson, NV
Community No.: 320005

Dear Ms. Norlin:

The enclosed addendum is being provided in response to the comment letter dated April 14, 2006 for the Mission Drive LOMR Case No.: 06-09-B663P. The comments that you provided for the specified project are addressed within the following response summary.

RESPONSE TO COMMENTS

Comment 1: The letter of completion for the Storm Drain Plan & Profile along with “as-Built” plans were submitted with Mission Drive Conveyance System LOMR dated March 2006. It can be found in Appendix D, titled Storm Drain Plan & Profile for Mission Drive/Greenway Rd Improvements (WSPG run from Mission Drive/Greenway Road Improvements Final Drainage Report February 2004)

Comment 2: As-built plans for culvert upstream of Patti Ann Woods Drive on Greenway Road were obtained at City of Henderson and are included in the addendum report. It can be found in Appendix E, under Mission-Greenway: As-Built Plans Reference (Paradise Hills No. 18-PENTACORE) for culvert upstream of Patti Ann Woods

Reference: Addendum to the LOMR for Case No.: 06-09-B663P (Mission Drive)

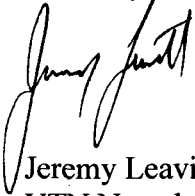
Comment 3: Topographic Work Maps entitled Annotated Flood Zone Map (Figure 2.3), Pre-Project Conditions “Effective Work Map” (Figure 2.4), Post-Project Conditions “Post Project Work Map” (Figure 2.5), and Mission-Greenway Culvert & Channel “Hydraulic Work Map” (Figure 2.6) have been certified by a registered professional engineer or licensed land surveyor.

Comment 4: Work Maps titled Mission-Greenway Culvert & Channel “Hydraulic Work Map” (Figure 2.6) for use with culvert and channel along Greenway Road and Mission Drive have been included in the addendum & have been certified by a registered professional engineer or licensed land surveyor. A Hydraulic Summary for Mission Drive/Greenway Road Improvements for the system VTN3.dat has been included.

Comment 5: A digital Copy of WSPG models VTN3.dat & HEC-1 Models “SDN3.dat and missiond.dat are included in the addendum along with the updated work maps under Updated Data CD (HEC-1, WSPG, Work Maps & figures)

If you have any questions or require additional information, do not hesitate to contact us.

Sincerely,



Jeremy Leavitt, P.E.

VTN Nevada

2727 South Rainbow Boulevard

Las Vegas, NV 89146

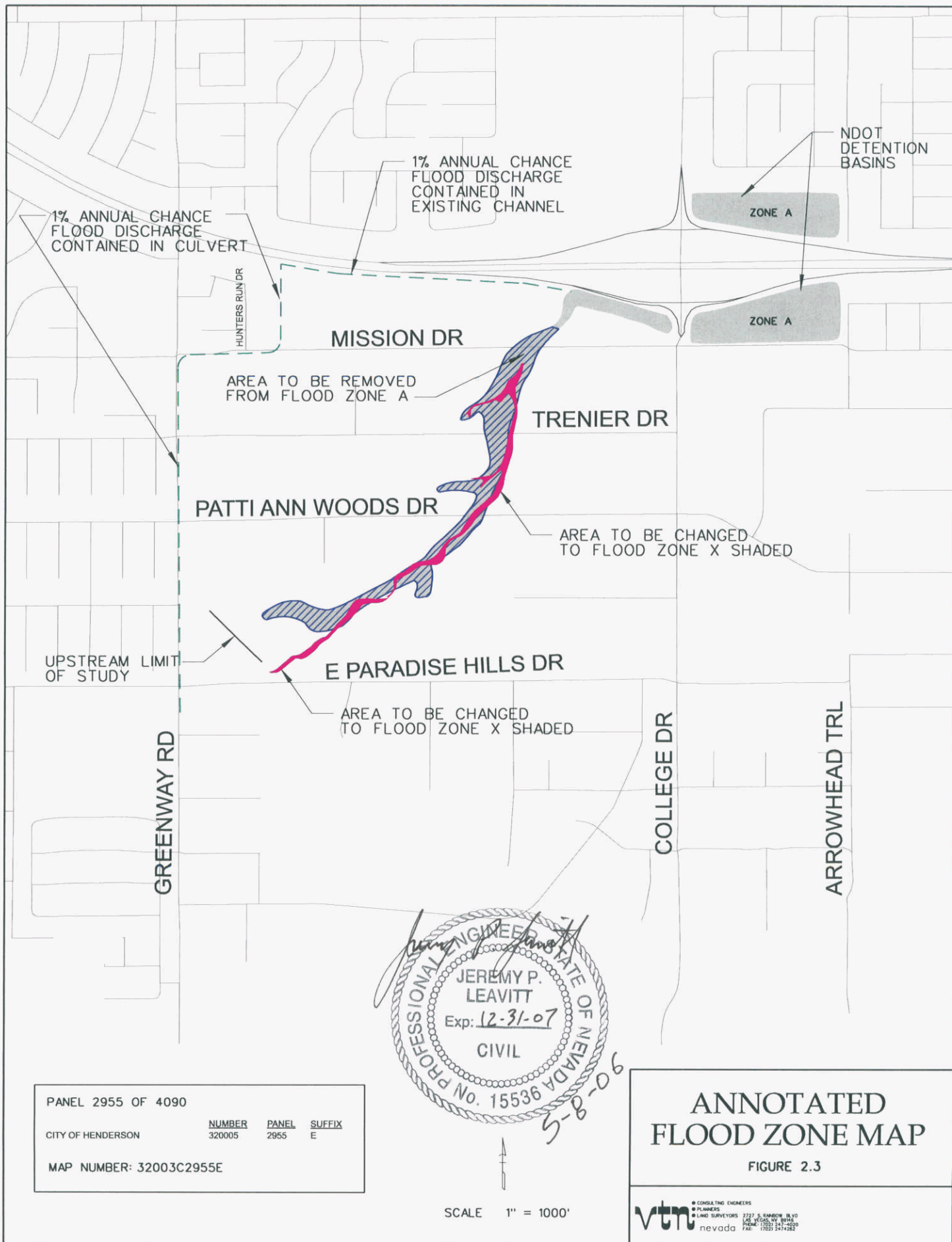
jeremyl@vtnnv.com

(702) 253-2359

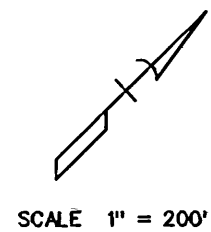
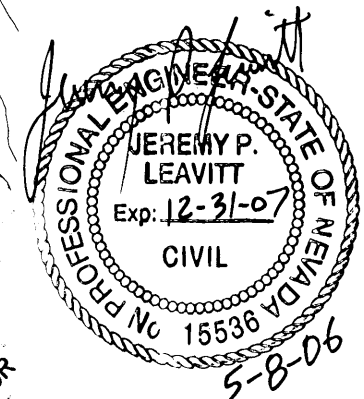
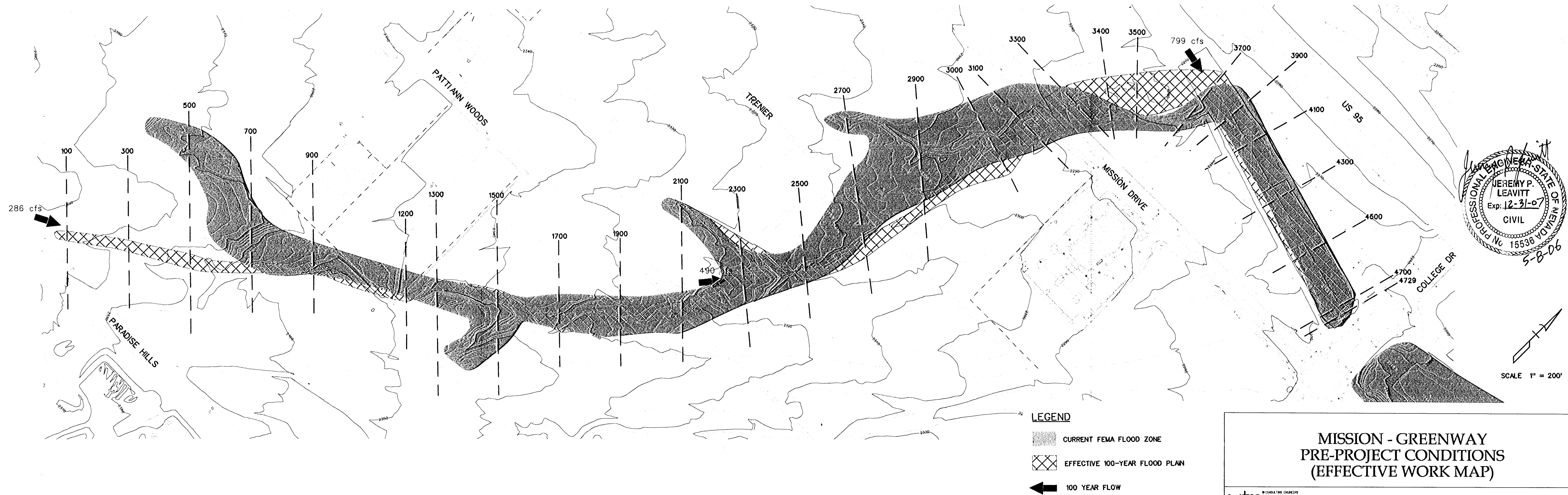
APPENDIX B

FIGURES

**VTN POST-PROJECT
ANNOTATED FLOOD ZONE MAP
-FIGURE 2.3**



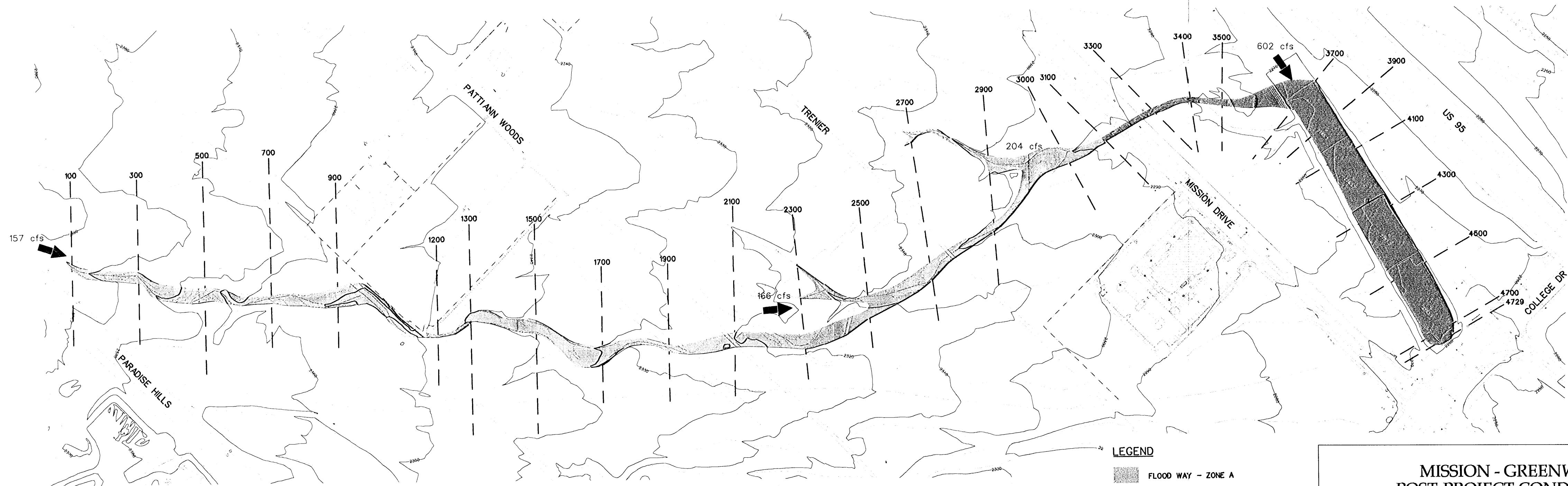
MISSION-GREENWAY: PRE-PROJECT CONDITIONS
(EFFECTIVE WORK MAP)
-FIGURE 2.4



MISSION - GREENWAY PRE-PROJECT CONDITIONS (EFFECTIVE WORK MAP)

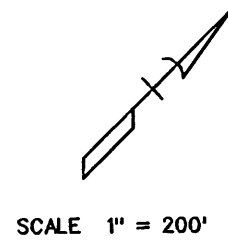
vtn CONSULTING ENGINEERS
PLANNERS
LAND SURVEYORS
7727 S. RANCHO BLVD.
LAS VEGAS, NV 89148
PHONE (702) 247-4200
FAX (702) 247-4201

MISSION-GREENWAY: POST-PROJECT CONDITIONS
(POST PROJECT WORK MAP)
-FIGURE 2.5



LEGEND

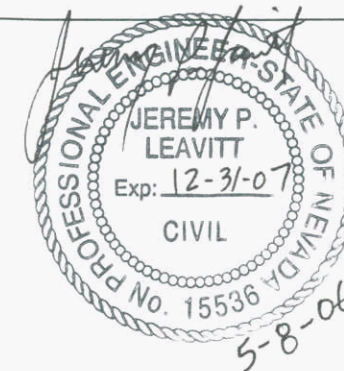
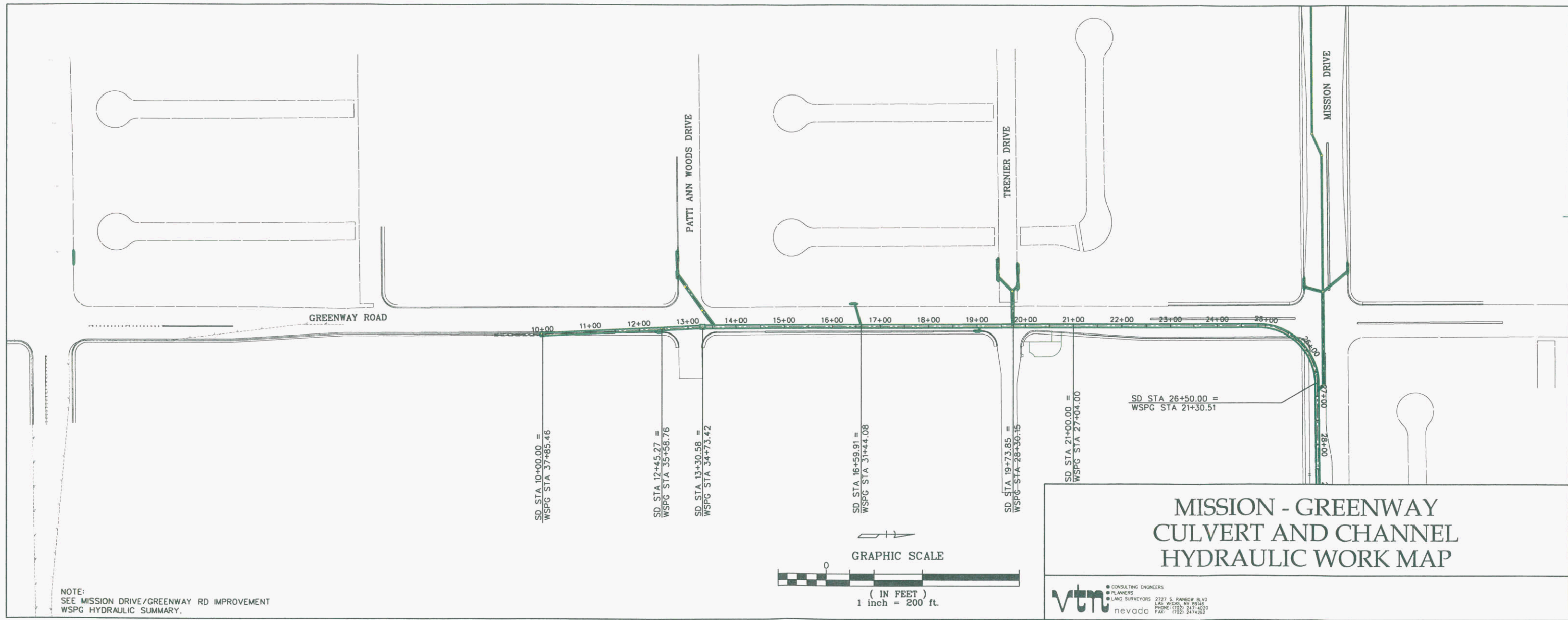
- FLOOD WAY - ZONE A
- FLOOD WAY - ZONE X SHADED
- 100 YEAR FLOW

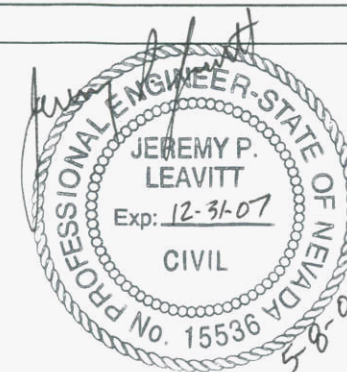
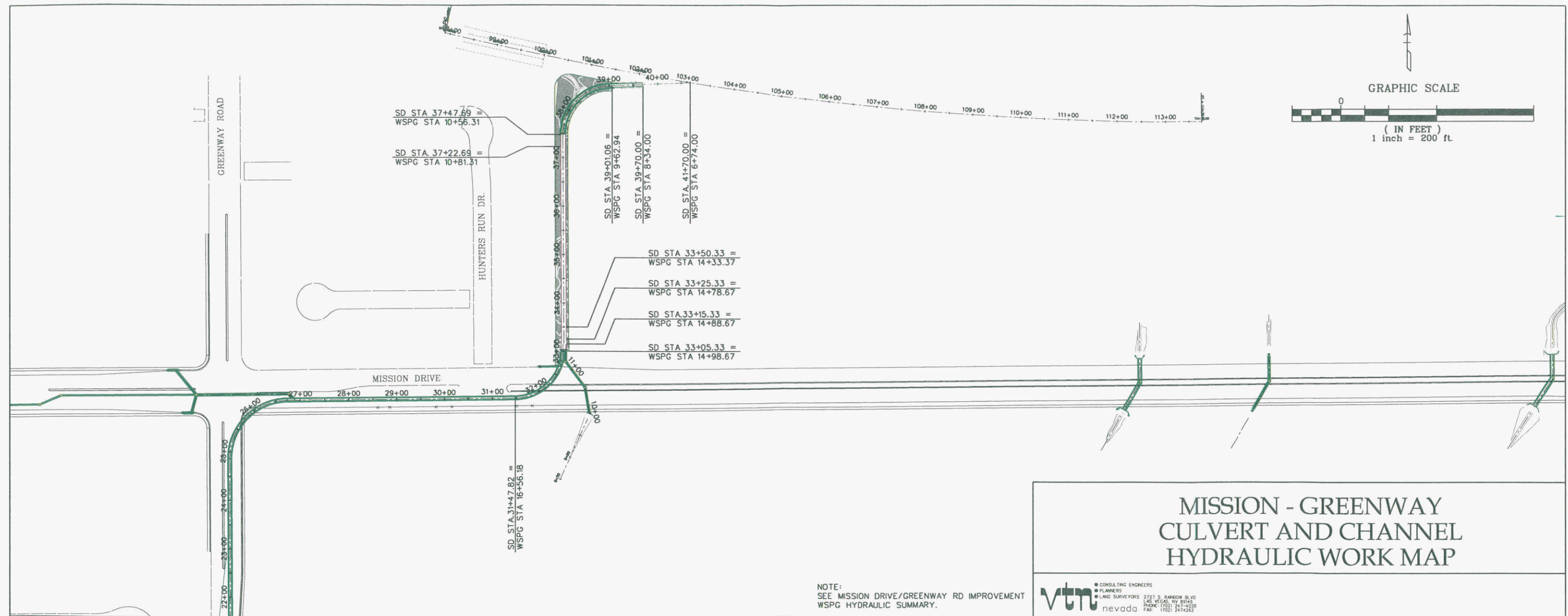


**MISSION - GREENWAY
POST-PROJECT CONDITIONS
(POST PROJECT WORK MAP)**

vtn CONSULTING ENGINEERS
PLANNERS
LAND SURVEYORS
NEVADA
2727 S. SANDY BLVD.
SUITE 200, LAS VEGAS, NV 89102
TEL: 702.251.1100 FAX: 702.251.1101

MISSION-GREENWAY: CULVERT & CHANNEL
(HYDRAULIC WORK MAP for WSPG - VTN3.OUT)
-FIGURE 2.6





**HYDRAULIC SUMMARY FOR MISSION
DRIVE/GREENWAY ROAD IMPROVEMENTS**
(For use with WSPG Model - VTN3.OUT)

MISSION DRIVE/GREENWAY ROADWAY IMPROVEMENT

For use with Mission/Greenway Storm Drain Plan & Profile/ WSPG
WSPG HYDRAULIC SUMMARY WITH 100YR FLOW CONDITION

WSPG STATION	SD PROFILE STATION	LENGTH IN WSPG (ft)	DESIGN FLOW (cfs)	INVERT ELEV (ft)	SLOPE (ft/ft)	DEPTH OF FLOW ⁽¹⁾ y* (ft)	DEPTH OF FLOW y (ft)	VELOCITY V (fps)	H.G.L. H (ft)	E.G.L. E (ft)	CHANNEL TYPE	BASE WIDTH b (ft)	Z	FROUDE NUMBER Fr	DESIGN WALL H.T. (ft)	FREEBOARD (ft)	COMMENTS
574.00			819.1	2303.54		2.119	2.119	9.37	2305.659	2307.02	EX. TRAP.	37	2	1.13	5	2.88	TEMP. RIPRAP
674.00	41+70.00	100.00	819.1	2305.64	0.021	2.101	2.101	9.46	2307.741	2309.13	EX. TRAP.	37	2	1.15	5	2.90	TEMP. RIPRAP
774.00	40+70.00	100.00	819.1	2307.74	0.021	1.124	0.982	21.40	2308.722	2315.83	EX. TRAP.	37	2	3.81	5	4.02	TEMP. RIPRAP
834.00	39+70.00	60.00	630.1	2309.00	0.021	3.590	3.473	22.68	2312.473	2320.46	RCB	8	0	2.14	6	2.53	OK
868.47	39+35.53	34.47	630.1	2309.80	0.023	3.642	3.536	22.27	2313.336	2321.04	RCB	8	0	2.09	6	2.46	OK
902.94	39+01.06	34.47	630.1	2310.61	0.023	3.710	3.617	21.77	2314.227	2321.59	RCB	8	0	2.02	6	2.38	OK
979.63	38+24.37	76.69	630.1	2312.39	0.023	3.928	3.877	20.31	2316.267	2322.67	RCB	8	0	1.82	6	2.12	OK
1056.31	37+47.69	76.68	630.1	2314.18	0.023	4.429	4.429	17.78	2318.609	2323.52	RCB	8	0	1.49	6	1.57	OK
1081.31	37+22.69	25.00	630.1	2314.76	0.023	4.667	4.667	16.87	2319.427	2323.65	RECT	8	0	1.38	6.5	1.83	REQ. FREEBOARD=1.70', OK
1453.67	33+50.33	372.36	630.1	2318.49	0.010	4.145	4.133	19.06	2322.623	2328.26	RECT	8	0	1.65	6.5	2.37	REQ. FREEBOARD=1.76', OK
1478.67	33+25.33	25.00	630.1	2318.74	0.010	4.063	4.037	19.51	2322.777	2328.69	RECT	8	0	1.71	11	6.96	OK
1488.67	33+15.33	10.00	630.1	2318.84	0.010	2.993	2.871	21.94	2321.711	2329.19	RECT	10	0	2.28	11	8.13	OK
1498.67	33+05.33	10.00	606.1	2318.94	0.010	5.441	5.441	18.57	2324.381	2329.74	RCB	6	0	1.40	6	0.56	OK
1656.18	31+47.82	157.51	606.1	2320.51	0.010	5.212	5.212	19.38	2325.722	2331.55	RCB	6	0	1.50	6	0.79	OK
2116.18	26+87.82	460.00	606.1	2325.12	0.010	4.092	3.923	25.75	2329.043	2339.34	RCB	6	0	2.29	6	2.08	OK
2119.68	26+84.32	3.50	580.7	2325.15	0.009	3.756	3.542	27.32	2328.692	2340.28	RCB	6	0	2.56	6	2.46	OK
2130.51	26+73.49	10.83	580.7	2325.26	0.010	3.725	3.504	27.62	2328.764	2340.61	RCB	6	0	2.60	6	2.50	OK
2318.25	24+85.75	187.74	580.7	2331.23	0.032	3.767	3.556	27.22	2334.786	2346.29	RCB	6	0	2.54	6	2.44	OK
2704.00	21+00.00	385.75	580.7	2343.53	0.032	4.187	4.067	23.80	2347.597	2356.39	RCB	6	0	2.08	6	1.93	OK
2804.00	20+00.00	100.00	580.7	2347.74	0.042	5.601	5.601	17.28	2353.341	2357.98	RCB	6	0	1.29	6	0.40	OK
2825.15	19+78.85	21.15	580.7	2348.12	0.018	6.000	6.000	16.24	2354.120	2358.22	RCB	6	0	1.17	6	0.00	OK
2830.15	19+73.85	5.00	494.9	2348.21	0.018	8.204	8.204	13.84	2356.414	2359.39	RCB	6	0	0.85	6	0.00	OK
2890.01	19+07.99	59.86	494.9	2349.26	0.018	7.650	7.650	13.84	2356.930	2359.90	RCB	6	0	0.88	6	0.00	OK
2892.01	19+05.99	2.00	480.6	2349.32	0.020	7.926	7.926	13.44	2357.246	2360.05	RCB	6	0	0.84	6	0.00	OK
2978.61	18+19.39	86.60	480.6	2350.87	0.018	7.131	7.131	13.44	2358.001	2360.81	RCB	6	0	0.89	6	0.00	OK
2978.61	18+19.39	0.00	480.6	2350.87	N/A	4.000	3.953	20.26	2354.823	2361.20	RCB	6	0	1.80	6	2.05	OK
3138.08	16+65.91	159.47	480.6	2353.72	0.018	4.231	4.226	18.96	2357.946	2363.53	RCB	6	0	1.63	6	1.77	OK
3144.08	16+59.91	6.00	458.3	2353.83	0.018	3.750	3.681	20.75	2357.511	2364.20	RCB	6	0	1.91	6	2.32	OK
3467.42	13+36.58	323.34	458.3	2359.63	0.018	4.092	4.086	18.69	2363.716	2369.14	RCB	6	0	1.63	6	1.91	OK
3473.42	13+30.58	6.00	360.0	2359.93	0.050	3.382	3.209	25.01	2363.139	2372.85	RCP	0	0	2.46	5.5	2.29	OK
3558.73	12+45.27	85.31	360.0	2363.44	0.041	3.589	3.469	22.80	2366.909	2374.98	RCP	0	0	2.16	5.5	2.03	OK
3563.73	12+40.27	5.00	330.3	2363.65	0.042	3.137	2.948	25.47	2366.598	2376.67	RCP	0	0	2.61	5.5	2.55	OK
3785.46	10+00.00	221.73	330.3	2372.79	0.041	3.966	3.966	18.01	2376.756	2381.79	RCP	0	0	1.59	5.5	1.53	OK
3809.00		23.54	330.3	2373.76	0.041	4.933	4.933	14.70	2378.693	2382.05	RCP	0	0	1.17	5.5	0.57	OK
4122.26		313.26	330.3	2375.72	0.006	6.393	6.393	13.90	2382.113	2385.11	RCP	0	0	0.97	5.5	0.00	OK
4126.26		4.00	288.1	2375.82	0.025	3.267	3.151	22.10	2378.971	2386.56	RCP	0	0	2.19	5	1.85	OK
4454.00		327.74	288.1	2383.78	0.024	3.423	3.343	20.65	2387.123	2393.74	RCP	0	0	1.99	5	1.66	OK
4719.59		265.59	288.1	2388.89	0.019	3.344	3.246	21.35	2392.136	2399.21	RCP	0	0	2.09	5	1.75	OK
4860.42		140.83	288.1	2393.31	0.031	4.241	4.241	16.23	2397.551	2401.64	RCP	0	0	1.39	5	0.76	OK
4864.42		4.00	226.1	2394.31	0.250	3.461	3.399	19.87	2397.709	2403.84	RCP	0	0	1.90	4	0.60	OK
5267.87		403.45	226.1	2403.84	0.024	3.681	3.652	18.79	2407.492	2412.97	RCP	0	0	1.73	4	0.35	OK
5667.87		400.00	226.1	2412.70	0.022	3.906	3.904	18.11	2416.604	2421.70	RCP	0	0	1.62	4	0.10	OK
5671.87		4.00	73.9	2414.20	0.375	2.467	2.452	15.12	2416.652	2420.20	RCP	0	0	1.70	2.5	0.05	OK
5998.89		327.02	7.4	2422.58	0.026	4.887	4.887	15.05	2427.467	2430.98	RCP	0	0	1.20	2.5	0.00	OK
6002.89		4.00	23.4	2423.08	0.125	7.131	7.131	7.45	2430.211	2431.07	RCP	0	0	0.49	2	0.00	OK
6329.90		327.01	23.4	2429.66	0.020	4.050	4.050	7.45	2433.710	2434.57	RCP	0	0	0.65	2	0.00	OK

(1) DEPTH WITH AIR ENTRAINMENT

APPENDIX E

REFERENCE MATERIAL

MISSION-GREENWAY: AS-BUILT PLANS REFERENCE
(Paradise Hills No.18 - PENTACORE)
For culvert upstream of Patti Ann Woods

ABBREVIATIONS

AC	ASPHALTIC CONCRETE	MVC	MIDDLE OF VERTICAL CURVE
BC	BACK OF CURB	N	NORTH
BCR	BACK OF CURB RETURN	OC	ON CURVE
BFE	BASE FLOOD ELEVATION	PB	PULL BOX
BK	BACK STATION	PC	POINT OF CURVATURE
BVC	BEGIN VERTICAL CURVE	PI	POINT OF INTERSECTION
CL	CENTERLINE	PL	PROPERTY LINE
CLINT	CENTERLINE INTERSECTION	PVI	POINT OF VERTICAL INTERSECTION
DI	DROP INLET	PT	POINT OF TANGENCY
E	EAST	PZ	PRESSURE ZONE
EA	EACH	R/W	RIGHT OF WAY
ECR	END CURB RETURN	S	SOUTH OR SEWER
EVC	END VERTICAL CURVE	SD	STORM DRAIN
FC	FACE OF CURB	SDH	STORM DRAIN MANHOLE
FF	FINISH FLOOR	SF	SQUARE FEET
FG	FINISH GRADE	SS	SANITARY SEWER
FH	FIRE HYDRANT	SSMH	SANITARY SEWER MANHOLE
FL	FLOW LINE	STLT	STREET LIGHT
GA	GAUGE	SW	SIDE WALK
GB	GRADE BREAK	SY	SQUARE YARD
GV	GATE VALVE	TB	TOP OF BANK
HP	HIGH POINT	TC	TOP OF CURB
INV	INVERT	TWH	TOP OF MANHOLE
KNKL	KNUCKLE	W	WEST OR WATER
LF	LINEAR FEET	VC	VERTICAL CURVE
LP	LOW POINT	VG	VALLEY GUTTER
MH	MANHOLE		

CITY OF HENDERSON TRAFFIC NOTES

- ANY EXISTING TRAFFIC CONTROL DEVICES AND/OR SIGNS SHALL BE MAINTAINED DURING THE PERIOD OF CONSTRUCTION SHALL BE REPOSITIONED, AS REQUIRED, PER M.U.T.C.D. AND CITY STANDARDS, UPON COMPLETION OF THE PROJECT.
- DEVELOPERS/CONTRACTORS ARE RESPONSIBLE FOR SUBMITTING TRAFFIC CONTROL/BARRICADING PLANS NOT LESS THAN THREE (3) WORKING DAYS BEFORE BEGINNING OF CONSTRUCTION WITHIN THE PUBLIC RIGHT OF WAY, INCLUDING SIDEWALKS. BEFORE ANY WORK IS STARTED IN THE RIGHT OF WAY, THE CONTRACTOR WILL INSTALL ALL ADVANCE WARNING SIGNS FOR THE CONSTRUCTION ZONE. THE CONTRACTOR WILL INSTALL TEMPORARY GROUND MOUNTED STOP SIGNS AT ALL NEW STREET ENCROACHMENTS INTO EXISTING CITY STREET IMMEDIATELY AFTER FIRST GRADING WORK IS ACCOMPLISHED, AND WILL MAINTAIN SAID SIGNS UNTIL PERMANENT SIGNS ARE INSTALLED.
- LOCATION AND DESCRIPTION OF NEW AND EXISTING TRAFFIC CONTROL DEVICES, STREET STRIPING, MEDIAN ISLANDS, DRIVEWAYS AND TRAFFIC SIGNALS MUST BE SHOWN ON PLANS SUBMITTED TO THE CITY FOR APPROVAL. ALL NEW TRAFFIC SIGNS WILL BE FABRICATED WITH HIGH INTENSITY GRADE (CLASS 4) REFLECTIVE SHEETING. ALL NEW TRAFFIC SIGNS, EXCEPT STREET NAME SIGNS, WILL HAVE "T-CAL" OR 3M SERIES 1160 OR APPROVED EQUIVALENT ANTI-GRAFFITI PROTECTIVE FILM.
- LOCATION AND DESCRIPTION OF NEW AND EXISTING STREET NAME SIGNS MUST BE SHOWN ON PLANS SUBMITTED TO THE CITY FOR APPROVAL. STREET NAME SIGNS WILL COMPLY WITH CLARK COUNTY STANDARD DRAWINGS NO. 249, 250 AND 251. ALL STREET NAME SIGNS WILL BE FABRICATED WITH DIAMOND GRADE V.P. (CLASS 5) REFLECTIVE SHEETING. ALL INTERSECTIONS WITH 100' OR GREATER R/W ROADWAYS WILL HAVE THE CITY OF HENDERSON LOGO ON BOTH STREET NAME PANELS. CONTACT CITY OF HENDERSON TRAFFIC SHOP THREE (3) WORKING DAYS IN ADVANCE, MONDAY THROUGH THURSDAY, AT 565-2148 TO RECEIVE LOGO TO BE APPLIED BY THE CONTRACTOR TO THE STREET NAME PANELS PER CITY OF HENDERSON STANDARD DETAIL.
- BLUE REFLECTORIZED PAVEMENT MARKINGS MUST BE INSTALLED AND CURB MUST BE PAINTED AT EVERY FIRE HYDRANT LOCATION PER CITY OF HENDERSON FIRE DEPARTMENT STANDARDS.
- ALL CONSTRUCTION SIGNING, BARRICADING AND PAVEMENT MARKINGS WILL CONFORM TO THE NEVADA WORK ZONE TRAFFIC CONTROL HANDBOOK - 1986 AND TO THE M.U.T.C.D. LATEST EDITION WITH ANY ADDENDA AND REVISIONS.
- WHERE STREETS END AT THE PROJECT BOUNDARY, THREE (3) 18" DIAMOND (MINIMUM), REFLECTORIZED, RED PANELS SHALL BE INSTALLED AT THE END OF THE ROADWAY AND MAINTAINED UNTIL ADJOINING PROJECT IS BUILT.
- IF THE IMPROVEMENTS NECESSITATE THE OBLITERATION, TEMPORARY OBSTRUCTION, TEMPORARY REMOVAL, OR RELOCATION OF ANY EXISTING TRAFFIC PAVEMENT MARKING, SUCH PAVEMENT MARKING WILL BE RESTORED OR REPLACED WITH LIKE MATERIALS TO THE SATISFACTION OF THE CITY TRAFFIC ENGINEER.

FIRE DEPARTMENT GENERAL NOTES:

FIRE HYDRANTS:

- ALL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH THE UNIFORM FIRE CODE APPENDIX II-B, FIRE HYDRANT LOCATIONS AND DISTRIBUTIONS, AS AMENDED.
- FIRE HYDRANTS SHALL BE MAINTAINED IN AN OPERATIVE CONDITION AT ALL TIMES WITH THE REQUIRED WATER SUPPLY AND SHALL BE ACCEPTED BY PUBLIC WORKS DEPARTMENT.
- FIRE HYDRANT SHALL HAVE PERMANENT MARKINGS IDENTIFYING MANUFACTURER, SIZE OF THE MAIN VALVE OPENING, YEAR OF MANUFACTURE, MODEL NUMBER, DIRECTION OF OPENING AND BURY DEPTH. ALL HYDRANTS SHALL MEET THE REQUIREMENTS OF THE UNIFORM DESIGN AND CONSTRUCTION STANDARDS FOR WATER DISTRIBUTION SYSTEMS.
- ALL PUBLIC FIRE HYDRANTS SHALL HAVE A SIX DIGIT NUMBER (AS DESIGNATED BY PUBLIC WORKS) PAINTED ON THE BARRIL BY THE HYDRANT INSTALLER. THE NUMBER SHALL BE IN 1" HIGH BLOCK NUMBERS USING BLACK ENAMEL PAINT. ALL NUMBERS SHALL MATCH APPROVED PLANS.
- ALL FIRE DEPARTMENT CONNECTIONS (FDC) FOR FIRE SPRINKLER OR STANDPIPE SYSTEMS SHALL BE LOCATED WITHIN 100 FEET OF A FIRE HYDRANT. THE 100 FEET SHALL BE MEASURED BY AN APPROVED UNOBSTRUCTED ROUTE. THE FDC SHALL BE LOCATED IN AN APPROVED LOCATION ON THE STREET OR FIRE LANE SIDE OF THE BUILDING BEING PROTECTED.
- FIRE HYDRANTS SHALL BE IN CONFORMANCE WITH THE FIRE PREVENTION DIVISION'S UNIFORM GUIDELINE.
- PRIOR TO CLOSING ANY WATER SUPPLY CONTROL VALVE OR PLACING ANY FIRE HYDRANT OUT OF SERVICE, THE HENDERSON FIRE DEPARTMENT DISPATCH CENTER (565-1214) SHALL BE CONTACTED.
- ALL SECTIONAL CONTROL VALVES CONTROLLING WATER SUPPLIES ON PRIVATE FIRE SERVICE MAINS SHALL BE LISTED POST INDICATING VALVES (PIV).

UNDERGROUND PIPING & VALVES:

- APPROVAL OF THESE PLANS IS FOR THE CONSTRUCTION OF OFFSITE IMPROVEMENTS ONLY. ALL ONSITE IMPROVEMENTS, AS DEFINED BY CITY OF HENDERSON, INCLUDING BLOCK WALLS, MUST BE APPROVED BY THE BUILDING AND PLANNING DIVISIONS OF THE CITY OF HENDERSON.
- CONTRACTOR SHALL PROVIDE ALL NECESSARY HORIZONTAL AND VERTICAL TRANSITION BETWEEN NEW CONSTRUCTION AND EXISTING SURFACES TO PROVIDE FOR PROPER DRAINAGE AND OF INGRESS AND EGRESS TO SAID CONSTRUCTION. EXTENT OF TRANSITIONS TO BE DETERMINED BY THE CITY ENGINEER.
- EXISTING UTILITIES ARE LOCATED ON PLANS FOR THE CONVENIENCE OF THE CONTRACTOR ONLY. THE CONTRACTOR SHALL BEAR FULL RESPONSIBILITY FOR THE PROTECTION OF UTILITIES AND THE ENGINEER BEARS NO RESPONSIBILITY FOR UTILITIES NOT SHOWN ON THE PLANS OR NOT IN THE LOCATION SHOWN ON THE PLANS. THIS INCLUDES ALL SERVICE LATERALS OF ANY KIND.
- POWER POLES AND/OR OTHER EXISTING FACILITIES NOT IN PROPER LOCATION BASED ON PROPOSED IMPROVEMENTS SHOWN HEREON WILL BE RELOCATED AT NO EXPENSE TO THE CITY OF HENDERSON.
- WHEELCHAIR RAMPS SHALL BE CONSTRUCTED IN EACH QUADRANT OF AN INTERSECTION PER STANDARD DRAWING NO. 235. EXACT LOCATION OF RAMPS SHALL BE DETERMINED IN THE FIELD BY A CITY INSPECTOR, OR AS SHOWN ON PLAN.
- CURB AND GUTTER WITH A GRADE OF LESS THAN FIVE-TENTHS OF ONE PERCENT SHALL BE CONSTRUCTED BY FORMING. EACH JOINT SHALL BE CHECKED FOR GRADE PRIOR TO CONSTRUCTION AND WATER TESTED AS SOON AS POSSIBLE AFTER CONSTRUCTION.
- ALL GRADING SHALL CONFORM TO THE SOILS REPORT.

FIRE LANES:

- FIRE APPARATUS ACCESS ROADS AND FIRE HYDRANTS INSTALLED FOR FIRE PROTECTION SHALL BE INSTALLED AND MADE SERVICEABLE PRIOR TO AND DURING THE TIME OF CONSTRUCTION.
- ACCESS TO BUILDINGS FOR THE PURPOSE OF FIREFIGHTING SHALL BE PROVIDED. CONSTRUCTION MATERIAL SHALL NOT BLOCK FIRE LINES, ACCESS TO BUILDINGS, HYDRANTS OR FIRE APPLIANCES.
- FIRE LANES SHALL BE IN CONFORMANCE WITH THE FIRE PREVENTION DIVISION'S UNIFORM GUIDELINE.

GATES:

- SHOP DRAWINGS FOR ALL GATES AND OPENERS SHALL BE SUBMITTED SEPARATELY FOR REVIEW AND APPROVAL. OBTAIN A COPY OF THE UNIFORM GUIDELINE FOR DETAILS.
- UPDATED 06/23/00
SUPERSEDES 11/04/99

GENERAL NOTES

STANDARD GENERAL NOTES (REV. 3-99) (UPDATE 4-99)

- ALL CONSTRUCTION SHALL CONFORM TO THE UNIFORM STANDARD SPECIFICATIONS FOR PUBLIC WORKS STANDARD DRAWINGS FOR PUBLIC WORKS CONSTRUCTION, OFFSITE IMPROVEMENTS, CLARK COUNTY AREA, NEVADA, 1988.
- APPLICATION FOR INSPECTION BY THE CITY OF HENDERSON PUBLIC WORKS SHALL BE MADE BY THE CONTRACTOR AT LEAST 24 HOURS BEFORE THE INSPECTION SERVICES WILL BE REQUIRED, 616-3965.
- WORK IN PUBLIC STREETS, ONCE BEGUN, SHALL BE PROSECUTED TO COMPLETION WITHOUT DELAY SO AS TO PROVIDE MINIMUM INCONVENIENCE TO ADJACENT PROPERTY OWNERS AND TO THE TRAVELING PUBLIC.
- THE CONTRACTOR SHALL TAKE ALL NECESSARY AND PROPER PRECAUTIONS TO PROTECT ADJACENT PROPERTIES FROM ANY AND ALL DAMAGE THAT MAY OCCUR FROM STORM WATER RUNOFF AND/OR DEPOSITION OF DEBRIS RESULTING FROM ANY AND ALL WORK IN CONNECTION WITH SUBDIVISION CONSTRUCTION.
- PRIOR TO FINAL ACCEPTANCE, BOND RELEASES, AND A CERTIFICATE OF OCCUPANCY, A CERTIFIED LEGIBLE AS-BUILT DRAWING MUST BE SUBMITTED TO THE CITY OF HENDERSON. AS-BUILT MUST SHOW ALL CHANGES AND ACTUAL FIELD LOCATIONS IN THE ABSENCE OF CHANGES. A COPY OF APPROVED DRAWINGS WILL BE REQUIRED STATING "INSTALLED AS PER DRAWINGS" AND CERTIFIED AS SUCH BY THE DEVELOPER'S ENGINEER.
- APPROVAL OF THESE PLANS IS FOR THE CONSTRUCTION OF OFFSITE IMPROVEMENTS ONLY. ALL ONSITE IMPROVEMENTS, AS DEFINED BY CITY OF HENDERSON, INCLUDING BLOCK WALLS, MUST BE APPROVED BY THE BUILDING AND PLANNING DIVISIONS OF THE CITY OF HENDERSON.
- CONTRACTOR SHALL PROVIDE ALL NECESSARY HORIZONTAL AND VERTICAL TRANSITION BETWEEN NEW CONSTRUCTION AND EXISTING SURFACES TO PROVIDE FOR PROPER DRAINAGE AND OF INGRESS AND EGRESS TO SAID CONSTRUCTION. EXTENT OF TRANSITIONS TO BE DETERMINED BY THE CITY ENGINEER.
- EXISTING UTILITIES ARE LOCATED ON PLANS FOR THE CONVENIENCE OF THE CONTRACTOR ONLY. THE CONTRACTOR SHALL BEAR FULL RESPONSIBILITY FOR THE PROTECTION OF UTILITIES AND THE ENGINEER BEARS NO RESPONSIBILITY FOR UTILITIES NOT SHOWN ON THE PLANS OR NOT IN THE LOCATION SHOWN ON THE PLANS. THIS INCLUDES ALL SERVICE LATERALS OF ANY KIND.
- POWER POLES AND/OR OTHER EXISTING FACILITIES NOT IN PROPER LOCATION BASED ON PROPOSED IMPROVEMENTS SHOWN HEREON WILL BE RELOCATED AT NO EXPENSE TO THE CITY OF HENDERSON.
- WHEELCHAIR RAMPS SHALL BE CONSTRUCTED IN EACH QUADRANT OF AN INTERSECTION PER STANDARD DRAWING NO. 235. EXACT LOCATION OF RAMPS SHALL BE DETERMINED IN THE FIELD BY A CITY INSPECTOR, OR AS SHOWN ON PLAN.
- CURB AND GUTTER WITH A GRADE OF LESS THAN FIVE-TENTHS OF ONE PERCENT SHALL BE CONSTRUCTED BY FORMING. EACH JOINT SHALL BE CHECKED FOR GRADE PRIOR TO CONSTRUCTION AND WATER TESTED AS SOON AS POSSIBLE AFTER CONSTRUCTION.
- ALL GRADING SHALL CONFORM TO THE SOILS REPORT.
- ENGINEER: CONVERSE CONSULTANTS SOUTHWEST, INC.
DATE: JULY 19, 1999
JOB NUMBER: CCSW PROJECT NO. 94-3368-01
- EARTHWORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PRELIMINARY GEOTECHNICAL REPORT.
- ALL STREET STRUCTURAL SECTIONS SHALL BE PER THE RECOMMENDATIONS OF THE SOILS ENGINEER. BASED ON CURB OR R-VALUES, NO PAVING OR BASE WORK SHALL COMMENCE UNTIL A STREET STRUCTURAL SECTION IS APPROVED BY THE CITY ENGINEER, CITY OF HENDERSON.
- BEFORE ANY WORK IS STARTED IN THE RIGHT-OF-WAY, THE CONTRACTOR SHALL INSTALL ALL ADVANCE WARNING SIGNS FOR THE CONSTRUCTION ZONE. THE CONTRACTOR SHALL INSTALL TEMPORARY STOP SIGNS AT ALL NEW STREET ENCROACHMENTS INTO EXISTING PUBLIC STREETS IMMEDIATELY AFTER THE FIRST GRADING WORK IS ACCOMPLISHED AND SHALL MAINTAIN SAID SIGNS UNTIL PERMANENT SIGNS ARE INSTALLED. ALL CONSTRUCTION SIGNING, BARRICADING, AND PAVEMENT MARKINGS SHALL CONFORM TO THE "NEVADA TRAFFIC CONTROL MANUAL" - CURRENT EDITION AND TO THE "MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES" - CURRENT EDITION AND BE APPROVED BY THE CITY OF HENDERSON BEFORE CONSTRUCTION BEGINS.
- WHERE EXISTING PAVEMENT IS CUT TO INSTALL UTILITY SERVICE LINES, BACKFILL AND PAVEMENT REPLACEMENT SHALL BE DONE PER STANDARD DRAWING 5502 AND SECTION 206, 207, AND 208 OF THE STANDARD SPECIFICATION ISSUE, 1986.
- ALL STATIONING IS REFERENCED TO CENTERLINE.
- EXACT LOCATION OF ALL SAWCUT LINES SHALL BE DETERMINED IN THE FIELD BY A CITY OF HENDERSON INSPECTOR.
- PROTECTION AND REPLACEMENT OF SURVEY MONUMENTS OR PROPERTY STAKES NOT DELINEATED ON THE CONTRACT DRAWINGS SHALL BE THE CONTRACTOR'S RESPONSIBILITY. REPLACEMENT OF SURVEY MONUMENTS OR PROPERTY STAKES SHALL BE DONE TO THE COH SURVEY SECTION'S SATISFACTION.
- AFFECTED UTILITY COMPANIES SHALL BE NOTIFIED AT LEAST TWO (2) WORKING DAYS PRIOR TO COMMENCEMENT OF CONSTRUCTION.
- CALL BEFORE YOU DIG, 1-800-227-2600.
- MODIFICATIONS TO EXISTING UTILITIES SHALL CONFORM TO THE OWNER'S UTILITY STANDARDS AND SPECIFICATIONS.
- THE CONTRACTOR SHALL TAKE REASONABLE MEASURES TO PROTECT EXISTING IMPROVEMENTS FROM DAMAGE AND ALL SUCH IMPROVEMENTS DAMAGED BY THE CONTRACTOR'S OPERATION SHALL BE REPAIRED OR RECONSTRUCTED TO THE ENGINEER'S SATISFACTION AT THE EXPENSE OF THE CONTRACTOR.
- CITY APPROVAL OF THE IMPROVEMENT PLANS IS GRANTED FOR ONE (1) YEAR ONLY. PLANS MUST BE RESUBMITTED FOR REVIEW AND APPROVAL TO THE DEPARTMENT OF PUBLIC WORKS, CITY OF HENDERSON, IF WORK IS NOT COMPLETED BY 20.
- ALL OFFSITE AND ONSITE WATER AND SEWER FACILITIES UP TO WITHIN 5 FEET OF BUILDINGS SHALL BE CONSTRUCTED TO PUBLIC WORKS STANDARDS.
- IF SEWER OR WATER LINES WITHIN THE PUBLIC UTILITY EASEMENTS REQUIRE REPAIRS, ALL SUCH REPAIRS WILL BE DONE IN ACCORDANCE WITH PUBLIC WORKS DEPARTMENT STANDARDS. CURBS AND GUTTERS AND SPECIAL PAVING REPAIRS SHALL BE THE RESPONSIBILITY OF THE HOMEOWNER'S ASSOCIATION.
- IF SIGNS ARE PRESENT ON THIS CONSTRUCTION SITE, PLEASE CONTACT THE SIGN COMPANY LISTED ON THE SIGN 24 HOURS PRIOR TO COMMENCING CONSTRUCTION IN THE SIGN'S LOCATION. CITY OWNED AND CITY SPONSORED SIGNS (KIOSKS) SHALL BE REMOVED AND REPLACED FOLLOWING CONSTRUCTION IN THEIR ORIGINAL LOCATION IN LIKE-NEW CONDITION AT CONSTRUCTION CONTRACTOR'S EXPENSE. ANY CONTRACTOR HAVING TO REMOVE A SIGN WHICH WAS DAMAGED PRIOR TO THE CONTRACTOR OCCUPANCY THE SIGN SHALL ARRANGE FOR VERIFICATION OF THE SIGN'S CONDITION BY A CITY INSPECTOR PRIOR TO REMOVAL. ALL SIGNS NOT PREVIOUSLY VERIFIED BY A CITY INSPECTOR SHALL BE ASSUMED TO BE IN LIKE-NEW CONDITION PRIOR TO REMOVAL.

ESTIMATE OF QUANTITIES

ESTIMATE OF QUANTITIES FOR PERMITTING PURPOSES ONLY.

NO.	DESCRIPTION	UNIT
1	2" Asphalt Paving	14,109 sy
2	3" Asphalt Paving	0 sy
3	4" Asphalt Paving	4,586 sy
4	5" Asphalt Paving	7,178 sy
5	Type I and/or Type II Base	8,531 cy
6	3/4" Open Grade	7,178 sy
7	Excavation & Embankments in row	10,442 cy
8	A Curb, Drainage Curb, L Type C&G	11,303 lf
9	Driveway	9,000 sf
10	Concrete Valley Gutter	1,738 sf
11	Conc. Sidewalk & Med. Island	33,718 sf
12	Service Point for Lights	1 ea
13	Light Standard (single lum.)	23 ea
14	Light Standard (double lum.)	11 ea
15	4" pvc Sewer Lateral	4,621 lf
16	8" pvc Sewer	6,192 lf
17	12" pvc Sewer	0 lf
18	Sewer Manhole Adjustment	0 lf
19	Sewer Manhole under 6'	0 ea
20	Sewer Manhole over 6'	21 ea
21	Sewer Back Water Valves	40 ea
22	Water Services to lot (3/4" meter)	90 ea
23	6" pvc Water	572 lf
24	8" pvc Water	4,870 lf
25	12" pvc Water	0 lf
26	18" pvc Water	0 lf
27	Fire Hydrant	9 ea
28	Utility Trench (st. light conduit)	5,025 lf
29	Street & Stop Signs	57 ea
30	Survey Monuments	11 ea
31	Storm Drain Junction Structure	1 ea
32	60" Diameter Storm Drain Manhole	11 lf
33	66" rcp storm drain	318 lf
34	60" rcp storm drain	740 lf
35	48" rcp storm drain	874 lf
36	36" rcp storm drain	80 lf
37	30" rcp storm drain	370 lf
38	24" rcp storm drain	441 lf
39	6" nuisance storm drain	331 lf
40	16" modified type 'C' drop inlet	1 ea
41	14.5" modified type 'C' drop inlet	1 ea
42	12" type 'C' drop inlet	1 ea
43	6" type 'C' drop inlet	1 ea
44	4" type 'C' drop inlet	1 ea
45	Pressure Reducing Valves	77 ea

NOTE TO CONTRACTOR:
QUANTITIES SHOWN ARE APPROXIMATIONS ONLY AND ARE INTENDED TO ILLUSTRATE SCOPE OF WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING THE EXACT QUANTITIES INVOLVED.

CITY APPROVAL OF THE IMPROVEMENT PLANS IS GRANTED FOR ONE (1) YEAR ONLY. PLANS MUST BE RESUBMITTED FOR REVIEW & APPROVAL TO THE DEPARTMENT OF PUBLIC WORKS, CITY OF HENDERSON IF WORK IS NOT COMPLETED BY: July 20 2002

APPROVED BY:

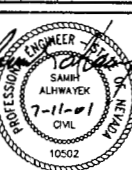
Ken Y. Koshiro
KEN Y. KOSHIRO, P.E.,
NEW DEVELOPMENT ENGINEER, C.O.H.
DATE: 7-20-01

PENTACORE

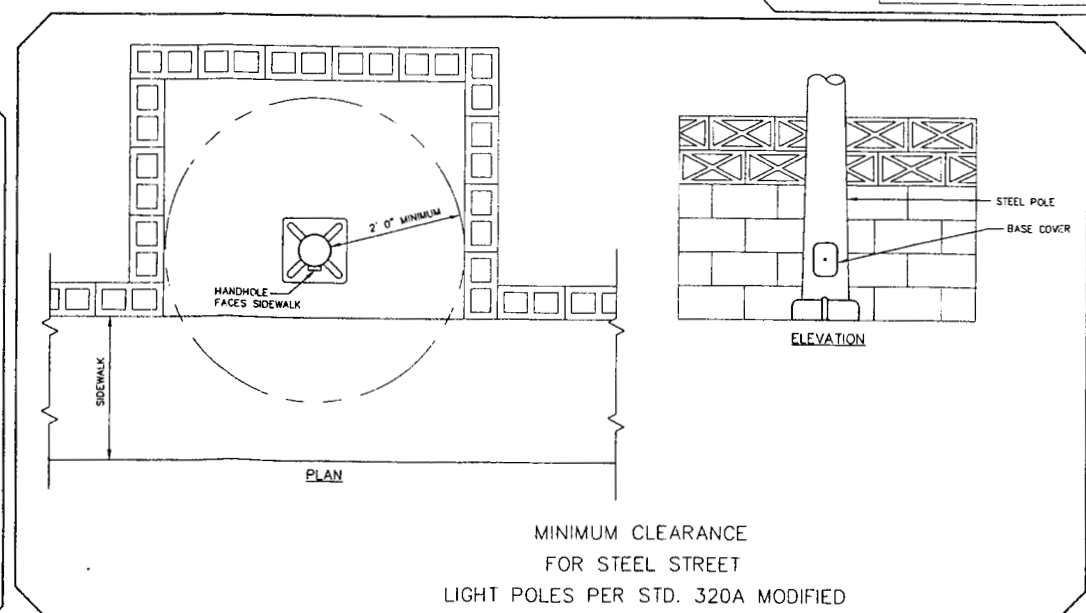
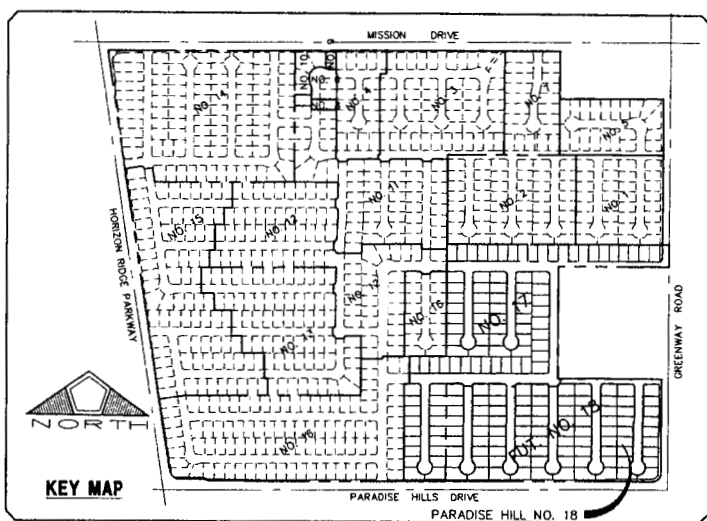
CIVIL ENGINEERING, LAND SURVEYING, PLANNING
CONSTRUCTION MANAGEMENT, CONSULTING
6763 WEST CHARLESTON BOULEVARD
LAS VEGAS, NEVADA 89146 (702)258-0115



KBHOME
PARADISE HILLS NO. 18
GENERAL NOTES & QUANTITIES



SHEET
2
OF 26



MINIMUM CLEARANCE
FOR STEEL STREET
LIGHT POLES PER STD. 320A MODIFIED

05848

EXISTING PARADISE HILLS NO. 16

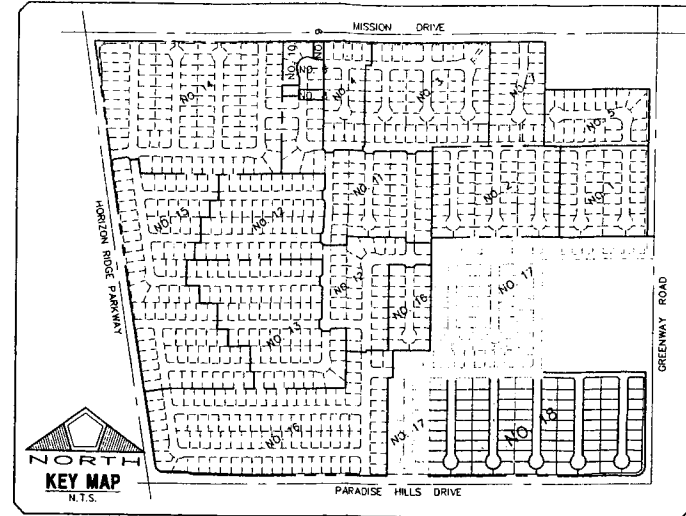
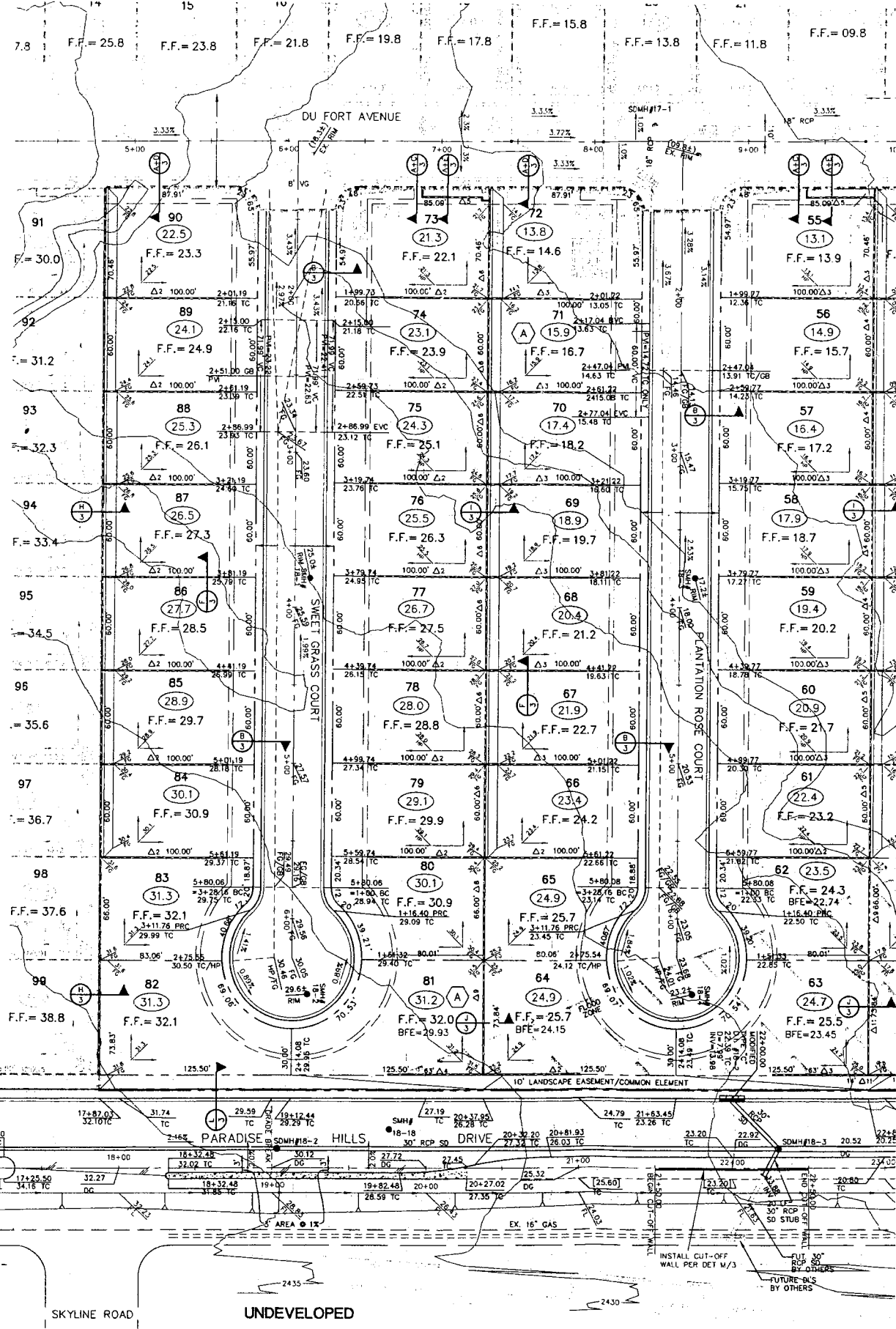
CO.H. PLAN #05898

EXISTING PARADISE HILLS NO. 17

CO.H. PLAN #05800

EXISTING PARADISE HILLS NO. 17

CO.H. PLAN #05800



SOLID GROUTING NOTE

SOLID GROUT FIRST 3 COURSES WHERE FF IS LESS THAN 1.5' HIGHER THAN ADJACENT TC.

Avoid hitting overhead power lines. It's costly.
Call before you do Overhead
1-702-593-6111

Avoid cutting underground.
Call before you Dig.
1-800-227-2600
UNDERGROUND SERVICE ALERT (USA)



BENCHMARK

CITY OF HENDERSON BM# 101, BRASS CAP IN THE TOP OF CURB ON THE NORTHEAST CORNER OF GREENWAY ROAD AND HEATHER STREET.
PROJECT DATUM = 2274.99
ELEVATION 2272.55 FEET NGVD 29 (DATUM USED)
ELEVATION 693.418 METERS NAVD 88.
ADD 2.44' TO NGVD 29 DATUM = NAVD 88

NOTE:
ALL PERIMETER WALLS ARE TO BE 6' IN HEIGHT WITH ADDITIONAL RETAINING AS SHOWN ON PLANS.

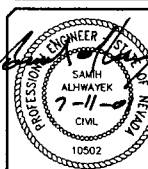
RETAINING WALL CONVERSION TABLE	
Δ1	0.67'
Δ2	1.33'
Δ3	2.00'
Δ4	2.67'
Δ5	3.33'
Δ6	4.00'
Δ7	4.67'
Δ8	5.33'
Δ9	6.00'
Δ10	6.67'
Δ11	7.33'

I CERTIFY THAT THIS GRADING PLAN CONFORMS TO THE APPROVED DRAINAGE STUDY FOR THIS SITE ON FILE AT THE CITY OF HENDERSON. PERM NO. 200100598
SAMIR ALHWAYEK, P.E. NO. 10502
DATE: 7-11-09
05848

PENTACORE
CIVIL ENGINEERING • LAND SURVEYING • PLANNING
CONSULTING
6703 WEST CHARLESTON BOULEVARD
LAS VEGAS, NEVADA 89146 (702)258-0115



KBHOME
PARADISE HILLS NO. 18
GRADING PLAN I



SHEET
5
OF 26

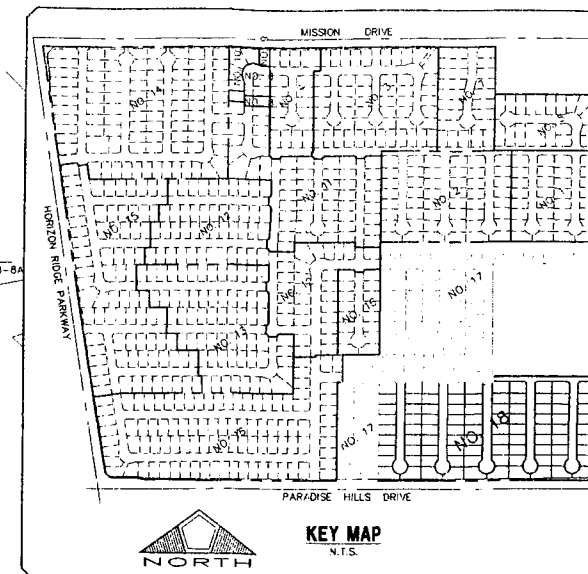
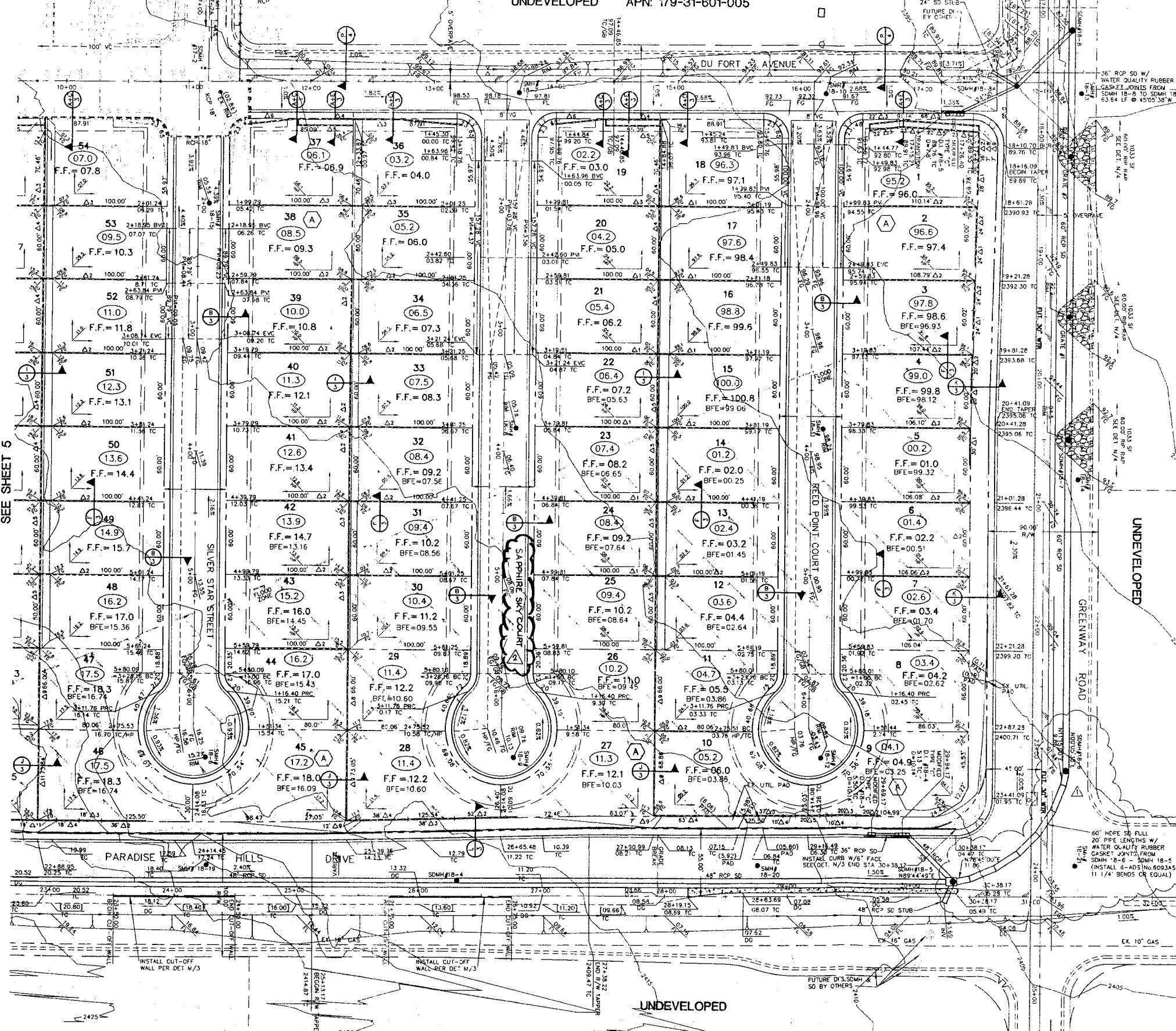
EXISTING PARADISE HILLS NO. 17

COH. PLAN #05800

09.8 F.F. = 05.9

UNDEVELOPED APN: 179-31-601-005

FOR ACCESS ROAD GRADING
SEE SHEET 13



SOLID GROUTING NOTE

SOLID GROUT FIRST 3 COURSES WHERE FF IS LESS THAN 1.5' HIGHER THAN ADJACENT TC.

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1-800-227-2600
(UNDERGROUND SERVICE ALERT (USA))



BENCHMARK

CITY OF HENDERSON BM# 101 BRASS CAP IN THE TOP OF CURB ON THE NORTHEAST CORNER OF GREENWAY ROAD AND HEATHER STREET.
PROJECT DATUM = 2274.99
ELEVATION 2272.55 FEET NGVD 29 (DATUM USED)
ELEVATION 693.418 METERS NAVD 88
ADD 2.44' TO NGVD 29 DATUM = NAVD 88

NOTE:
ALL PERIMETER WALLS ARE TO BE 6' IN HEIGHT WITH ADDITIONAL RETAINING AS SHOWN ON PLANS.

RETAINING WALL CONVERSION TABLE	
Δ1	0.67
Δ2	1.33
Δ3	2.00
Δ4	2.67
Δ5	3.33
Δ6	4.00
Δ7	4.67
Δ8	5.33
Δ9	6.00
Δ10	6.67

I CERTIFY THAT THIS GRADING PLAN CONFORMS TO THE APPROVED DRAINAGE STUDY FOR THIS SITE ON FILE AT THE CITY OF HENDERSON. PERMIT NO. 2010C00596
SAMIH ALHWAYEK, P.E. NO. 10562
DATE: 06-01

DATE	BY	DESCRIPTION
11-11-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME

DATE	BY	DESCRIPTION
11-11-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME
08-17-01	SA	CHANGED STREET NAME

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LAS VEGAS, NEVADA 89146 (702) 258-0115

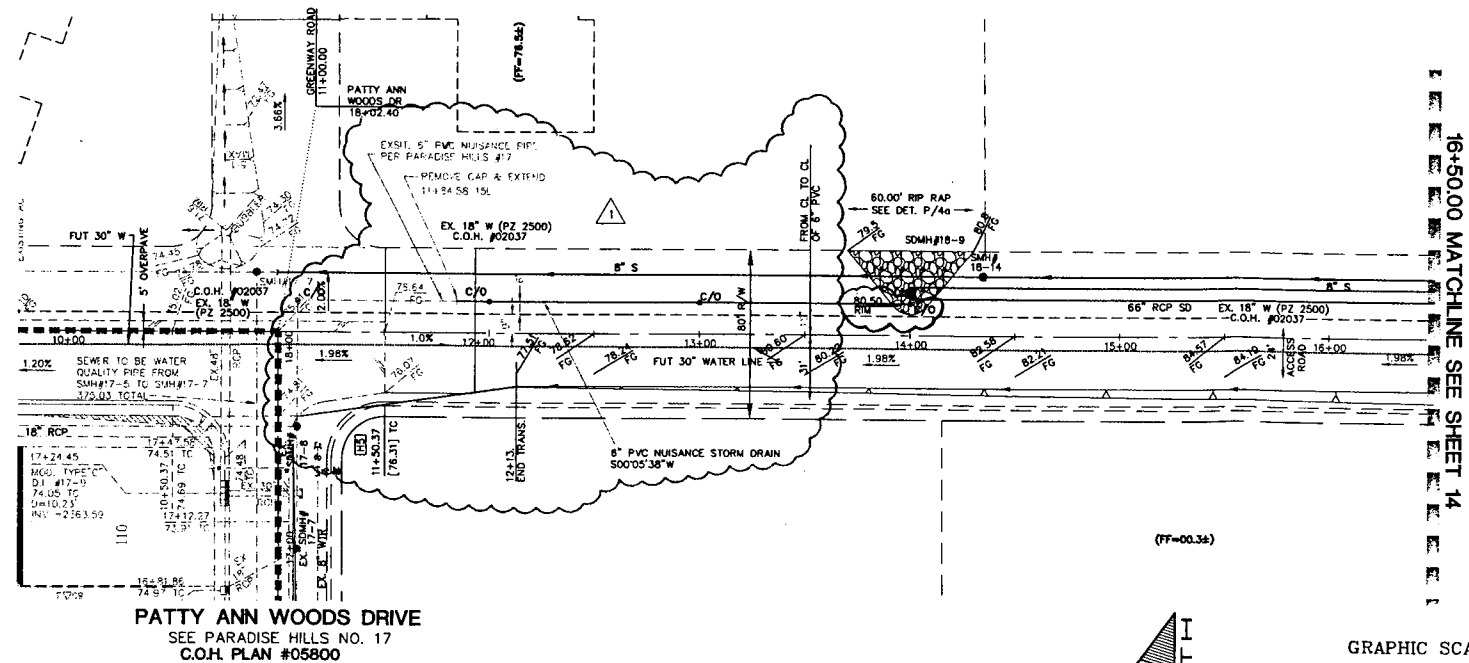
KBHOME
PARADISE HILLS NO. 18
GRADING PLAN II

PROFESSIONAL ENGINEER
SAMIH ALHWAYEK
06-01
10562

05848

EXISTING PARADISE HILLS NO. 1

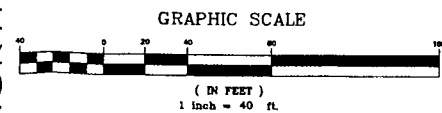
C.O.H. PLAN #04244



PATTY ANN WOODS DRIVE
SEE PARADISE HILLS NO. 17
C.O.H. PLAN #05800

GREENWAY ROAD PLAN

SCALE: 1" = 40'

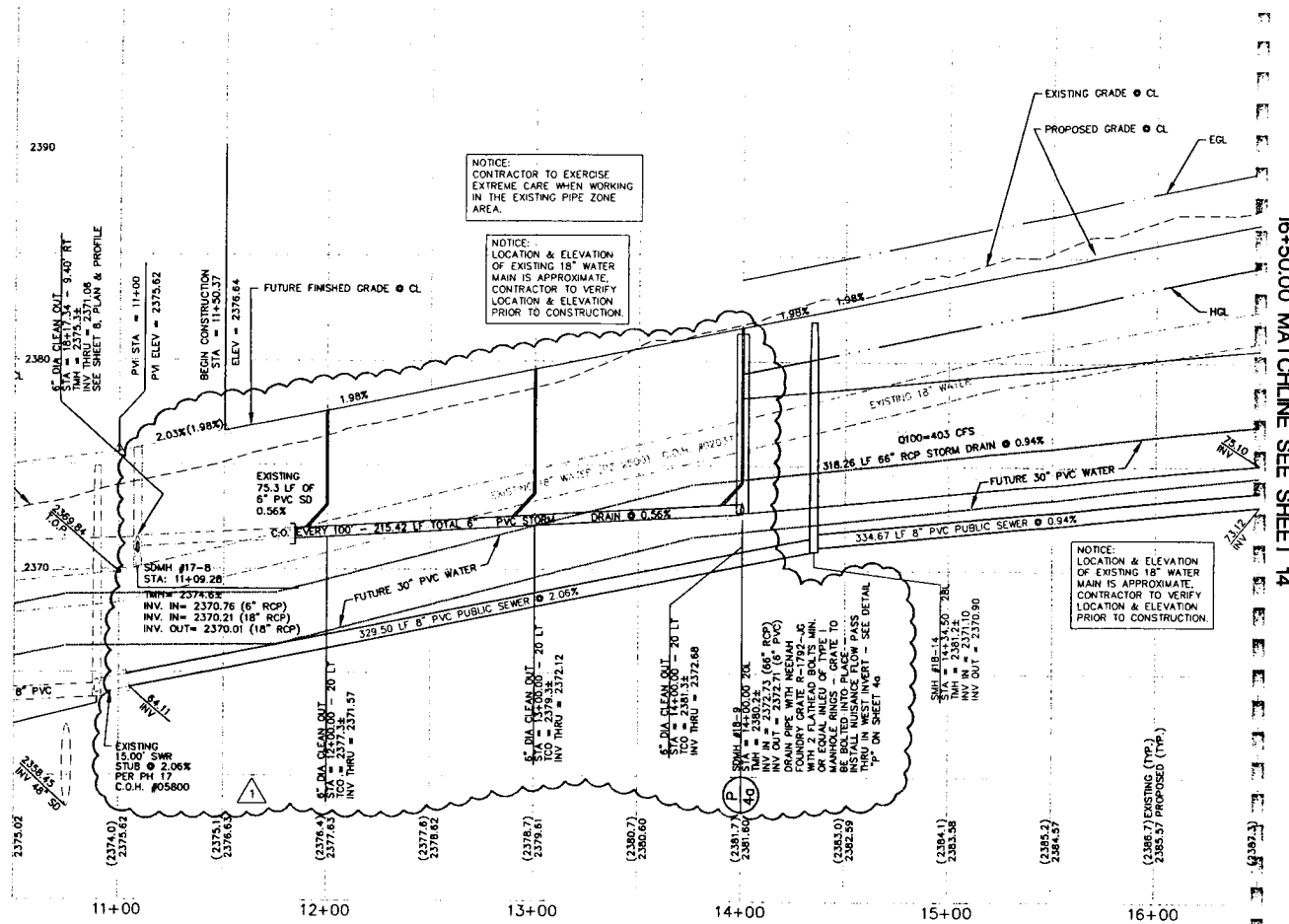


RAMP NO.	GRADE (%) "B" TO "A"	"A" (FT) MIN.	"B" (FT) MIN.
H1	-6 TO -5.01	4.5	21.5
H2	-5 TO -4.01	4.5	13.0
H3	-4 TO -3.01	4.5	12.0
H4	-3 TO -2.01	4.5	9.5
H5	-2 TO 2	8.0	8.0
H6	2.01 TO 3	9.5	4.5
H7	3.01 TO 4	12.0	4.5
H8	4.01 TO 5	15.0	4.5
H9	5.01 TO 6	21.5	4.5

SEE CLARK COUNTY AREA STANDARD
DRAWING NO. 235 CASE III

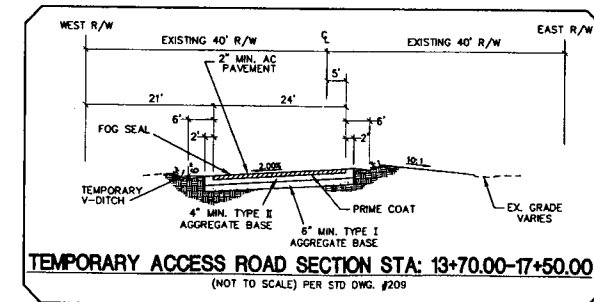
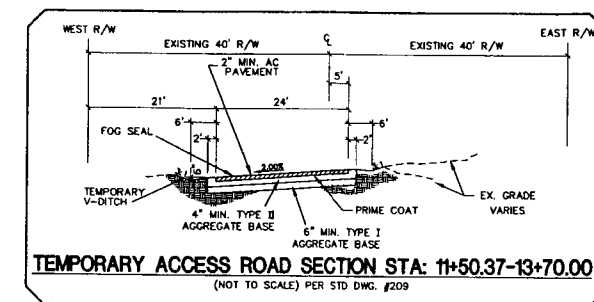
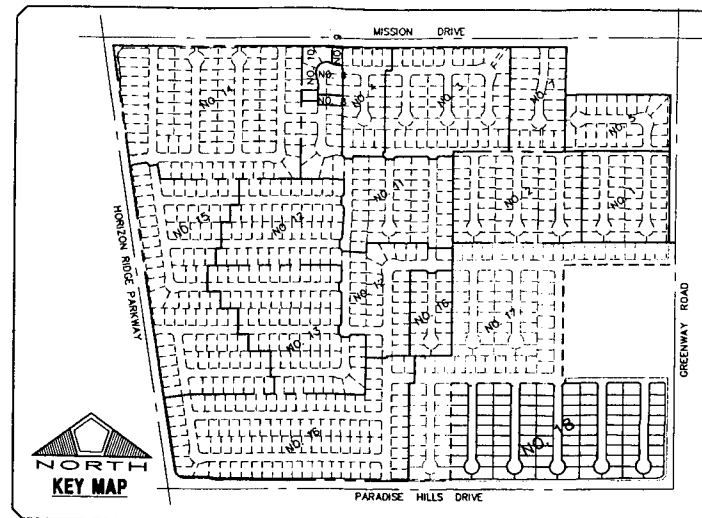
EXISTING PARADISE HILLS NO. 1

C.O.H. PLAN #04244



GREENWAY ROAD PROFILE

SCALE: HORIZ. 1" = 40'
VERT. 1" = 4'



CONSTRUCTION NOTES

1. CONSTRUCT SIDEWALK PER USD No. 234
2. CONSTRUCT TYPE "L" CURB & GUTTER PER USD No. 216
3. CONSTRUCT VALLEY GUTTER PER STANDARD DWG NO. 228
4. CONSTRUCT HANDICAP RAMP PER STANDARD DWG NO. 235 CASE III - SEE SW RAMP TRANSITION TABLE
5. CONSTRUCT MEDIAN ISLAND PER STANDARD DWG NO. 218

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UNDERGROUND SERVICE ALERT (USA)

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1-702-593-6111

BENCHMARK

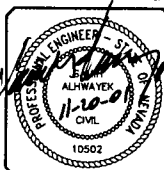
CITY OF HENDERSON BM# 101, BRASS CAP IN THE TOP OF CURB ON THE NORTHEAST CORNER OF GREENWAY ROAD AND HEATHER STREET.
PROJECT DATUM = 2274.99
ELEVATION 2272.55 FEET NGVD 29 (DATUM USED)
ELEVATION 693.418 METERS NAVD 88
ADD 2.44' TO NGVD 29 DATUM = NAVD 88

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BY: July 20 2002
APPROVED BY: Robert Malina
NEW DEVELOPMENT ENGINEER, C.O.H.
DATE: 11-27-01 (9-12-01)

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LAS VEGAS, NEVADA 89146 (702) 258-0115



KBHOME
PARADISE HILLS NO. 18
GREENWAY ROAD
PLAN & PROFILE I
STA: 11+50.37 TO 16+50.00



SHEET
13 Rev 1
OF 26

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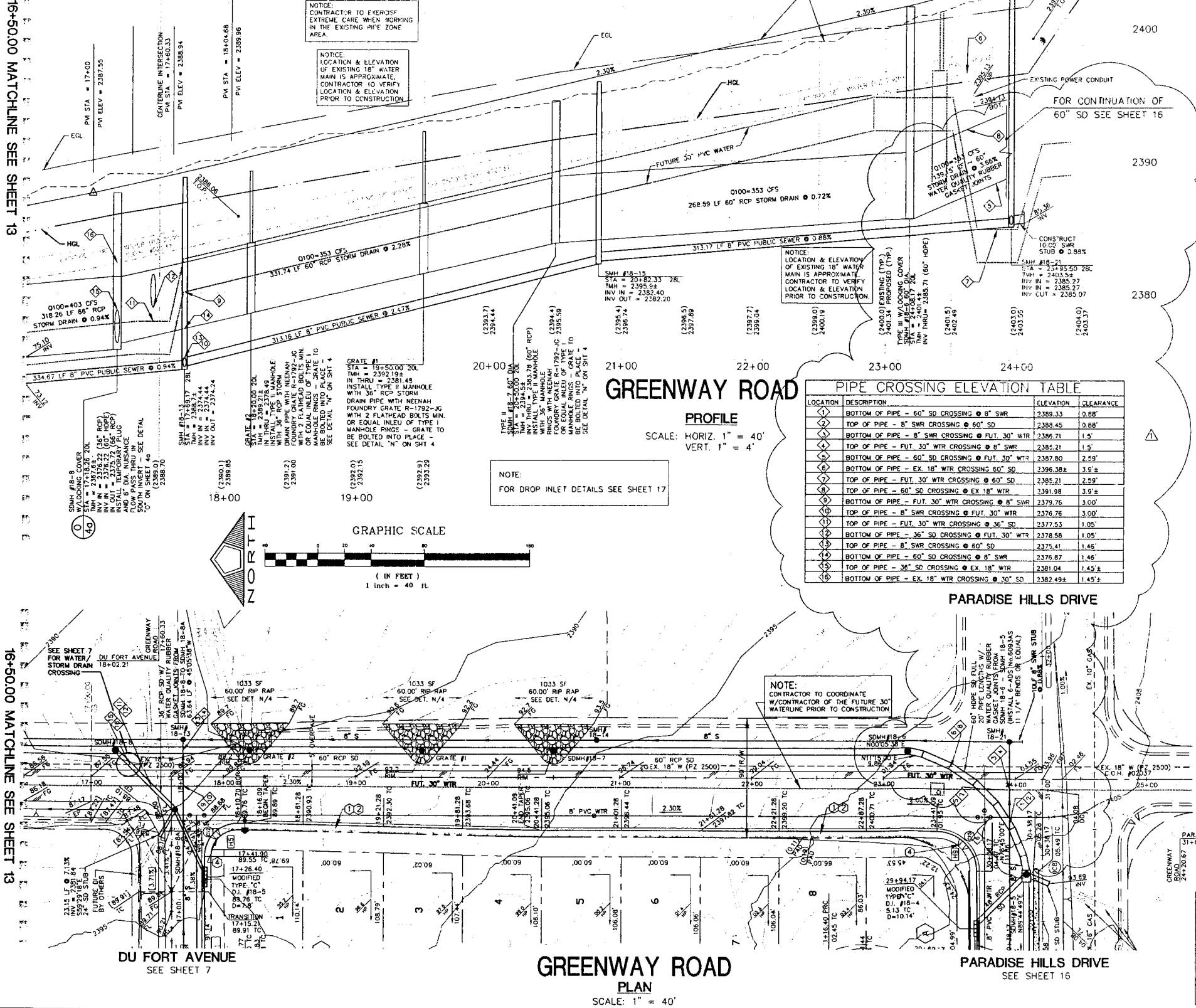
Unit 18 Curve Table

No.	Radius	Delta	Length	Tangent
100	20.00	89.42	31.51	44.58
101	20.00	89.42	31.51	44.58
102	20.00	89.42	31.51	44.58
103	20.00	89.42	31.51	44.58
104	20.00	89.42	31.51	44.58
105	20.00	89.42	31.51	44.58
106	20.00	89.42	31.51	44.58
107	20.00	89.42	31.51	44.58
108	20.00	89.42	31.51	44.58
109	20.00	89.42	31.51	44.58
110	20.00	89.42	31.51	44.58
111	20.00	89.42	31.51	44.58
112	20.00	89.42	31.51	44.58
113	20.00	89.42	31.51	44.58
114	20.00	89.42	31.51	44.58
115	20.00	89.42	31.51	44.58
116	20.00	89.42	31.51	44.58
117	20.00	89.42	31.51	44.58
118	20.00	89.42	31.51	44.58
119	20.00	89.42	31.51	44.58
120	20.00	89.42	31.51	44.58

NOTICE: CONTRACTOR TO EXERCISE EXTREME CARE WHEN WORKING IN THE EXISTING PIPE ZONE AREA.

NOTICE: LOCATION & ELEVATION OF EXISTING 18" WATER MAIN IS APPROXIMATE. CONTRACTOR TO VERIFY LOCATION & ELEVATION PRIOR TO CONSTRUCTION.

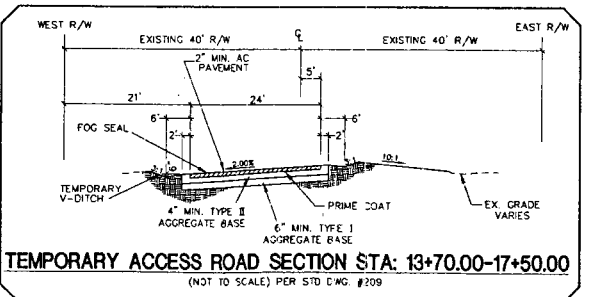
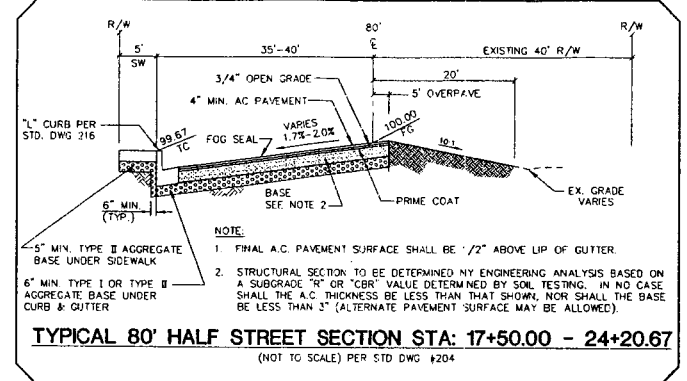
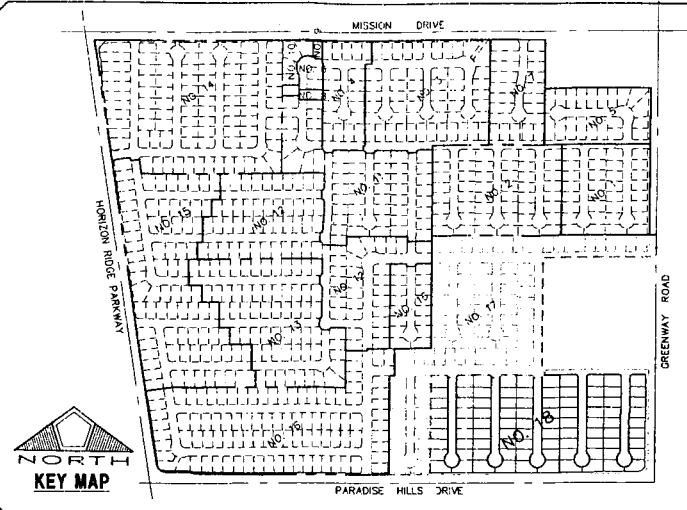
NOTICE: CONTRACTOR TO EXERCISE EXTREME CARE WHEN WORKING IN THE EXISTING PIPE ZONE AREA.



GREENWAY ROAD PROFILE

SCALE: HORIZ. 1" = 40'
VERT. 1" = 4'

LOCATION	DESCRIPTION	ELEVATION	CLEARANCE
1	BOTTOM OF PIPE - 60" SD CROSSING @ 8" SWR	2389.33	0.88'
2	TOP OF PIPE - 8" SWR CROSSING @ 60" SD	2388.45	0.88'
3	BOTTOM OF PIPE - 8" SWR CROSSING @ FUT. 30" WTR	2386.71	1.5'
4	TOP OF PIPE - FUT. 30" WTR CROSSING @ 8" SWR	2385.21	1.5'
5	BOTTOM OF PIPE - 60" SD CROSSING @ FUT. 30" WTR	2387.80	2.59'
6	TOP OF PIPE - EX. 18" WTR CROSSING @ 60" SD	2385.21	2.59'
7	TOP OF PIPE - FUT. 30" WTR CROSSING @ 60" SD	2385.21	2.59'
8	TOP OF PIPE - 60" SD CROSSING @ EX. 18" WTR	2381.99	3.9'
9	BOTTOM OF PIPE - FUT. 30" WTR CROSSING @ 8" SWR	2379.76	3.00'
10	TOP OF PIPE - 8" SWR CROSSING @ FUT. 30" WTR	2376.76	3.00'
11	TOP OF PIPE - FUT. 30" WTR CROSSING @ 36" SD	2377.53	1.05'
12	BOTTOM OF PIPE - 36" SD CROSSING @ FUT. 30" WTR	2378.58	1.05'
13	TOP OF PIPE - 8" SWR CROSSING @ 60" SD	2375.41	1.46'
14	BOTTOM OF PIPE - 60" SD CROSSING @ 8" SWR	2376.87	1.46'
15	TOP OF PIPE - 36" SD CROSSING @ EX. 18" WTR	2381.04	1.45'
16	BOTTOM OF PIPE - EX. 18" WTR CROSSING @ 30" SD	2382.48	1.45'



RAMP NO.	GRADE (%)	"B" TO "A"	"A" (FT) MIN.	"B" (FT) MIN.
H1	-6 TO -5.01	4.5	21.5	
H2	-5 TO -4.01	4.5	5.0	
H3	-4 TO -3.01	4.5	2.0	
H4	-3 TO -2.01	4.5	9.5	
H5	-2 TO 2	8.0	8.0	
H6	2.01 TO 3	5.5	4.5	
H7	3.01 TO 4	12.0	4.5	
H8	4.01 TO 5	15.0	4.5	
H9	5.01 TO 6	21.5	4.5	

BENCHMARK
CITY OF HENDERSON BM 101, BRASS CAP IN THE TOP OF CURB ON THE NORTHEAST CORNER OF GREENWAY ROAD AND HEATHER STREET.
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APPROVED BY: *Allen Medina*
KEN Y. KOSHIO, P.E.,
NEW DEVELOPMENT ENGINEER, C.O.H.
DATE: 8-9-01
05848

- CONSTRUCTION NOTES
- CONSTRUCT SIDEWALK PER USD No. 234
 - CONSTRUCT TYPE "L" CURB & GUTTER PER USD No. 216
 - CONSTRUCT VALLEY GUTTER PER STANDARD DWG NO. 228
 - CONSTRUCT HANDICAP RAMP PER STANDARD DWG NO. 235 CASE III - SEE SW RAMP TRANSITION TABLE
 - CONSTRUCT MEDIAN ISLAND PER STANDARD DWG NO. 218

DATE: 8/9/01
DRAWN BY: JKM
CHECKED BY: JKM
DESIGNED BY: JKM
JOB NO.: 000000000
SCALE: 1" = 40'

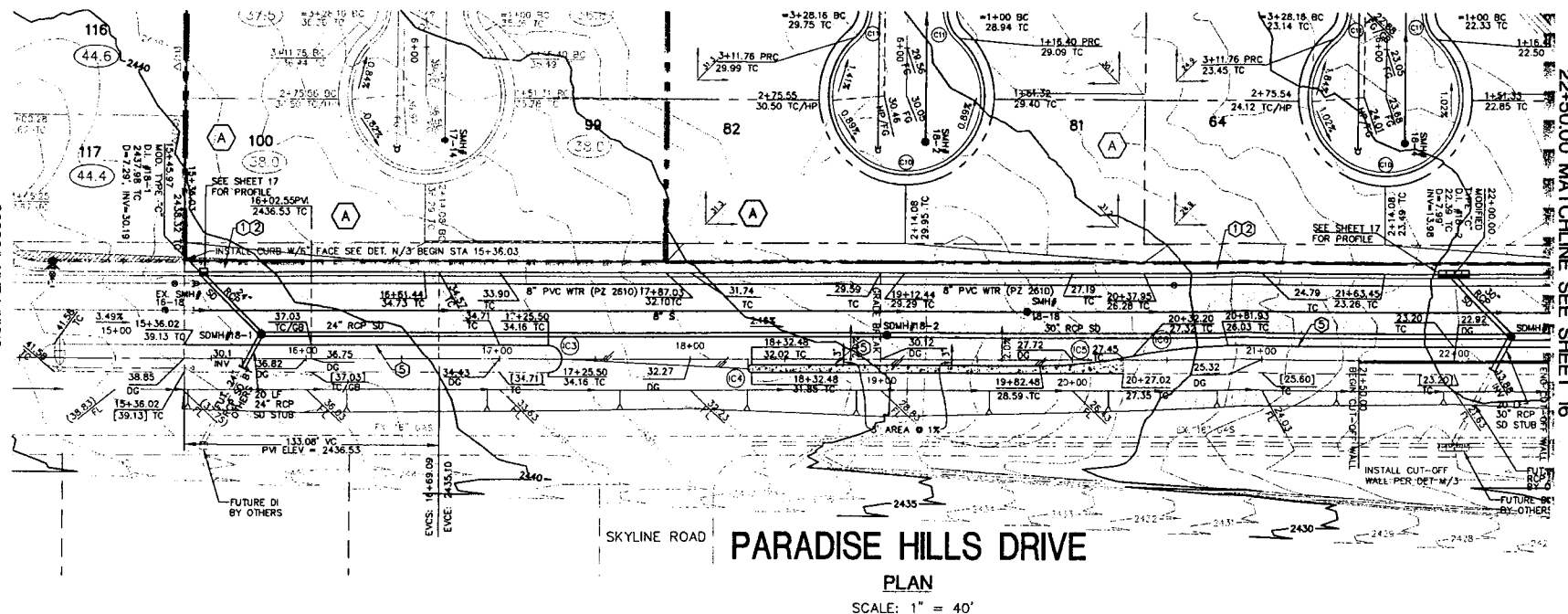
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CONSULTING
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LAS VEGAS, NEVADA 89146 (702)258-0115

KBHOME
PARADISE HILLS NO. 18
GREENWAY ROAD
PLAN & PROFILE II
STA: 16+50.00 TO 24+20.67

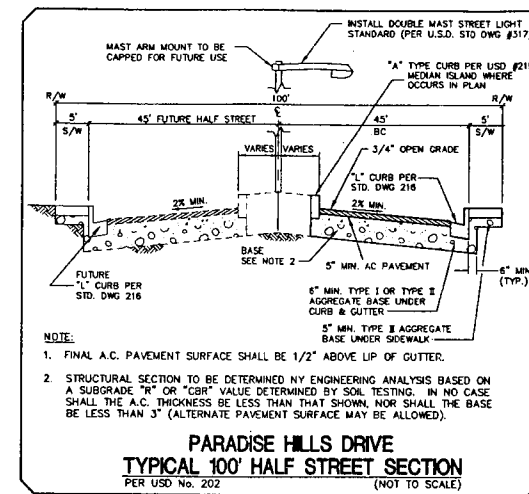
14REV 1
OF 26

C.O.H. PLAN #05696

C.O.H. PLAN #05896



ZZ+30.00 MAIL CHINE SEE SHEET 10



RAMP NO.	GRADE "B" TO "A" (%)	"A" (FT) MIN.	"B" (FT) MIN.
H1	-6 TO -5.01	4.5	21.5
H2	-5 TO -4.01	4.5	15.0
H3	-4 TO -3.01	4.5	12.0
H4	-3 TO -2.01	4.5	9.5
H5	-2 TO -1.01	8.0	8.0
H6	2.01 TO 3	9.5	4.5
H7	3.01 TO 4	12.0	4.5
H8	4.01 TO 5	15.0	4.5
H9	5.01 TO 6	21.5	4.5

BENCHMARK

CITY APPROVAL OF THE IMPROVEMENT
PLANS IS GRANTED FOR ONE (1) YEAR
ONLY. PLANS MUST BE RESUBMITTED
FOR REVIEW & APPROVAL TO THE
DEPARTMENT OF PUBLIC WORKS, CITY
OF HENDERSON IF WORK IS NOT
COMPLETED
BY: July 20 2002

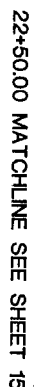
APPROVED BY:
Ken Y. Koshiro
KEN Y. KOSHIRO, P.E.,
NEW DEVELOPMENT ENGINEER, C.O.H.
7-20-01
DATE: 050906

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before you do
Overhead
1-702-593-6111

KBHOMESM
PARADISE HILLS NO. 18
PARADISE HILLS DRIVE
PLAN & PROFILE I
STA: 15+36.02 TO 22+50.00

SHEET
15
OF 26

16REV 1

ISLAND CURB CURVE TABLE					
AGE	CURVE	LENGTH	RADIUS	DELTA	TANGENT
0.03	IC3	21.99	7.00	180°00'00"	INFINITE
0.51	IC4	5.28	2.00	180°00'00"	INFINITE
9.57	IC5	50.06	250.03	11°28'20"	25.00
0.22	IC6	50.06	250.03	11°28'20"	25.00
0.74	IC7	44.78	250.00	10°54'47"	22.00
2.04	IC8	6.28	2.00	180°00'00"	INFINITE
9.36					

ISLAND CURB CURVE TABLE					
AGE	CURVE	LENGTH	RADIUS	DELTA	TANGENT
0.03	IC3	21.99	7.00	180°00'00"	INFINITE
0.51	IC4	5.28	2.00	180°00'00"	INFINITE
9.57	IC5	50.06	250.03	11°28'20"	25.00
0.22	IC6	50.06	250.03	11°28'20"	25.00
0.74	IC7	44.78	250.00	10°54'47"	22.00
2.04	IC8	6.28	2.00	180°00'00"	INFINITE
9.36					

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**KBHOME** SM

PARADISE HILLS DRIVE
PLAN & PROFILE

STA: 22+50.00 TO 31+07.69

STA: 22+50.00 TO 31+07.69

APPENDIX F

DATA CD

**UPDATED DATA CD
(HEC-1, WSPG, Work Maps & Figures)**